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MEMORANDUM

BASIC PRESSURE MEASUREMENTS AT TRANSONIC SPEEDS ON
A THIN 45° SWEPTBACK HIGHLY TAPERED WING WITH
SYSTEMATIC SPANWISE TWIST VARIATIONS
WING WITH LINEAR SPANWISE TWIST VARIATION

By John P. Mugler, Jr.

Langley Research Center
Langley Field, Va.

**NATIONAL AERONAUTICS AND
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SUMMARY

Pressure distributions obtained in the Langley 8-foot transonic pressure tunnel on a thin, highly tapered, twisted, 45° sweptback wing in combination with a body are presented. The wing has a linear spanwise twist variation from 0° at 10 percent of the semispan to 6° at the tip. The tip is at a lower angle of attack than the root. Tests were made at stagnation pressures of 1.0 and 0.5 atmosphere, at Mach numbers from 0.800 to 1.200, and at angles of attack from -4° to 12° .

INTRODUCTION

A research program has been conducted at the Langley Research Center to determine the loads due to wing twist at transonic and supersonic speeds. As part of this program, tests have been made in the Langley 8-foot transonic pressure tunnel on four wings; an untwisted wing to serve as a reference, and wings with linear, quadratic, and cubic variations of twist across the span. Reference 1 presents the basic pressure measurements on the untwisted wing at transonic speeds. The present paper presents the basic pressure measurements on the wing with a linear variation of twist across the span. These data are being presented without analysis.

SYMBOLS

b	wing span
b'/2	unsupported semispan (distance from outer face of wing mounting block to tip)
c	airfoil section chord, measured parallel to plane of symmetry
\bar{c}	wing mean aerodynamic chord
c_m	wing section pitching-moment coefficient about 0.25c, $\int_0^1 (C_{p,L} - C_{p,U}) \left(0.25 - \frac{x}{c}\right) d(x/c)$
c_n	wing section normal-force coefficient, $\int_0^1 (C_{p,L} - C_{p,U}) d(x/c)$
C_p	pressure coefficient
$C_{p,sonic}$	pressure coefficient corresponding to local Mach number of 1.0
D	diameter
l	body length
M	Mach number
q	free-stream dynamic pressure
R	Reynolds number based on \bar{c}
x	distance measured from leading edge of wing or from nose of body (positive rearward)
y	spanwise distance measured from body center line
y'	spanwise distance measured from outer face of wing mounting block
$\frac{\partial \Delta \alpha}{\partial n}$	wing-twist influence coefficient due to normal load at 0.25c

$\frac{\partial \Delta \alpha}{\partial m}$	wing-twist influence coefficient due to moment about 0.25c
α	angle of attack of wing-body center line
$\Delta \alpha$	angle of attack of wing station minus angle of attack of wing-body center line
Subscripts:	
L	lower surface
U	upper surface

APPARATUS

Tunnel

This investigation was conducted in the Langley 8-foot transonic pressure tunnel. The test section of this facility is rectangular in cross section. The upper and lower walls are slotted longitudinally to allow continuous operation through the transonic speed range with negligible effects of choking and blockage. During this investigation, the tunnel was operated at stagnation pressures of approximately 1.0 and 0.5 atmosphere. The dewpoint of the tunnel air was controlled and kept constant at approximately 0° F. The stagnation temperature of the tunnel air was automatically controlled and was kept constant and uniform across the tunnel at 123° F. Control of both dewpoint and stagnation temperature in this manner minimized humidity effects. Details of the test section have been presented in reference 2.

Models

The wing tested has the same plan form, thickness, and camber distribution as the untwisted wing described in reference 1. However, the wing of the present investigation had twist built into each wing panel from 10 percent of the semispan to the tip. The sections were twisted about the leading edge in planes parallel to the model plane of symmetry with the trailing edges up; therefore, the tips are at a lower angle of attack than the wing-body center line. The twist varied linearly from 0° at the 10-percent-semispan station to 6° at the tip. The wing was constructed of steel and was tested as a midwing configuration. The wing was tested in combination with the basic body of reference 1.

Details of the wing-body combination are presented in figure 1 and the wing twist characteristics are presented in table I.

TESTS

The wing-body combination was tested at Mach numbers from 0.800 to 1.200, at tunnel stagnation pressures of 1.0 and 0.5 atmosphere, and at angles of attack from -4° to 12° .

Transition strips were fixed on the model during all the tests. The strips were about 0.10 inch wide and were formed by sprinkling No. 120 carborundum grains on a plastic adhesive. The strips extended from the wing-body juncture to the wing tip at 10 percent of the local chord on the upper and lower wing surfaces and formed a ring around the body at 10 percent of the body length.

The Reynolds number based on the wing mean aerodynamic chord varied over the Mach number range from approximately 2.6×10^6 to 2.9×10^6 during tests at 1.0 atmosphere and from approximately 1.3×10^6 to 1.5×10^6 during tests at 0.5 atmosphere. (See fig. 2.)

MEASUREMENTS AND ACCURACY

Measurements of the local static pressures on the model were made using flush-mounted orifices distributed over the upper and lower wing surfaces and along longitudinal body rows. Figure 3 shows the location of the six stations on the wing and the five rows on the body where the orifices were located. Pressure coefficients determined from these measurements are estimated to be accurate within ± 0.006 .

The angle of attack of the model was measured by the use of a strain-gage attitude transmitter mounted in the nose of the model and is estimated to be accurate within $\pm 0.1^\circ$. Calibrations of the test section of the Langley 8-foot transonic pressure tunnel indicate that local deviations from the average free-stream Mach number are of the order of ± 0.005 at subsonic speeds. With increases in Mach number, these deviations increased but did not exceed ± 0.010 in the region of the wing at $M = 1.2$. Several representative Mach number distributions at the center of the test section have been presented in reference 2. The average stream Mach number was held to within ± 0.003 of the nominal values shown in the figures.

The stagnation pressures of 1,058 and 2,116 pounds per square foot have been designated 0.5 and 1.0 atmosphere, respectively, throughout this paper. The stagnation pressure was generally held to within ± 10 pounds per square foot during tests at 0.5 atmosphere and ± 20 pounds per square foot during tests at 1.0 atmosphere.

Influence coefficients were obtained for this wing from a static calibration and are presented in table II. Wing-twist angles, computed by using the experimental wing section data in conjunction with the influence coefficients of table II, are estimated to be accurate to within about $\pm 0.25^\circ$.

RESULTS

The pressure coefficients for the wing in the presence of the body are presented in tables III and IV for stagnation pressures of 0.5 and 1.0 atmosphere, respectively. Pressure coefficients for the body in the presence of the wing are presented in tables V and VI for stagnation pressures of 0.5 and 1.0 atmosphere, respectively. The values of the free-stream dynamic pressure shown in the tables are the average values over the angle-of-attack range. The pressure coefficients have been plotted to show the pressure-coefficient distributions over the surfaces and are presented in figure 4 for the wing and in figure 5 for the body. The distributions over the wing (fig. 4) have been numerically integrated for section normal-force and section pitching-moment coefficients about $0.25c$ and the results are presented in table VII. The section data were used in conjunction with the influence coefficients of table II to calculate the change in angle of attack at several wing stations and these values are also presented in table VII.

In figures 4 and 5, data have been presented for both stagnation pressures in the same figure. Fixing transition during the tests tended to minimize the effects of Reynolds number on the pressure coefficients. This fact is evident from figures 4 and 5 which show that in all cases changing the stagnation pressure from 0.5 to 1.0 atmosphere had no significant effects on the pressure coefficients over the body or over the inboard wing stations. Aeroelastic effects caused the wing to twist over the outboard regions. The results in table VII show that the outboard wing sections are generally operating at a lesser angle of attack at a stagnation pressure of 1.0 atmosphere than at a stagnation pressure of 0.5 atmosphere because of the differences in dynamic pressure. Therefore, the differences in the pressure distributions over the outboard wing sections at the two different stagnation pressures in

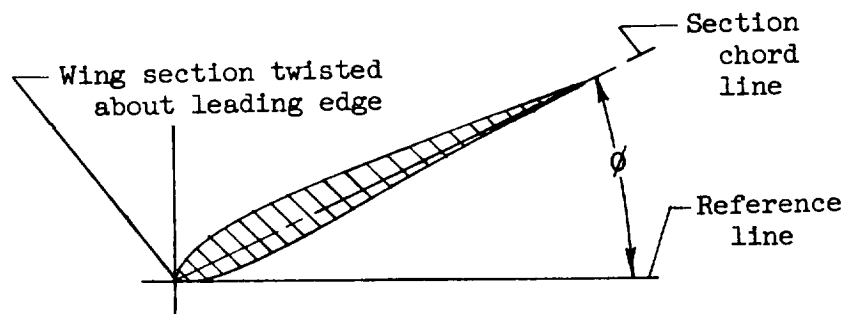
figure 4 should be attributed to the differences in local angle of attack and not to Reynolds number effects.

Langley Research Center,
National Aeronautics and Space Administration,
Langley Field, Va., October 3, 1958.

REFERENCES

1. Mugler, John P., Jr.: Basic Pressure Measurements at Transonic Speeds on a Thin 45° Sweptback Highly Tapered Wing With Systematic Spanwise Twist Variations - Untwisted Wing. NASA MEMO 10-20-58L, 1958.
2. Mugler, John P., Jr.: Transonic Wind-Tunnel Investigation of the Aerodynamic Loading Characteristics of a 60° Delta Wing in the Presence of a Body With and Without Indentation. NACA RM L55G11, 1955.

TABLE I.- WING TWIST CHARACTERISTICS



Typical Section

$\frac{y}{b/2}$	ϕ , deg
0	0
.10	0
.12	.133
.25	1.000
.40	2.000
.60	3.324
.80	4.667
.95	5.657
1.00	6.000

TABLE II.- WING DEFLECTION CHARACTERISTICS

Twist measurement station, $\frac{y}{b/2}$	Rate of change in twist angle due to a load at section quarter chord, $\frac{\partial \Delta\alpha}{\partial n}$, deg/lb, at -				
	$\frac{y'}{b'/2} = 0.185$	$\frac{y'}{b'/2} = 0.348$	$\frac{y'}{b'/2} = 0.565$	$\frac{y'}{b'/2} = 0.795$	$\frac{y'}{b'/2} = 0.948$
0.25	0	-0.0003	-0.0007	-0.0010	-0.0014
.40	0	-.0002	-.0016	-.0027	-.0031
.60	0	-.0002	-.0012	-.0088	-.0143
.80	0	-.0002	-.0006	-.0102	-.0382
.95	.0001	-.0002	-.0006	-.0099	-.0460

Twist measurement station, $\frac{y}{b/2}$	Rate of change in twist angle due to a pitching moment about section quarter chord, $\frac{\partial \Delta\alpha}{\partial m}$, deg/in-lb, at -				
	$\frac{y'}{b'/2} = 0.185$	$\frac{y'}{b'/2} = 0.348$	$\frac{y'}{b'/2} = 0.565$	$\frac{y'}{b'/2} = 0.795$	$\frac{y'}{b'/2} = 0.948$
0.25	0.0001	0.0001	0.0001	0.0001	0.0003
.40	.0001	.0003	.0002	.0002	.0009
.60	.0002	.0005	.0020	.0018	.0027
.80	.0002	.0005	.0031	.0123	.0119
.95	.0002	.0005	.0030	.0182	.0692

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY

(a) 12-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$			$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c	
		M = 0.600; q = 300 lb/sq ft									M = 0.900; q = 350 lb/sq ft									
Upper surface		.000	-.130	.136	.383	.489	.550	.537	.392			.049	.243	.436	.522	.575	.598	.529	.000	
		.025	.393	.304	.179	.053	-.110	-.601	-1.424			.406	.316	.204	.080	-.072	-.525	-1.038	.025	
		.072	.245	.160	.062	-.027	-.133	-.350	-.574			.257	.176	.095	-.001	-.098	-.267	-.489	.072	
		.150	.117	.038	-.051	-.125	-.205	-.381	-.583			.123	.042	-.043	-.113	-.192	-.322	-.479	.150	
		.250	.061	-.002	-.082	-.145	-.212	-.372	-.531			.061	-.005	-.081	-.144	-.211	-.349	-.475	.250	
		.350	.008	-.052	-.121	-.179	-.239	-.392	-.548			.008	-.058	-.130	-.191	-.255	-.395	-.504	.350	
		.450	-.026	-.077	-.140	-.192	-.249	-.384	-.495			-.030	-.095	-.160	-.219	-.282	-.417	-.530	.450	
		.550	-.068	-.118	-.176	-.224	-.275	-.395	-.456			-.088	-.148	-.218	-.296	-.371	-.488	-.604	.550	
		.650	-.045	-.091	-.144	-.182	-.220	-.314	-.358			-.068	-.118	-.179	-.241	-.344	-.488	-.601	.650	
		.750	-.034	-.070	-.113	-.143	-.170	-.233	-.289			-.050	-.091	-.144	-.182	-.235	-.355	-.475	.750	
Lower surface		.840	-.028	-.056	-.084	-.107	-.121	-.167	-.220			-.041	-.071	-.111	-.133	-.158	-.235	-.325	.840	
		.920	-.016	-.032	-.051	-.060	-.070	-.094	-.134			-.023	-.045	-.066	-.076	-.087	-.135	-.156	.920	
		.031	-.370	-.227	-.072	.033	.159	.363	.550			-.293	-.174	-.048	.056	.164	.374	.556	.031	
		.072	-.308	-.208	-.083	.010	.097	.270	.446			-.253	-.173	-.073	.005	.103	.284	.446	.072	
		.150	-.269	-.189	-.085	-.027	.061	.209	.360			-.237	-.171	-.084	-.019	.060	.220	.358	.150	
		.250	-.263	-.198	-.103	-.048	.026	.156	.286			-.258	-.201	-.114	-.052	.018	.162	.287	.250	
		.350																	.350	
		.450	-.274	-.217	-.140	-.091	-.029	.076	.181			-.290	-.242	-.170	-.111	-.050	.074	.177	.450	
		.550	-.258	-.206	-.137	-.090	-.035	.061	.154			-.332	-.272	-.188	-.123	-.062	.056	.148	.550	
		.650	-.229	-.189	-.128	-.087	-.042	.041	.123			-.348	-.273	-.175	-.121	-.067	.037	.114	.650	
Upper surface		.750	-.163	-.135	-.086	-.052	-.010	.055	.118			-.290	-.183	-.119	-.075	-.035	.053	.114	.750	
		.850	-.098	-.078	-.047	-.017	.012	.064	.105			-.127	-.097	-.063	-.030	-.005	.066	.106	.850	
		.900	-.070	-.050	-.023	.001	.025	.073	.104			-.074	-.060	-.036	-.006	.014	.075	.101	.900	
		M = 0.940; q = 365 lb/sq ft									M = 0.980; q = 380 lb/sq ft									
		.000	.113	.289	.472	.535	.590	.615	.575			.174	.336	.509	.567	.617	.652	.619	.000	
		.025	.408	.323	.223	.092	-.046	-.485	-.955			.434	.346	.253	.128	-.004	-.403	-.895	.025	
		.072	.260	.182	.104	.015	-.078	-.241	-.451			.285	.202	.131	.051	-.032	-.173	-.395	.072	
		.150	.122	.042	-.034	-.108	-.178	-.325	-.432			.147	.067	-.005	-.073	-.139	-.269	-.383	.150	
		.250	.061	-.010	-.073	-.137	-.199	-.326	-.438			.084	.013	-.045	-.101	-.160	-.269	-.379	.250	
		.350	-.002	-.065	-.129	-.183	-.257	-.370	-.464			.020	-.048	-.100	-.170	-.215	-.315	-.420	.350	
	.450	-.040	-.105	-.163	-.223	-.279	-.406	-.497			-.029	-.090	-.140	-.192	-.250	-.346	-.445	.450		
Lower surface		.550	-.109	-.179	-.257	-.311	-.360	-.478	-.574			-.113	-.184	-.231	-.280	-.330	-.426	-.527	.550	
		.650	-.089	-.147	-.238	-.311	-.366	-.478	-.571			-.097	-.186	-.237	-.289	-.340	-.425	-.520	.650	
		.750	-.073	-.118	-.175	-.304	-.362	-.481	-.576			-.088	-.172	-.237	-.290	-.344	-.430	-.531	.750	
		.840	-.062	-.093	-.128	-.232	-.360	-.502	-.569			-.103	-.178	-.254	-.311	-.364	-.454	-.551	.840	
		.920	-.048	-.059	-.075	-.088	-.228	-.441	-.425			-.099	-.165	-.234	-.287	-.336	-.431	-.531	.920	
		.031	-.257	-.146	-.028	.059	.170	.379	.565			-.214	-.099	.012	.102	.200	.398	.588	.031	
		.072	-.224	-.155	-.058	.005	.105	.289	.457			-.179	-.102	-.023	.051	.135	.311	.484	.072	
		.150	-.230	-.166	-.080	-.029	.063	.222	.369			-.201	-.127	-.055	.017	.087	.243	.397	.150	
		.250	-.239	-.189	-.119	-.064	.017	.161	.296			-.207	-.159	-.095	-.029	.037	.179	.322	.250	
		.350																	.350	
	.450	-.289	-.233	-.174	-.133	-.063	.066	.184			-.263	-.206	-.146	-.098	-.052	.075	.204	.450		
	.550	-.328	-.274	-.221	-.162	-.085	.043	.150			-.302	-.252	-.195	-.147	-.091	.044	.169	.550		
	.650	-.348	-.310	-.249	-.176	-.096	.018	.115			-.328	-.285	-.227	-.181	-.129	.012	.130	.650		
	.750	-.349	-.315	-.196	-.114	-.056	.030	.109			-.332	-.290	-.239	-.189	-.135	.021	.124	.750		
	.850	-.336	-.261	-.074	-.049	-.016	.037	.098			-.331	-.284	-.232	-.176	-.107	.030	.111	.850		
	.900	-.300	-.166	-.038	-.017	.005	.043	.087			-.324	-.273	-.221	-.158	-.082	.032	.103	.900		

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$			x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$			x/c							
M = 0.800; q = 300 lb/sq ft										M = 0.900; q = 350 lb/sq ft																			
Upper surface		.000	-.187	.032	.250	.393	.376	-.133	-.846			-.064	.100	.270	.403	.405	.060	-.444	.000			-.064	.100	.270	.403	.405	.060	-.444	.000
		.027	.338	.248	.117	-.036	-.248	-.886	-1.405			.330	.244	.120	-.024	-.215	-.812	-1.177	.027			.330	.244	.120	-.024	-.215	-.812	-1.177	.027
		.075	.193	.106	-.014	-.127	-.273	-.575	-1.142			.187	.096	-.015	-.125	-.271	-.508	-.988	.075			.187	.096	-.015	-.125	-.271	-.508	-.988	.075
		.140	.120	.042	-.063	-.157	-.270	-.519	-.975			.114	.037	-.068	-.165	-.277	-.496	-.778	.140			.114	.037	-.068	-.165	-.277	-.496	-.778	.140
		.250	.031	-.039	-.126	-.198	-.281	-.478	-.804			.023	-.050	-.139	-.216	-.298	-.484	-.727	.250			.023	-.050	-.139	-.216	-.298	-.484	-.727	.250
		.350	-.030	-.096	-.174	-.243	-.311	-.494	-.649			-.047	-.118	-.207	-.290	-.369	-.500	-.728	.350			-.047	-.118	-.207	-.290	-.369	-.500	-.728	.350
		.450	-.050	-.109	-.175	-.228	-.289	-.433	-.498			-.068	-.131	-.213	-.280	-.392	-.543	-.708	.450			-.068	-.131	-.213	-.280	-.392	-.543	-.708	.450
		.550	-.048	-.100	-.154	-.199	-.251	-.358	-.407			-.065	-.123	-.192	-.257	-.378	-.540	-.669	.550			-.065	-.123	-.192	-.257	-.378	-.540	-.669	.550
		.650	-.047	-.088	-.138	-.171	-.209	-.285	-.352			-.066	-.115	-.169	-.225	-.276	-.334	-.420	.650			-.066	-.115	-.169	-.225	-.276	-.334	-.420	.650
		.750	-.030	-.058	-.097	-.118	-.144	-.195	-.273			-.043	-.079	-.119	-.149	-.181	-.221	-.284	.750			-.043	-.079	-.119	-.149	-.181	-.221	-.284	.750
	.850	.007	-.015	-.042	-.050	-.067	-.097	-.168			-.002	-.029	-.052	-.065	-.077	-.123	-.235	.850			-.002	-.029	-.052	-.065	-.077	-.123	-.235	.850	
	.923	.026	.012	-.003	-.004	-.007	-.025	-.089			.025	.009	-.005	-.007	-.011	-.029	-.143	.923			.025	.009	-.005	-.007	-.011	-.029	-.143	.923	
Lower surface		.026	-.777	-.630	-.299	-.112	.090	.329	.467			-.710	-.597	-.333	-.105	.075	.328	.466	.026			-.710	-.597	-.333	-.105	.075	.328	.466	.026
		.074	-.792	-.538	-.158	-.072	.066	.246	.391			-.680	-.465	-.168	-.065	.054	.247	.384	.074			-.680	-.465	-.168	-.065	.054	.247	.384	.074
		.150	-.622	-.291	-.136	-.059	.035	.184	.313			-.575	-.319	-.151	-.065	.020	.183	.309	.150			-.575	-.319	-.151	-.065	.020	.183	.309	.150
		.250	-.200	-.122	-.059	.014	.141	.261	.313			-.229	-.230	-.147	-.073	-.003	.143	.250	.250			-.229	-.230	-.147	-.073	-.003	.143	.250	.250
		.350	-.232	-.209	-.136	-.077	-.009	.102	.212			-.282	-.261	-.171	-.103	-.034	.097	.199	.350			-.282	-.261	-.171	-.103	-.034	.097	.199	.350
		.450	-.242	-.207	-.139	-.090	-.027	.073	.168			-.320	-.275	-.187	-.122	-.056	.067	.162	.450			-.320	-.275	-.187	-.122	-.056	.067	.162	.450
		.550	-.203	-.171	-.115	-.073	-.017	.069	.150			-.319	-.251	-.156	-.102	-.046	.061	.137	.550			-.319	-.251	-.156	-.102	-.046	.061	.137	.550
		.650	-.165	-.137	-.091	-.057	-.009	.062	.128			-.289	-.188	-.123	-.080	-.034	.057	.118	.650			-.289	-.188	-.123	-.080	-.034	.057	.118	.650
		.750	-.105	-.083	-.048	-.021	.015	.075	.120			-.123	-.103	-.069	-.032	-.001	.072	.114	.750			-.123	-.103	-.069	-.032	-.001	.072	.114	.750
		.850	-.052	-.042	-.018	.003	.028	.068	.093			-.051	-.050	-.027	-.003	.016	.067	.083	.850			-.051	-.050	-.027	-.003	.016	.067	.083	.850
	.900	-.022	-.016	.002	.016	.038	.064	.079			-.014	-.013	-.001	.017	.029	.066	.065	.900			-.014	-.013	-.001	.017	.029	.066	.065	.900	
M = 0.940; q = 365 lb/sq ft										M = 0.980; q = 380 lb/sq ft																			
Upper surface		.000	-.013	.130	.286	.402	.417	.125	-.338			.039	.173	.314	.422	.444	.206	-.230	.000			.039	.173	.314	.422	.444	.206	-.230	.000
		.027	.329	.238	.128	-.013	-.184	-.750	-1.074			.345	.249	.148	.021	-.140	-.619	-1.073	.027			.345	.249	.148	.021	-.140	-.619	-1.073	.027
		.075	.180	.094	-.011	-.124	-.255	-.471	-.978			.199	.106	.012	-.097	-.219	-.444	-.867	.075			.199	.106	.012	-.097	-.219	-.444	-.867	.075
		.140	.110	.032	-.066	-.163	-.275	-.467	-.744			.124	.040	-.047	-.136	-.239	-.404	-.636	.140			.124	.040	-.047	-.136	-.239	-.404	-.636	.140
		.250	.017	-.056	-.137	-.215	-.291	-.473	-.693			.029	-.044	-.110	-.187	-.267	-.412	-.579	.250			.029	-.044	-.110	-.187	-.267	-.412	-.579	.250
		.350	-.066	-.145	-.225	-.291	-.343	-.487	-.677			-.064	-.140	-.197	-.254	-.303	-.425	-.579	.350			-.064	-.140	-.197	-.254	-.303	-.425	-.579	.350
		.450	-.089	-.159	-.241	-.317	-.392	-.532	-.681			-.094	-.166	-.234	-.294	-.362	-.479	-.602	.450			-.094	-.166	-.234	-.294	-.362	-.479	-.602	.450
		.550	-.087	-.147	-.242	-.335	-.398	-.532	-.657			-.087	-.191	-.256	-.311	-.369	-.476	-.601	.550			-.087	-.191	-.256	-.311	-.369	-.476	-.601	.550
		.650	-.090	-.147	-.214	-.336	-.412	-.544	-.640			-.118	-.201	-.266	-.329	-.391	-.499	-.610	.650			-.118	-.201	-.266	-.329	-.391	-.499	-.610	.650
		.750	-.066	-.102	-.140	-.270	-.398	-.531	-.613			-.105	-.207	-.273	-.330	-.386	-.481	-.601	.750			-.105	-.207	-.273	-.330	-.386	-.481	-.601	.750
		.850	-.025	-.038	-.052	-.062	-.222	-.446	-.530			-.075	-.157	-.233	-.297	-.360	-.456	-.584	.850			-.075	-.157	-.233	-.297	-.360	-.456	-.584	.850
		.923	.004	-.002	-.001	.005	-.033	-.197	-.293			-.089	-.133	-.194	-.232	-.278	-.358	-.519	.923			-.089	-.133	-.194	-.232	-.278	-.358	-.519	.923
Lower surface		.026	-.681	-.574	-.339	-.131	.059	.319	.473			-.642	-.534	-.303	-.077	.083	.332	.496	.026			-.642	-.534	-.303	-.077	.083	.332	.496	.026
		.074	-.625	-.439	-.170	-.089	.042	.242	.392			-.577	-.369	-.162	-.039	.064	.256	.411	.074			-.577	-.369	-.162	-.039	.064	.256	.411	.074
		.150	-.539	-.308	-.157	-.082	.011	.178	.314			-.523	-.284	-.139	-.044	.028	.190	.334	.150			-.523	-.284	-.139	-.044	.028	.190	.334	.150
		.250	-.253	-.223	-.151	-.092	-.018	.132	.256			-.245	-.203	-.120	-.058	-.005	.142	.277	.250			-.245	-.203	-.120	-.058	-.005	.142	.277	.250
		.350	-.288	-.260	-.196	-.137	-.050	.087	.203			-.264	-.239	-.165	-.113	-.048	.094	.225	.350			-.264	-.239	-.165	-.113	-.048	.094	.225	.350
		.450	-.313	-.284	-.218	-.172	-.082	.050	.162			-.289	-.258	-.197	-.146	-.093	.048	.178	.450			-.289	-.258	-.197	-.146	-.093	.048	.178	.450
		.550	-.325	-.298	-.229	-.153	-.072	.042	.137			-.310	-.272	-.216	-.163	-.108	.034	.153	.550			-.310	-.272	-.216	-.163	-.108	.034	.153	.550
		.650	-.356	-.324	-.196	-.125	-.054	.033	.115			-.343	-.302	-.247	-.192	-.129	.020	.127	.650			-.343	-.302	-.247	-.192	-.129	.020	.127	.650
		.750	-.333	-.268	-.078	-.056	-.016	.044	.106			-.329	-.283	-.226	-.164	-.100	.032	.114	.750			-.329	-.283	-.226	-.164	-.100	.032	.114	.750
		.850	-.270	-.085	-.025	-.017	.005	.030	.064			-.322	-.278	-.222	-.168	-.095	.008	.073	.850			-.322	-.278	-.222	-.168	-.095	.008	.073	.850
	.900	-.119	-.025	.000	.008	.022	.017	.041			-.313	-.264	-.213	-.155	-.076	-.012	.041	.900			-.313	-.264	-.213	-.155	-.076	-.012	.041	.900	

TABLE III.- PRESSURE COEFFICIENTS AT STAGMATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - concluded

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	
	M = 1.050; q = 397 lb/sq ft								
Upper surface	.000	.119	.237	.358	.462	.489	.279	-.114	
	.027	.391	.301	.194	.074	-.075	-.515	-.982	
	.075	.250	.161	.060	-.044	-.151	-.374	-.821	
	.140	.179	.095	.002	-.087	-.173	-.312	-.499	
	.250	.087	.022	-.061	-.136	-.203	-.332	-.461	
	.350	-.009	-.070	-.140	-.185	-.236	-.344	-.468	
	.450	-.036	-.102	-.173	-.238	-.295	-.395	-.498	
	.550	-.060	-.125	-.194	-.251	-.297	-.394	-.497	
	.650	-.072	-.133	-.213	-.273	-.325	-.418	-.512	
	.750	-.080	-.146	-.213	-.269	-.313	-.402	-.505	
	.850	-.044	-.107	-.178	-.243	-.292	-.386	-.491	
	.923	-.056	-.099	-.156	-.212	-.250	-.311	-.435	
	M = 1.200; q = 457 lb/sq ft								
Lower surface	.026	-.535	-.465	-.244	-.028	.126	.381	.539	
	.074	-.459	-.309	-.100	.001	.108	.307	.458	
	.150	-.426	-.210	-.091	-.005	.080	.241	.385	
	.250	-.182	-.142	-.067	.000	.050	.194	.329	
	.350	-.194	-.174	-.118	-.056	.004	.145	.277	
	.450	-.216	-.192	-.137	-.085	-.029	.098	.230	
	.550	-.235	-.207	-.153	-.104	-.046	.085	.207	
	.650	-.268	-.235	-.185	-.136	-.074	.071	.183	
	.750	-.256	-.215	-.166	-.112	-.043	.087	.179	
	.850	-.254	-.212	-.166	-.115	-.050	.066	.133	
	.900	-.254	-.209	-.162	-.113	-.049	.053	.108	
	M = 1.050; q = 397 lb/sq ft								
Upper surface	.000	.259	.347	.441	.500	.523	.427	.191	
	.027	.396	.318	.231	.108	-.013	-.379	-.646	
	.075	.259	.173	.093	.005	-.082	-.309	-.602	
	.140	.194	.120	.047	-.034	-.105	-.247	-.532	
	.250	.114	.049	-.008	-.078	-.136	-.267	-.292	
	.350	.057	.003	-.043	-.102	-.155	-.263	-.329	
	.450	.004	-.057	-.106	-.172	-.224	-.309	-.369	
	.550	-.011	-.066	-.115	-.176	-.218	-.293	-.360	
	.650	-.038	-.097	-.142	-.196	-.239	-.324	-.399	
	.750	-.032	-.084	-.128	-.181	-.221	-.303	-.374	
	.850	-.021	-.076	-.122	-.174	-.214	-.293	-.360	
	.923	-.014	-.060	-.104	-.154	-.198	-.273	-.331	
	M = 1.200; q = 457 lb/sq ft								
Lower surface	.026	-.413	-.351	-.180	-.003	.130	.347	.522	
	.074	-.279	-.198	-.051	.025	.116	.287	.450	
	.150	-.204	-.130	-.037	.023	.097	.241	.386	
	.250	-.154	-.093	-.018	.042	.095	.222	.347	
	.350	-.142	-.102	-.045	.000	.050	.168	.300	

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c	
	M = 0.800; q = 408 lb/sq ft									M = 0.900; q = 350 lb/sq ft								
Upper surface	.000	.176	.248	.328	.358	-.039	-1.085	-1.299		.224	.275	.336	.361	.054	-.994	-1.240	.000	
	.030	.393	.330	.210	.033	-.261	-1.157	-1.289		.383	.311	.196	.028	-.244	-1.094	-1.271	.030	
	.078	.234	.146	.025	-.115	-.303	-.846	-1.261		.216	.126	.005	-.135	-.320	-.798	-1.231	.078	
	.150	.140	.062	-.046	-.155	-.295	-.664	-1.254		.125	.041	-.070	-.188	-.334	-.626	-1.133	.150	
	.260	.071	.007	-.089	-.173	-.284	-.524	-1.253		.057	-.016	-.122	-.222	-.342	-.590	-1.030	.260	
	.350	.025	-.039	-.121	-.190	-.273	-.463	-1.090		.008	-.059	-.148	-.242	-.380	-.583	-.955	.350	
	.450	-.008	-.066	-.135	-.196	-.264	-.408	-.909		-.022	-.087	-.166	-.248	-.390	-.596	-.860	.450	
	.550	-.028	-.073	-.134	-.178	-.242	-.339	-.769		-.039	-.096	-.162	-.220	-.276	-.418	-.679	.550	
	.660	-.030	-.069	-.118	-.155	-.198	-.267	-.553		-.044	-.090	-.144	-.191	-.246	-.357	-.517	.660	
	.750	-.026	-.056	-.095	-.121	-.148	-.192	-.407		-.037	-.073	-.113	-.144	-.176	-.219	-.280	.750	
	.860	.010	-.017	-.039	-.053	-.068	-.098	-.270		.001	-.021	-.046	-.061	-.081	-.075	-.155	.860	
	.930	.026	.007	-.004	-.012	-.019	-.033	-.181		.020	.005	-.010	-.012	-.020	-.016	-.024	.930	
Lower surface	.032	-.861	-.777	-.344	-.187	.089	.336	.454		-.856	-.862	-.422	-.206	.056	.318	.439	.032	
	.083	-.741	-.552	-.211	-.113	.057	.247	.379		-.667	-.525	-.241	-.126	.030	.235	.359	.083	
	.160	-.759	-.513	-.183	-.115	.029	.177	.304		-.668	-.458	-.219	-.125	.001	.170	.285	.160	
	.240	-.806	-.400	-.170	-.092	.005	.134	.242		-.765	-.428	-.222	-.118	-.028	.122	.226	.240	
	.360	-.449	-.262	-.154	-.089	-.013	.100	.193		-.587	-.382	-.206	-.122	-.047	.087	.178	.360	
	.450	-.179	-.188	-.122	-.069	-.005	.087	.164		-.404	-.292	-.160	-.098	-.033	.078	.153	.450	
	.550	-.095	-.125	-.075	-.033	.019	.094	.155		-.209	-.170	-.098	-.046	.001	.090	.148	.550	
	.660	-.051	-.069	-.031	.005	.048	.109	.148		-.060	-.085	-.042	-.001	.033	.106	.146	.660	
	.750	-.007	-.021	.004	.035	.068	.119	.139		.003	-.029	.002	.036	.060	.117	.137	.750	
	.840	.013	.002	.023	.045	.071	.104	.113		.025	.001	.022	.047	.067	.109	.106	.840	
	.910	.029	.023	.033	.045	.067	.087	.077		.041	.021	.033	.050	.063	.090	.064	.910	
	M = 0.940; q = 365 lb/sq ft									M = 0.960; q = 380 lb/sq ft								
Upper surface	.000	.243	.287	.344	.363	.112	-.953	-1.198		.268	.309	.360	.383	.170	-.817	-1.168	.000	
	.030	.369	.297	.194	.033	-.205	-1.115	-1.226		.380	.300	.206	.058	-.152	-.974	-1.263	.030	
	.078	.199	.110	-.004	-.139	-.303	-.799	-1.181		.205	.111	.012	-.112	-.258	-.732	-1.213	.078	
	.150	.110	.019	-.088	-.195	-.326	-.562	-1.092		.109	.017	-.070	-.183	-.302	-.479	-1.095	.150	
	.260	.036	-.043	-.151	-.232	-.335	-.561	-.974		.039	-.051	-.122	-.206	-.324	-.500	-.772	.260	
	.350	-.016	-.089	-.197	-.282	-.365	-.576	-.910		-.022	-.121	-.193	-.261	-.347	-.512	-.678	.350	
	.450	-.048	-.118	-.206	-.336	-.412	-.581	-.824		-.065	-.166	-.244	-.315	-.382	-.526	-.655	.450	
	.550	-.063	-.122	-.184	-.341	-.442	-.615	-.722		-.084	-.177	-.264	-.352	-.439	-.560	-.665	.550	
	.660	-.067	-.111	-.168	-.291	-.422	-.602	-.651		-.116	-.185	-.278	-.345	-.417	-.548	-.664	.660	
	.750	-.059	-.089	-.122	-.130	-.419	-.599	-.609		-.115	-.208	-.300	-.366	-.436	-.555	-.668	.750	
	.860	-.011	-.029	-.048	-.049	-.084	-.290	-.445		-.090	-.161	-.253	-.338	-.407	-.519	-.633	.860	
	.930	.016	.004	-.006	-.004	.004	-.133	-.353		-.050	-.055	-.127	-.175	-.258	-.356	-.450	.930	
Lower surface	.032	-.876	-.898	-.468	-.274	.015	.305	.440		-.894	-.862	-.467	-.184	.032	.304	.458	.032	
	.083	-.625	-.506	-.247	-.163	.004	.222	.360		-.582	-.466	-.230	-.114	.013	.225	.372	.083	
	.160	-.602	-.422	-.235	-.171	-.030	.156	.284		-.554	-.370	-.207	-.122	-.031	.152	.298	.160	
	.240	-.694	-.397	-.264	-.170	-.058	.104	.226		-.549	-.342	-.231	-.151	-.077	.098	.236	.240	
	.360	-.585	-.405	-.283	-.184	-.076	.062	.172		-.553	-.366	-.265	-.193	-.120	.051	.183	.360	
	.450	-.441	-.393	-.262	-.150	-.058	.052	.147		-.476	-.370	-.278	-.211	-.142	.039	.155	.450	
	.550	-.379	-.365	-.122	-.083	-.017	.064	.140		-.427	-.350	-.271	-.198	-.127	.051	.147	.550	
	.660	-.340	-.236	-.037	-.017	.024	.079	.136		-.378	-.313	-.241	-.153	-.040	.065	.142	.660	
	.750	-.174	-.049	.008	.028	.056	.089	.128		-.317	-.254	-.180	-.087	.007	.064	.127	.750	
	.840	-.026	.014	.027	.041	.066	.075	.087		-.262	-.195	-.130	-.048	.007	.037	.085	.840	
	.910	.030	.035	.041	.043	.065	.046	.042		-.157	-.110	-.068	-.015	-.004	-.009	.024	.910	

	x/c	$\alpha = -40^\circ$	$\alpha = -20^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 40^\circ$	$\alpha = 60^\circ$	$\alpha = 120^\circ$	
	M = 1.030; q = 397 lb/sq ft								
Upper surface	.000	.329	.369	.401	.426	.239	-.674	-1.019	
	.030	.423	.354	.251	.115	-.083	-.829	-1.110	
	.078	.254	.169	.060	-.057	-.186	-.635	-1.055	
	.150	.159	.082	-.018	-.121	-.228	-.397	-.974	
	.260	.083	.018	-.063	-.160	-.251	-.417	-.714	
	.350	.019	-.055	-.125	-.202	-.275	-.426	-.570	
	.450	-.026	-.099	-.181	-.243	-.309	-.437	-.551	
	.550	-.038	-.118	-.204	-.292	-.360	-.474	-.566	
	.660	-.070	-.137	-.214	-.282	-.346	-.465	-.564	
	.750	-.091	-.153	-.233	-.301	-.362	-.473	-.574	
	.860	-.068	-.125	-.204	-.281	-.338	-.447	-.552	
	.930	-.068	-.105	-.160	-.226	-.281	-.337	-.409	
Lower surface	.032	-.778	-.771	-.476	-.133	.082	.353	.502	
	.083	-.473	-.404	-.172	-.063	.070	.270	.420	
	.160	-.449	-.307	-.148	-.060	.030	.206	.347	
	.240	-.427	-.274	-.167	-.089	-.018	.146	.286	
	.360	-.439	-.297	-.201	-.131	-.061	.096	.233	
	.450	-.397	-.304	-.218	-.152	-.081	.086	.211	
	.550	-.356	-.286	-.210	-.144	-.072	.102	.207	
	.660	-.314	-.251	-.182	-.113	-.024	.118	.203	
	.750	-.259	-.195	-.128	-.055	.030	.124	.190	
	.840	-.220	-.160	-.094	-.028	.031	.096	.150	
	.910	-.175	-.124	-.073	-.033	.004	.047	.089	
	M = 1.000; q = 437 lb/sq ft								
Upper surface	.000	.439	.457	.489	.482	.357	-.290	-.649	
	.030	.456	.395	.321	.177	-.002	-.492	-.740	
	.078	.286	.207	.131	.035	-.097	-.417	-.695	
	.150	.194	.120	.047	-.038	-.126	-.356	-.658	
	.260	.136	.060	.000	-.088	-.162	-.307	-.626	
	.350	.075	.015	-.053	-.132	-.187	-.316	-.608	
	.450	.023	-.033	-.088	-.158	-.224	-.348	-.526	
	.550	-.018	-.091	-.140	-.207	-.253	-.362	-.494	
	.660	-.032	-.090	-.145	-.207	-.253	-.354	-.410	
	.750	-.060	-.112	-.161	-.224	-.273	-.362	-.432	
	.860	-.048	-.099	-.148	-.205	-.252	-.349	-.425	
	.930	-.038	-.093	-.134	-.189	-.236	-.327	-.405	
Lower surface	.032	-.582	-.616	-.410	-.094	.085	.357	.515	.032
	.083	-.444	-.388	-.109	-.020	.097	.296	.438	.083
	.160	-.289	-.180	-.078	.002	.079	.242	.366	.160
	.240	-.250	-.172	-.086	.017	.050	.180	.301	.240
	.360	-.235	-.180	-.105	.053	.006	.120	.241	.360
	.450	-.251	-.202	-.131	.088	-.034	.085	.212	.450
	.550	-.249	-.207	-.139	.088	-.033	.079	.215	.550
	.660	-.217	-.188	-.130	.079	-.022	.092	.274	.660
	.750	-.178	-.133	-.084	.045	.006	.133	.291	.750
	.840	-.144	-.106	-.045	.007	.057	.181	.268	.840
	.910	-.126	-.095	-.036	.013	.060	.159	.222	.910

	$\alpha = -40^\circ$	$\alpha = -20^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 40^\circ$	$\alpha = 60^\circ$	$\alpha = 120^\circ$	x/c
	M = 1.125; q = 421 lb/sq ft							
	.377	.402	.437	.450	.309	-.467	-.794	.000
	.425	.355	.276	.161	-.058	-.643	-.873	.030
	.253	.176	.089	-.003	-.132	-.542	-.835	.078
	.170	.040	.010	-.075	-.164	-.376	-.782	.150
	.109	.003	-.034	-.110	-.208	-.359	-.724	.260
	.044	-.022	-.080	-.157	-.237	-.378	-.595	.350
	-.004	-.070	-.125	-.187	-.250	-.392	-.468	.450
	-.028	-.105	-.177	-.239	-.298	-.404	-.473	.550
	-.049	-.168	-.269	-.228	-.290	-.404	-.472	.660
	-.070	-.132	-.190	-.248	-.304	-.420	-.486	.750
	-.040	-.117	-.176	-.232	-.290	-.395	-.466	.860
	-.037	-.096	-.137	-.214	-.268	-.335	-.418	.930
	-.731	-.661	-.470	-.120	.067	.348	.505	.032
	-.474	-.369	-.145	-.046	.084	.277	.429	.083
	-.398	-.244	-.119	-.022	.061	.212	.358	.160
	-.331	-.203	-.128	-.043	.025	.162	.302	.240
	-.312	-.232	-.145	-.082	-.023	.109	.235	.360
	-.324	-.236	-.168	-.107	-.046	.088	.240	.450
	-.310	-.225	-.158	-.099	-.039	.097	.248	.550
	-.278	-.204	-.141	-.077	-.014	.136	.258	.660
	-.228	-.160	-.094	-.035	.035	.177	.258	.750
	-.189	-.109	-.057	.005	.063	.163	.222	.860
	-.167	-.009	-.050	.005	.048	.123	.171	.910
								.000
								.030
								.078
								.150
								.260
								.350
								.450
								.550
								.660
								.750
								.860
								.930

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 60-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c
M = 0.800; q = 300 lb/sq ft																	
Upper surface	.000	-.433	-.097	.244	.465	.402	-.430	-.675	-.421	-.059	.251	.467	.403	-.312	-.733	.000	
	.020	.422	.362	.239	.064	-.306	-.939	-.733	.411	.349	.230	.040	-.367	-1.295	-.893	.020	
	.077	.298	.219	.095	-.036	-.253	-.867	-.707	.284	.204	.083	-.067	-.326	-1.119	-.839	.077	
	.150	.207	.127	.020	-.091	-.249	-.832	-.707	.199	.111	-.002	-.125	-.327	-.965	-.814	.150	
	.250	.134	.057	-.035	-.128	-.248	-.767	-.692	.118	.041	-.054	-.161	-.327	-.675	-.760	.250	
	.350	.077	.012	-.069	-.145	-.243	-.656	-.674	.067	.002	-.084	-.179	-.298	-.651	-.731	.350	
	.450	.057	.006	-.066	-.126	-.203	-.482	-.622	.052	-.008	-.081	-.156	-.255	-.626	-.672	.450	
	.550	.010	-.037	-.096	-.149	-.215	-.374	-.627	.006	-.049	-.115	-.177	-.258	-.547	-.666	.550	
	.640	-.001	-.039	-.093	-.132	-.185	-.267	-.603	-.007	-.052	-.107	-.158	-.222	-.260	-.617	.640	
	.740	-.012	-.045	-.086	-.115	-.152	-.180	-.577	-.016	-.055	-.095	-.135	-.170	-.128	-.587	.740	
Lower surface	.850	.016	-.006	-.036	-.058	-.074	-.093	-.533	.014	-.014	-.043	-.062	-.083	-.055	-.536	.850	
	.900	.032	.007	-.020	-.027	-.044	-.058	-.517	.031	.003	-.023	-.032	-.046	-.027	-.531	.900	
	.922	.040	.012	-.013	-.018	-.027	-.044	-.510	.040	.009	-.015	-.020	-.027	-.013	-.502	.922	
	.040	-.695	-.597	-.374	-.177	.075	.311	.417	-.779	-.656	-.425	-.202	.049	.287	.392	.040	
	.090	-.681	-.575	-.337	-.122	.058	.250	.358	-.757	-.620	-.381	-.133	.035	.235	.338	.090	
	.150	-.671	-.566	-.303	-.104	.039	.200	.302	-.737	-.600	-.334	-.116	.018	.187	.284	.150	
	.250	-.686	-.574	-.229	-.064	.065	.178	.260	-.725	-.610	-.278	-.074	.047	.173	.248	.250	
	.340	-.730	-.590	-.168	-.069	.037	.144	.209	-.737	-.643	-.210	-.073	.022	.137	.197	.340	
	.450	-.733	-.590	-.098	-.053	.040	.125	.171	-.725	-.553	-.125	-.054	.028	.122	.162	.450	
	.550	-.706	-.584	-.062	-.017	.043	.113	.140	-.739	-.540	-.079	-.021	.035	.114	.132	.550	
Upper surface	.650	-.503	-.284	-.020	.016	.055	.112	.113	-.539	-.129	-.030	.013	.053	.118	.106	.650	
	.800	.012	.051	.024	.058	.080	.112	.055	.052	.050	.025	.057	.078	.120	.056	.800	
	.874	.139	.075	.041	.060	.079	.095	-.011	.183	.082	.042	.063	.077	.109	.006	.874	
	M = 0.940; q = 365 lb/sq ft																
	.000	-.339	-.021	.240	.439	.414	-.172	-.673	-.248	.042	.246	.417	.413	-.023	-.602	.000	
	.020	.391	.318	.204	.016	-.314	-1.228	-.911	.380	.289	.188	.029	-.243	-1.081	-1.314	.020	
	.077	.261	.175	.060	-.094	-.310	-1.093	-.883	.248	.143	.042	-.095	-.265	-.939	-1.208	.077	
	.150	.169	.084	-.023	-.161	-.342	-1.035	-.890	.154	.050	-.043	-.159	-.304	-.895	-1.204	.150	
	.250	.095	.015	-.078	-.239	-.390	-.824	-.845	.068	-.028	-.135	-.232	-.360	-.743	-1.163	.250	
	.350	.044	-.024	-.103	-.280	-.405	-.583	-.804	.017	-.094	-.195	-.285	-.397	-.514	-1.132	.350	
.450	.032	-.030	-.092	-.208	-.406	-.587	-.721	-.007	-.105	-.199	-.297	-.394	-.526	-1.020	.450		
.550	-.015	-.063	-.124	-.176	-.433	-.679	-.737	-.058	-.174	-.253	-.337	-.438	-.612	-1.058	.550		
Lower surface	.640	-.024	-.064	-.114	-.158	-.419	-.653	-.692	-.074	-.187	-.275	-.355	-.421	-.615	-.953	.640	
	.740	-.033	-.063	-.102	-.139	-.433	-.658	-.644	-.071	-.078	-.356	-.460	-.567	-.683	-.909	.740	
	.850	-.005	-.024	-.044	-.064	-.035	-.157	-.567	-.038	-.038	-.092	-.275	-.443	-.647	-.818	.850	
	.900	.010	-.011	-.022	-.035	-.005	-.081	-.553	-.029	-.027	-.009	-.090	-.282	-.607	-.740	.900	
	.922	.015	-.006	-.010	-.018	.008	-.052	-.529	-.027	-.020	.014	-.038	-.181	-.499	-.646	.922	
	.040	-.775	-.685	-.518	-.291	-.009	.256	.382	-.744	-.631	-.521	-.332	-.062	.231	.379	.040	
	.090	-.752	-.640	-.458	-.197	-.007	.208	.328	-.717	-.596	-.469	-.211	-.066	.186	.328	.090	
	.150	-.747	-.621	-.388	-.175	-.020	.161	.271	-.714	-.581	-.405	-.215	-.083	.137	.272	.150	
	.250	-.750	-.582	-.292	-.122	.022	.145	.234	-.721	-.568	-.359	-.192	-.068	.118	.236	.250	
	.340	-.760	-.533	-.219	-.102	-.001	.107	.187	-.746	-.553	-.350	-.221	-.106	.083	.186	.340	
.450	-.701	-.475	-.137	-.079	.014	.096	.152	-.762	-.546	-.322	-.192	-.062	.062	.149	.450		
.550	-.663	-.334	-.090	-.036	.024	.084	.123	-.768	-.483	-.292	-.167	-.039	.041	.118	.550		
.650	-.550	-.216	-.038	.002	.048	.089	.099	-.685	-.371	-.234	-.097	-.003	.035	.098	.650		
.800	-.278	-.088	.023	.043	.084	.093	.055	-.400	-.184	-.033	.043	.039	.027	.062	.800		
.874	-.127	-.038	.045	.053	.086	.081	.004	-.269	-.105	.028	.064	.042	-.002	.014	.874		

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - Concluded

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	
		M = 1.050; q = 597 lb/sq ft							
Upper surface	.000	-.136	.109	.294	.459	.458	.078	-.461	
	.020	.410	.342	.235	.089	-.173	-.939	-1.164	
	.077	.280	.199	.097	-.033	-.188	-.796	-1.052	
	.150	.185	.107	.010	-.102	-.229	-.760	-1.045	
	.250	.102	.024	-.068	-.179	-.276	-.665	-1.014	
	.350	.041	-.049	-.128	-.220	-.318	-.442	-.990	
	.450	.023	-.050	-.141	-.233	-.318	-.432	-.885	
	.550	-.046	-.110	-.182	-.268	-.363	-.519	-.941	
	.640	-.054	-.133	-.212	-.282	-.350	-.531	-.897	
	.740	-.095	-.199	-.291	-.408	-.477	-.596	-.859	
Lower surface	.850	-.073	-.139	-.239	-.324	-.443	-.562	-.769	
	.900	-.057	-.115	-.200	-.309	-.389	-.556	-.734	
	.922	-.047	-.096	-.166	-.273	-.357	-.539	-.706	
	.040	-.637	-.555	-.453	-.270	-.012	.270	.425	
	.090	-.068	-.516	-.398	-.145	-.007	.227	.375	
	.150	-.600	-.502	-.336	-.153	.021	.185	.322	
	.250	-.600	-.487	-.285	-.136	.009	.165	.288	
	.340	-.618	-.473	-.279	-.158	.057	.132	.242	
	.450	-.637	-.470	-.257	-.146	.031	.114	.208	
	.550	-.641	-.437	-.236	-.127	.027	.095	.176	
Upper surface	.650	-.632	-.379	-.201	-.104	-.021	.088	.158	
	.800	-.435	-.249	-.111	-.036	.019	.078	.122	
	.874	-.299	-.182	-.067	-.017	.021	.049	.083	
		M = 1.000; q = 437 lb/sq ft							
	.000	.048	.206	.343	.487	.502	.275	-.098	
	.020	.437	.373	.293	.154	-.043	-.552	-.781	
	.077	.310	.235	.157	.043	-.085	-.484	-.685	
	.150	.216	.136	.071	-.026	-.139	-.480	-.691	
	.250	.142	.065	-.004	-.082	-.175	-.460	-.684	
	.350	.082	.006	-.059	-.129	-.202	-.428	-.678	
Lower surface	.450	.066	-.003	-.069	-.133	-.190	-.361	-.603	
	.550	.023	-.043	-.108	-.206	-.254	-.385	-.659	
	.640	-.006	-.054	-.102	-.181	-.275	-.379	-.644	
	.740	-.074	-.170	-.223	-.274	-.335	-.429	-.648	
	.850	-.044	-.108	-.188	-.264	-.314	-.421	-.641	
	.900	-.039	-.113	-.181	-.258	-.314	-.424	-.644	
	.922	-.037	-.109	-.171	-.252	-.307	-.415	-.645	
	.040	-.496	-.464	-.383	-.208	.009	.264	.428	
	.090	-.462	-.425	-.338	-.113	.020	.222	.385	
	.150	-.421	-.399	-.245	-.087	.014	.185	.340	
.250	-.386	-.343	-.170	-.066	.033	.178	.332		
.340	-.369	-.305	-.177	-.097	-.025	.122	.299		
.450	-.321	-.268	-.161	-.091	-.019	.144	.291		
.550	-.309	-.256	-.146	-.067	-.001	.151	.277		
.650	-.294	-.239	-.119	-.051	.013	.155	.273		
.800	-.259	-.185	-.059	.004	.072	.186	.257		
.874	-.216	-.158	-.034	.023	.085	.177	.226		

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued
(e) 80-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c
	M = 0.800; q = 308 lb/sq ft																
Upper surface	.036	.432	.390	.297	.157	-.180	-.620	-.504		.437	.392	.296	.144	-.231	-1.311	-.578	.036
	.084	.350	.290	.188	.060	-.183	-.609	-.494		.353	.292	.189	.045	-.229	-1.250	-.578	.084
	.150	.258	.195	.090	-.017	-.203	-.576	-.487		.262	.195	.088	-.038	-.255	-1.175	-.571	.150
	.260	.175	.115	.029	-.069	-.205	-.548	-.471		.177	.114	.023	-.090	-.255	-1.138	-.533	.260
	.350	.111	.058	-.016	-.106	-.215	-.510	-.458		.112	.054	-.023	-.129	-.269	-.851	-.513	.350
	.460	.052	.012	-.050	-.127	-.214	-.474	-.443		.059	.012	-.061	-.152	-.274	-.491	-.476	.460
	.550	.016	-.017	-.068	-.135	-.206	-.454	-.433		.020	-.017	-.081	-.158	-.260	-.391	-.471	.550
	.600	-.011	-.031	-.078	-.133	-.199	-.439	-.423		-.004	-.032	-.091	-.160	-.247	-.334	-.467	.600
	.660	-.032	-.039	-.079	-.128	-.186	-.413	-.418		-.027	-.040	-.095	-.152	-.227	-.286	-.459	.660
	.760	-.065	-.046	-.068	-.100	-.143	-.369	-.401		-.064	-.047	-.082	-.125	-.173	-.205	-.441	.760
.860	-.132	-.062	-.055	-.074	-.094	-.323	-.388		-.125	-.058	-.066	-.088	-.112	-.130	-.431	.860	
.900	-.169	-.073	-.044	-.061	-.078	-.302	-.382		-.165	-.074	-.048	-.070	-.084	-.098	-.431	.900	
Lower surface	.079	-.449	-.476	-.420	-.184	.041	.261	.329		-.436	-.480	-.432	-.216	.046	.265	.324	.079
	.160	-.436	-.463	-.406	-.124	.019	.197	.254		-.423	-.466	-.419	-.123	.017	.210	.252	.160
	.250	-.426	-.462	-.418	-.094	.040	.169	.208		-.420	-.468	-.426	-.089	.037	.177	.207	.250
	.350	-.416	-.478	-.415	.060	.041	.142	.161		-.421	-.493	-.432	-.058	.039	.154	.164	.350
	.450	-.400	-.485	-.327	.040	.048	.121	.123		-.403	-.515	-.378	-.035	.046	.139	.130	.450
	.550	-.410	-.500	.185	.020	.053	.103	.084		-.427	-.541	-.275	-.016	.048	.123	.090	.550
	.650	-.410	-.499	.134	.012	.062	.105	.078		-.430	-.539	-.225	-.004	.060	.128	.086	.650
	.690	-.431	-.492	.022	.012	.071	.085	.045		-.438	-.535	-.088	.022	.073	.122	.050	.690
	.800	-.410	-.443	.037	.007	.070	.052	-.016		-.401	-.490	.016	.024	.073	.105	-.001	.800
	M = 0.940; q = 365 lb/sq ft																
Upper surface	.036	.422	.381	.298	.125	-.272	-1.245	-.728		.400	.323	.225	.106	-.131	-1.086	-1.281	.036
	.084	.339	.287	.191	.026	-.300	-1.171	-.640		.312	.217	.107	-.015	-.214	-.986	-1.235	.084
	.150	.246	.195	.094	-.053	-.339	-1.111	-.634		.223	.118	.000	-.117	-.280	-.938	-1.189	.150
	.260	.169	.109	.026	-.105	-.363	-1.063	-.595		.140	.040	-.078	-.196	-.323	-.904	-1.149	.260
	.350	.104	.057	.029	-.146	-.404	-1.004	-.586		.078	-.008	-.141	-.256	-.373	-.881	-1.140	.350
	.460	.055	.009	-.065	-.171	-.423	-.907	-.562		.033	-.029	-.205	-.309	-.425	-.837	-1.092	.460
	.550	.018	-.022	-.084	-.175	-.346	-.679	-.542		.000	-.051	-.243	-.335	-.466	-.819	-1.081	.550
	.600	-.006	-.033	-.096	-.180	-.258	-.553	-.533		-.016	-.056	-.258	-.355	-.478	-.792	-1.046	.600
	.660	-.025	-.045	-.101	-.174	-.173	-.492	-.525		-.026	-.058	-.234	-.367	-.479	-.667	-.969	.660
	.760	-.058	-.051	-.088	-.143	-.133	-.413	-.509		-.034	-.050	-.009	-.380	-.461	-.613	-.837	.760
.860	-.116	-.062	-.068	-.100	-.101	-.348	-.499		-.072	-.048	-.017	-.100	-.410	-.665	-.758	.860	
.900	-.152	-.070	-.051	-.081	-.078	-.316	-.495		-.104	-.055	-.009	-.010	-.387	-.679	-.745	.900	
Lower surface	.079	-.532	-.517	-.450	-.219	.016	.228	.311		-.680	-.699	-.721	-.600	-.085	.174	.306	.079
	.160	-.506	-.490	-.434	-.143	-.001	.176	.239		-.643	-.665	-.701	-.414	-.088	.114	.224	.160
	.250	-.473	-.474	-.438	-.112	.028	.145	.198		-.612	-.630	-.662	-.249	-.036	.088	.189	.250
	.350	-.458	-.488	-.439	-.075	.038	.123	.154		-.596	-.621	-.607	-.096	-.024	.063	.149	.350
	.450	-.441	-.543	-.395	-.056	.044	.113	.121		-.561	-.638	-.506	-.024	-.004	.049	.123	.450
	.550	-.454	-.592	-.312	-.033	.051	.097	.087		-.524	-.672	-.362	.008	.003	.030	.090	.550
	.650	-.459	-.590	.266	.027	.063	.105	.084		-.503	-.669	-.293	.030	.019	.040	.090	.650
	.690	-.471	-.572	.135	.001	.078	.095	.054		-.496	-.656	-.071	.063	.036	.030	.068	.690
	.800	-.433	-.510	-.011	-.005	.076	.071	.002		-.490	-.567	.105	.080	.032	.007	.021	.800

TABLE III.- PRESSURE COEFFICIENTS AT STAG LATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(e) 80-percent-semispan station - Concluded

[illegible]

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(f) 95-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c	
	M = 0.800; q = 308 lb/sq ft									M = 0.900; q = 350 lb/sq ft								
Upper surface	.080	.291	.268	.203	.106	-.126	-.435	-.347	Upper surface	.304	.278	.209	.095	-.183	-.582	-.410	.080	
	.150	.216	.187	.121	.026	-.166	-.407	-.343		.229	.199	.129	.015	-.227	-.561	-.406	.150	
	.250	.107	.079	.026	-.058	-.194	-.370	-.341		.118	.083	.026	-.073	-.250	-.530	-.400	.250	
	.360	.035	.008	-.029	-.094	-.192	-.331	-.335		.041	.009	-.040	-.127	-.267	-.498	-.397	.360	
	.450	-.027	-.040	-.066	-.114	-.180	-.299	-.331		-.033	-.055	-.084	-.154	-.235	-.467	-.394	.450	
	.560	-.082	-.089	-.088	-.123	-.164	-.274	-.324		-.103	-.109	-.113	-.148	-.190	-.434	-.394	.560	
	.650	-.115	-.115	-.092	-.111	-.144	-.247	-.322		-.144	-.135	-.109	-.126	-.160	-.400	-.390	.650	
	.760																.760	
.800	-.162	-.151	-.087	-.085	-.109	-.216	-.322	-.207	-.181	-.106	-.090	-.116	-.357	-.393	-.800			
Lower surface	.110	-.193	-.226	-.344	-.228	-.009	.184	.231	Lower surface	-.224	-.243	-.341	-.256	.010	.232	.233	.110	
	.190	-.181	-.207	-.325	-.146	-.002	.122	.154		-.215	-.223	-.323	-.155	.003	.164	.152	.190	
	.260																.260	
	.360	-.176	-.192	-.314	-.081	.005	.050	.056		-.219	-.211	-.314	-.087	-.001	.082	.049	.360	
	.450	-.178	-.180	-.303	-.046	.019	.029	.012		-.225	-.199	-.307	-.045	.012	.045	-.002	.450	
	.560	-.175	-.167	-.281	-.009	.039	.020	-.015		-.220	-.189	-.293	.000	.037	.028	-.037	.560	
	.600	-.174	-.162	-.267	.007	.049	.011	-.028		-.219	-.184	-.283	.018	.041	.017	-.058	.600	
	.710	-.172	-.153	-.219	.033	.062	.005	-.052		-.219	-.177	-.244	.045	.058	.005	-.081	.710	
	M = 0.940; q = 365 lb/sq ft									M = 0.960; q = 380 lb/sq ft								
Upper surface	.080	.313	.294	.218	.086	-.249	-.604	-.460	Upper surface	.312	.282	.183	.036	-.222	-.984	-.181	.080	
	.150	.236	.217	.138	.009	-.259	-.570	-.458		.238	.206	.124	-.060	-.317	-.933	-.146	.150	
	.250	.128	.108	.028	-.081	-.238	-.526	-.449		.132	.093	.040	-.144	-.350	-.927	-.134	.250	
	.360	.043	.027	-.042	-.150	-.261	-.485	-.447		.053	.017	-.022	-.202	-.382	-.919	-.121	.360	
	.450	-.030	-.034	-.099	-.206	-.301	-.455	-.443		-.027	-.053	-.083	-.271	-.427	-.909	-.105	.450	
	.560	-.113	-.085	-.128	-.166	-.237	-.430	-.440		-.115	-.123	-.125	-.303	-.487	-.875	-.085	.560	
	.650	-.155	-.115	-.119	-.127	-.140	-.420	-.441		-.167	-.149	-.099	-.036	-.502	-.855	-.052	.650	
	.760																.760	
.800	-.231	-.167	-.112	-.094	-.119	-.407	-.443	-.244	-.209	-.089	-.017	-.387	-.793	-.946	.800			
Lower surface	.110	-.289	-.289	-.341	-.268	.017	.192	.228	Lower surface	-.378	-.305	-.327	-.288	-.085	.129	.235	.110	
	.190	-.274	-.275	-.315	-.177	.010	.127	.148		-.364	-.285	-.293	-.181	-.065	.077	.158	.190	
	.260																.260	
	.360	-.269	-.272	-.306	-.108	.001	.041	.047		-.357	-.306	-.261	-.113	-.056	.005	.066	.360	
	.450	-.262	-.266	-.298	-.070	.009	-.005	-.010		-.342	-.321	-.249	-.061	-.048	-.043	.012	.450	
	.560	-.255	-.270	-.300	-.018	.035	-.033	-.052		-.335	-.324	-.241	.002	-.007	-.086	-.045	.560	
	.600	-.247	-.275	-.293	.002	.041	-.044	-.076		-.331	-.319	-.236	.021	.006	-.106	-.075	.600	
	.710	-.240	-.284	-.273	.031	.060	-.060	-.106		-.317	-.306	-.222	.059	.029	-.123	-.120	.710	

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$		
		M = 1.050; q = 597 lb/sq ft									
Upper surface	.080	.320	.256	.181	.072	-.124	-.824	-1.087			
	.150	.253	.184	.098	-.026	-.226	-.788	-1.041			
	.250	.148	.075	-.006	-.108	-.267	-.786	-1.030			
	.360	.074	.001	-.062	-.163	-.300	-.778	-1.012			
	.450	.002	-.079	-.131	-.220	-.345	-.779	-1.008			
	.560	-.080	-.187	-.239	-.315	-.414	-.778	-.986			
	.650	-.139	-.246	-.318	-.385	-.452	-.763	-.965			
	.760										
	.800	-.221	-.279	-.420	-.472	-.502	-.757	-.956			
Lower surface	.110	-.521	-.508	-.755	-.629	-.183	.150	.280			
	.190	-.490	-.477	-.716	-.458	-.165	.108	.215			
	.260										
	.360	-.460	-.453	-.656	-.326	-.131	.046	.126			
	.450	-.453	-.433	-.611	-.259	-.103	.007	.079			
	.560	-.438	-.410	-.583	-.175	-.056	-.035	.024			
	.600	-.430	-.399	-.558	-.130	-.036	-.005	.005			
	.710	-.410	-.371	-.475	-.075	-.024	-.081	-.049			
	M = 1.200; q = 457 lb/sq ft										
Upper surface	.080	.359	.309	.250	.160	.040	-.431	-.698			
	.150	.294	.238	.165	.063	-.063	-.424	-.675			
	.250	.207	.143	.083	-.008	-.109	-.436	-.669			
	.360	.156	.094	.029	-.056	-.146	-.444	-.665			
	.450	.099	.048	-.012	-.097	-.183	-.456	-.665			
	.560	.014	-.029	-.081	-.159	-.231	-.468	-.660			
	.650	-.066	-.103	-.148	-.222	-.285	-.468	-.640			
	.760										
	.800	-.168	-.214	-.255	-.318	-.357	-.488	-.640			
Lower surface	.110	-.701	-.754	-.619	-.568	-.249	.196	.367			.110
	.190	-.677	-.713	-.594	-.570	-.199	.164	.317			.190
	.260										.260
	.360	-.692	-.708	-.602	-.347	-.149	.135	.262			.360
	.450	-.650	-.681	-.558	-.287	-.133	.131	.235			.450
	.560	-.623	-.662	-.506	-.218	-.085	.124	.196			.560
	.600	-.588	-.651	-.434	-.174	-.031	.109	.170			.600
	.710	-.460	-.586	-.256	-.062	.086	.087	.127			.710

		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c	
		M = 1.125; q = 421 lb/sq ft							
	.348	.289	.223	.133	-.015	-.602	-.840	.080	
	.286	.223	.141	.031	-.118	-.584	-.806	.150	
	.190	.120	.055	-.041	-.165	-.584	-.800	.250	
	.123	.070	-.002	-.090	-.203	-.585	-.791	.360	
	.051	.008	-.057	-.142	-.243	-.591	-.791	.450	
	-.046	-.091	-.143	-.218	-.304	-.595	-.787	.560	
	-.114	-.173	-.218	-.283	-.358	-.589	-.769	.650	
								.760	
								.806	
	-.172	-.278	-.329	-.379	-.420	-.607	-.766		
	-.626	-.796	-.757	-.671	-.235	.196	.340	.110	
	-.594	-.774	-.754	-.522	-.183	.160	.284	.190	
								.260	
	-.560	-.722	-.681	-.336	-.138	.119	.216	.360	
	-.529	-.642	-.516	-.280	-.103	.098	.176	.450	
	-.504	-.579	-.351	-.186	-.009	.064	.128	.560	
	-.494	-.557	-.285	-.128	.037	.044	.101	.600	
-.481	-.514	-.170	-.054	.072	.018	.059	.710		

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY

(a) 12-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$			$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c		
		M = 0.800; q = 618 lb/sq ft									M = 0.900; q = 701 lb/sq ft										
Upper surface	.000	-.125	.143	.362	.500	.550	.531	.391			.051	.252	.419	.528	.578	.591	.522	.000			
	.025	.395	.289	.178	.041	-.123	-.525	-1.378			.402	.301	.190	.064	-.077	-.491	-1.138	.025			
	.072	.252	.159	.067	-.036	-.131	-.351	-.563			.263	.171	.081	-.012	-.093	-.271	-.499	.072			
	.150	.129	.050	-.022	-.105	-.194	-.384	-.577			.130	.053	-.022	-.096	-.174	-.343	-.481	.150			
	.250	.064	-.006	-.071	-.141	-.215	-.378	-.532			.062	-.007	-.077	-.145	-.212	-.344	-.483	.250			
	.350	.012	-.051	-.111	-.176	-.243	-.395	-.551			.004	-.061	-.127	-.194	-.256	-.397	-.504	.350			
	.450	-.020	-.078	-.132	-.192	-.250	-.384	-.508			-.031	-.093	-.155	-.221	-.281	-.422	-.534	.450			
	.550	-.062	-.117	-.165	-.219	-.274	-.393	-.469			-.087	-.149	-.215	-.290	-.362	-.486	-.624	.550			
	.650	-.047	-.094	-.133	-.179	-.224	-.312	-.364			-.069	-.123	-.176	-.240	-.348	-.484	-.611	.650			
Lower surface	.750	-.034	-.071	-.102	-.138	-.171	-.231	-.284			-.052	-.095	-.136	-.184	-.233	-.347	-.483	.750			
	.840	-.024	-.056	-.078	-.102	-.127	-.162	-.209			-.042	-.076	-.106	-.136	-.158	-.237	-.383	.840			
	.920	-.011	-.032	-.045	-.056	-.069	-.094	-.126			-.022	-.046	-.062	-.076	-.085	-.137	-.184	.920			
	.031	-.371	-.223	-.088	.042	.158	.366	.550			-.310	-.183	-.061	.054	.167	.372	.556	.031			
	.072	-.307	-.197	-.088	.009	.104	.280	.448			-.266	-.166	-.071	.017	.109	.285	.454	.072			
	.150	-.267	-.178	-.089	-.008	.067	.218	.361			-.250	-.166	-.085	-.009	.068	.223	.368	.150			
	.250	-.260	-.185	-.105	-.034	.031	.165	.291			-.267	-.192	-.114	-.045	.025	.165	.293	.250			
	.350																	.350			
	.450	-.271	-.206	-.141	-.081	-.029	.082	.183			-.300	-.237	-.171	-.108	-.046	.073	.180	.450			
Upper surface	.550	-.254	-.198	-.138	-.083	-.034	.064	.155			-.337	-.270	-.187	-.119	-.058	.054	.149	.550			
	.650	-.226	-.181	-.129	-.081	-.039	.045	.123			-.362	-.269	-.178	-.118	-.065	.034	.114	.650			
	.750	-.161	-.125	-.084	-.046	-.012	.059	.120			-.307	-.179	-.120	-.075	-.030	.048	.112	.750			
	.850	-.101	-.075	-.045	-.015	.010	.067	.110			-.131	-.097	-.064	-.033	.000	.061	.103	.850			
	.900	-.067	-.047	-.020	.004	.026	.077	.108			-.079	-.060	-.034	-.009	.021	.072	.102	.900			
	M = 0.940; q = 730 lb/sq ft									M = 0.980; q = 758 lb/sq ft											
	.000	.120	.296	.449	.543	.593	.611	.565			.183	.343	.480	.572	.619	.641	.614	.000			
	.025	.411	.306	.201	.084	-.050	-.432	-1.013			.431	.331	.228	.119	-.011	-.346	-.921	.025			
	.072	.272	.180	.094	.008	-.069	-.227	-.450			.294	.207	.124	.045	-.030	-.178	-.390	.072			
	.150	.138	.059	-.013	-.084	-.152	-.301	-.435			.158	.082	.015	-.048	-.122	-.255	-.379	.150			
	.250	.064	-.009	-.075	-.139	-.193	-.319	-.435			.081	.013	-.049	-.102	-.159	-.274	-.374	.250			
.350	.004	-.066	-.128	-.185	-.255	-.362	-.468			.017	-.047	-.102	-.164	-.218	-.316	-.416	.350				
.450	-.036	-.103	-.163	-.220	-.275	-.396	-.500			-.029	-.087	-.140	-.193	-.251	-.352	-.444	.450				
.550	-.102	-.177	-.249	-.305	-.359	-.474	-.582			-.113	-.178	-.228	-.276	-.332	-.435	-.526	.550				
.650	-.085	-.150	-.241	-.312	-.361	-.470	-.573			-.101	-.185	-.235	-.284	-.343	-.428	-.521	.650				
.750	-.069	-.120	-.175	-.234	-.283	-.387	-.486			-.094	-.174	-.228	-.279	-.344	-.436	-.529	.750				
Lower surface	.840	-.059	-.096	-.128	-.172	-.222	-.326	-.423			-.106	-.177	-.234	-.284	-.346	-.462	-.550	.840			
	.920	-.043	-.060	-.071	-.083	-.100	-.135	-.165			-.105	-.165	-.228	-.284	-.348	-.435	-.534	.920			
	.031	-.248	-.160	-.041	.065	.172	.373	.563			-.216	-.123	-.008	.095	.197	.393	.583	.031			
	.072	-.231	-.148	-.056	.024	.115	.286	.460			-.183	-.106	-.025	.053	.139	.307	.482	.072			
	.150	-.232	-.154	-.075	-.004	.067	.224	.374			-.200	-.121	-.050	.020	.091	.243	.396	.150			
	.250	-.243	-.189	-.112	-.047	.022	.162	.298			-.211	-.152	-.089	-.029	.037	.177	.319	.250			
	.350																	.350			
	.450	-.291	-.231	-.172	-.122	-.062	.062	.181			-.268	-.204	-.148	-.099	-.051	.071	.197	.450			
	.550	-.324	-.271	-.216	-.151	-.083	.038	.149			-.302	-.250	-.192	-.147	-.090	.039	.162	.550			
	.650	-.347	-.309	-.248	-.183	-.094	.013	.109			-.327	-.284	-.228	-.183	-.130	.003	.122	.650			
	.750	-.358	-.313	-.252	-.183	-.055	.023	.105			-.336	-.292	-.241	-.196	-.141	.010	.115	.750			
.850	-.351	-.289	-.227	-.153	-.016	.034	.094			-.338	-.287	-.235	-.184	-.117	.021	.105	.850				
.900	-.306	-.217	-.153	-.085	.006	.043	.090			-.329	-.274	-.220	-.166	-.089	.029	.100	.900				

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - C included

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$			$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c		
		M = 1.030; q = 794 lb/sq ft																			
Upper surface		.000	.261	.407	.530	.612	.662	.694	.657			.341	.454	.528	.596	.634	.681	.724	.000		
		.025	.479	.374	.272	.163	.044	-.288	-.793			.411	.306	.215	.079	-.045	-.367	-.647	.025		
		.072	.344	.254	.174	.095	.032	-.095	-.317			.311	.224	.165	.080	.009	-.162	-.345	.072		
		.150	.212	.133	.066	.005	-.068	-.190	-.294			.199	.133	.073	-.006	-.071	-.165	-.259	.150		
		.250	.137	.065	.003	-.049	-.095	-.196	-.296			.135	.074	.029	-.030	-.089	-.172	-.244	.250		
		.350	.074	.009	-.055	-.109	-.155	-.237	-.335			.077	.015	-.029	-.083	-.136	-.212	-.276	.350		
		.450	.031	-.025	-.084	-.141	-.189	-.270	-.364			.044	-.017	-.060	-.118	-.165	-.235	-.297	.450		
		.550	-.059	-.115	-.172	-.223	-.265	-.352	-.444			-.039	-.096	-.137	-.187	-.231	-.303	-.367	.550		
		.650	-.063	-.120	-.174	-.228	-.273	-.347	-.441			-.035	-.091	-.133	-.185	-.233	-.300	-.363	.650		
		.750	-.054	-.121	-.181	-.232	-.276	-.358	-.448			-.045	-.097	-.140	-.193	-.239	-.308	-.363	.750		
Lower surface		.840	-.070	-.131	-.199	-.254	-.299	-.385	-.472			-.068	-.124	-.164	-.217	-.259	-.320	-.383	.840		
		.920	-.060	-.113	-.176	-.229	-.273	-.362	-.460			-.040	-.098	-.138	-.188	-.231	-.304	-.375	.920		
		.031	-.138	-.059	.045	.142	.246	.444	.622			-.167	-.061	.007	.112	.203	.391	.594	.031		
		.072	-.102	-.034	.028	.102	.188	.359	.523			-.098	-.025	.029	.098	.165	.321	.505	.072		
		.150	-.131	-.065	-.003	.067	.139	.297	.439			-.115	-.047	.000	.075	.144	.283	.438	.150		
		.250	-.137	-.095	-.040	.018	.088	.234	.365			-.117	-.062	-.019	.048	.100	.227	.371	.250		
		.350																	.350		
		.450	-.194	-.148	-.099	-.046	.009	.127	.247			-.162	-.105	-.066	-.008	.044	.153	.269	.450		
		.550	-.226	-.184	-.138	-.088	-.031	.091	.211			-.194	-.138	-.097	-.039	.009	.114	.237	.550		
		.650	-.256	-.218	-.174	-.124	-.067	.051	.171			-.218	-.164	-.134	-.078	-.031	.081	.202	.650		
Upper surface		.750	-.262	-.223	-.182	-.137	-.078	.058	.165			-.219	-.164	-.131	-.073	-.034	.077	.206	.750		
		.850	-.268	-.218	-.178	-.130	-.065	.074	.159			-.207	-.154	-.122	-.073	-.031	.088	.217	.850		
		.900	-.259	-.207	-.165	-.115	-.047	.087	.159			-.191	-.144	-.110	-.061	-.013	.111	.227	.900		
Lower surface		.000	.385	.473	.549	.603	.647	.695	.735										.000		
		.025	.397	.302	.199	.089	-.013	-.321	-.580										.025		
		.072	.310	.239	.163	.076	.009	-.175	-.341										.072		
		.150	.189	.119	.057	.007	-.048	-.142	-.249										.150		
		.250	.163	.107	.050	-.014	-.083	-.149	-.219										.250		
		.350	.112	.058	.004	-.043	-.093	-.181	-.249										.350		
		.450	.075	.027	-.023	-.074	-.120	-.197	-.263										.450		
		.550	-.003	-.053	-.100	-.148	-.190	-.262	-.318										.550		
		.650	-.002	-.054	-.106	-.149	-.188	-.255	-.323										.650		
		.750	-.016	-.057	-.100	-.142	-.181	-.252	-.329										.750		
Upper surface		.840	-.046	-.089	-.132	-.175	-.212	-.284	-.347										.840		
		.920	-.029	-.071	-.113	-.153	-.192	-.270	-.340										.920		
Lower surface		.031	-.142	-.069	.015	.097	.185	.373	.567										.031		
		.072	-.084	-.024	.036	.096	.163	.304	.484										.072		
		.150	-.102	-.050	.009	.052	.113	.254	.436										.150		
		.250	-.101	-.056	-.005	.046	.109	.230	.382										.250		
		.350																	.350		
		.450	-.129	-.082	-.033	.009	.061	.168	.297										.450		
		.550	-.156	-.116	-.070	.023	.027	.137	.259										.550		
		.650	-.186	-.145	-.100	.057	.003	.104	.215										.650		
		.750	-.184	-.137	-.092	.047	.004	.083	.199										.750		
		.850	-.165	-.144	-.102	.060	.020	.068	.193										.850		
	.900	-.159	-.127	-.097	.059	.016	.085	.215										.900			

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$			$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c
		M = 0.800; q = 618 lb/sq ft								M = 0.900; q = 701 lb/sq ft									
Upper surface		.000	-.194	.027	.229	.396	.373	-.144	-.835			-.084	.089	.265	.394	.405	.066	-.459	.000
		.027	.338	.242	.132	-.039	-.247	-.798	1.266			.330	.241	.126	-.025	-.204	-.855	1.110	.027
		.075	.193	.099	.001	-.130	-.273	-.586	1.064			.186	.092	-.009	-.131	-.267	-.544	-.945	.075
		.140	.114	.030	-.060	-.167	-.287	-.538	-.936			.105	.019	-.073	-.178	-.299	-.538	-.788	.140
		.250	.035	-.038	-.111	-.194	-.282	-.475	-.813			.024	-.053	-.130	-.213	-.287	-.482	-.707	.250
		.350	-.028	-.097	-.163	-.239	-.317	-.499	-.720			-.051	-.128	-.207	-.294	-.370	-.500	-.695	.350
		.450	-.047	-.109	-.165	-.229	-.296	-.434	-.566			-.071	-.140	-.211	-.285	-.392	-.545	-.683	.450
		.550	-.044	-.099	-.144	-.199	-.253	-.358	-.473			-.067	-.128	-.187	-.260	-.379	-.540	-.670	.550
		.650	-.043	-.089	-.127	-.167	-.212	-.283	-.396			-.066	-.118	-.168	-.225	-.271	-.358	-.637	.650
		.750	-.024	-.059	-.086	-.117	-.148	-.194	-.298			-.042	-.082	-.116	-.151	-.181	-.463	-.553	.750
Lower surface		.850	.011	-.015	-.031	-.050	-.067	-.095	-.180			-.002	-.028	-.047	-.067	-.078	-.127	-.252	.850
		.923	.030	.014	.007	-.003	-.011	-.024	-.095			.027	.008	.003	-.005	-.009	-.030	-.132	.923
		.026	-.765	-.562	-.287	-.077	.096	.335	.465			-.769	-.573	-.291	-.089	.078	.325	.465	.026
		.074	-.753	-.464	-.163	-.036	.071	.252	.387			-.778	-.401	-.168	-.045	.057	.244	.384	.074
		.150	-.571	-.283	-.141	-.040	.046	.194	.317			-.582	-.275	-.153	-.056	.034	.187	.315	.150
		.250	-.272	-.216	-.128	-.052	.017	.147	.257			-.234	-.238	-.149	-.073	.002	.138	.251	.250
		.350	-.256	-.211	-.139	-.072	-.012	.106	.210			-.295	-.266	-.172	-.101	-.031	.095	.202	.350
		.450	-.248	-.202	-.141	-.081	-.027	.078	.169			-.331	-.279	-.193	-.120	-.053	.063	.160	.450
		.550	-.204	-.166	-.114	-.065	-.019	.072	.149			-.342	-.255	-.159	-.098	-.042	.059	.139	.550
		.650	-.165	-.134	-.090	-.049	-.012	.064	.128			-.323	-.183	-.124	-.077	-.032	.053	.117	.650
Upper surface		.750	-.102	-.078	-.046	-.015	.014	.076	.121			-.127	-.105	-.067	-.034	.005	.070	.111	.750
		.850	-.054	-.041	-.016	.005	.024	.068	.093			-.057	-.052	-.028	-.005	.020	.062	.078	.850
		.900	-.023	-.013	.005	.021	.035	.068	.081			-.021	-.019	-.000	.014	.032	.063	.063	.900
		.000	-.029	.121	.282	.398	.418	.144	-.322			.029	.163	.306	.415	.441	.212	-.211	.000
		.027	.331	.239	.128	-.011	-.175	-.750	1.245			.344	.253	.150	.026	-.133	-.658	1.161	.027
		.075	.184	.090	-.010	-.125	-.246	-.485	1.069			.196	.107	.011	-.097	-.216	-.415	1.052	.075
		.140	.103	.016	-.075	-.177	-.283	-.496	-.638			.114	.035	-.054	-.142	-.245	-.441	-.553	.140
		.250	.019	-.061	-.134	-.202	-.289	-.468	-.600			.027	-.044	-.107	-.181	-.266	-.421	-.526	.250
		.350	-.064	-.149	-.227	-.291	-.347	-.475	-.609			-.067	-.140	-.199	-.254	-.308	-.430	-.538	.350
		.450	-.088	-.167	-.247	-.325	-.391	-.524	-.646			-.099	-.167	-.236	-.299	-.365	-.483	-.585	.450
Lower surface		.550	-.084	-.152	-.248	-.340	-.397	-.520	-.631			-.089	-.194	-.255	-.311	-.370	-.479	-.578	.550
		.650	-.088	-.150	-.215	-.334	-.407	-.538	-.610			-.124	-.201	-.263	-.328	-.393	-.504	-.603	.650
		.750	-.062	-.103	-.141	-.262	-.400	-.521	-.596			-.117	-.214	-.271	-.329	-.385	-.486	-.583	.750
		.850	-.018	-.037	-.049	-.056	-.206	-.449	-.532			-.078	-.161	-.232	-.294	-.359	-.464	-.567	.850
		.923	.011	.007	.004	.007	-.021	-.188	-.287			-.088	-.135	-.193	-.237	-.278	-.377	-.500	.923
		.026	-.717	-.561	-.286	-.094	.068	.315	.469			-.653	-.536	-.273	-.080	.080	.326	.487	.026
		.074	-.719	-.376	-.164	-.046	.049	.238	.387			-.647	-.320	-.162	-.032	.062	.249	.405	.074
		.150	-.536	-.275	-.155	-.060	.025	.178	.317			-.485	-.239	-.139	-.046	.038	.190	.334	.150
		.250	-.246	-.224	-.151	-.084	-.012	.127	.253			-.228	-.199	-.121	-.065	-.002	.136	.270	.250
		.350	-.295	-.261	-.195	-.125	-.052	.080	.200			-.272	-.240	-.169	-.118	-.051	.083	.215	.350
Lower surface		.450	-.316	-.287	-.218	-.159	-.082	.043	.157			-.295	-.260	-.196	-.146	-.096	.039	.168	.450
		.550	-.331	-.303	-.233	-.137	-.070	.036	.132			-.316	-.275	-.216	-.168	-.110	.026	.143	.550
		.650	-.365	-.326	-.218	-.104	-.056	.026	.107			-.349	-.306	-.250	-.190	-.134	.012	.117	.650
		.750	-.338	-.275	-.080	-.044	-.014	.041	.100			-.329	-.283	-.223	-.168	-.106	.023	.108	.750
		.850	-.294	-.097	-.023	-.010	.006	.023	.057			-.329	-.283	-.227	-.177	-.103	.002	.063	.850
		.900	-.117	-.025	.005	.014	.022	.015	.034			-.323	-.270	-.217	-.170	-.084	-.021	.033	.900

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$		
M = 1.030; q = 794 lb/sq ft											
Upper surface		.000	.110	.229	.351	.454	.488	.284	-.114		
		.027	.391	.296	.197	.077	-.069	-.556	-1.019		
		.075	.246	.153	.059	.039	-.149	-.321	-.916		
		.140	.168	.084	-.004	-.094	-.183	-.352	-.487		
		.250	.082	.016	-.056	-.134	-.203	-.336	-.451		
		.350	-.013	-.076	-.138	-.188	-.239	-.345	-.460		
		.450	-.042	-.110	-.180	-.251	-.297	-.402	-.506		
		.550	-.067	-.132	-.195	-.254	-.300	-.396	-.499		
		.650	-.078	-.138	-.208	-.274	-.325	-.426	-.521		
		.750	-.091	-.152	-.214	-.270	-.313	-.405	-.504		
Lower surface		.850	-.098	-.155	-.217	-.265	-.292	-.389	-.490		
		.923	-.053	-.115	-.179	-.245	-.292	-.389	-.490		
			-.060	-.106	-.157	-.213	-.251	-.329	-.445		
		.026	-.539	-.461	-.204	-.027	.127	.377	.527		
		.074	-.517	-.245	-.099	.012	.110	.302	.447		
		.150	-.431	-.180	-.091	.002	.090	.244	.377		
		.250	-.177	-.138	-.072	.008	.055	.189	.314		
		.350	-.204	.179	-.119	-.060	.002	.136	.262		
		.450	-.225	-.194	-.140	-.088	-.029	.090	.216		
		.550	-.243	-.211	-.159	-.108	-.048	.076	.193		
Upper surface		.650	-.274	-.237	-.193	-.139	-.076	.061	.168		
		.750	-.259	-.216	-.171	-.114	-.048	.077	.162		
		.850	-.261	-.215	-.173	-.121	-.057	.057	.122		
		.900	-.262	-.210	-.170	-.119	-.057	.044	.097		
M = 1.200; q = 873 lb/sq ft											
Lower surface		.000	.256	.351	.439	.502	.519	.435	.176		
		.027	.395	.326	.229	.107	-.014	-.396	-.695		
		.075	.253	.174	.091	.001	-.087	-.324	-.655		
		.140	.178	.114	.044	-.038	-.119	-.262	-.601		
		.250	.113	.051	-.013	-.077	-.135	-.254	-.314		
		.350	.050	-.001	-.048	-.101	-.157	-.265	-.331		
		.450	-.003	-.057	-.116	-.174	-.225	-.315	-.383		
		.550	-.015	-.071	-.125	-.179	-.225	-.302	-.371		
		.650	-.044	-.098	-.152	-.200	-.242	-.326	-.407		
		.750	-.038	-.085	-.129	-.177	-.222	-.302	-.382		
Upper surface		.850	-.024	-.080	-.131	-.174	-.215	-.297	-.368		
		.923	-.013	-.060	-.108	-.157	-.201	-.279	-.347		
		.026	-.397	-.367	-.167	.001	.134	.350	.533		
		.074	-.324	-.165	-.060	.031	.117	.286	.459		

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c
M = 0.900; q = 618 lb/sq ft									M = 0.900; q = 701 lb/sq ft								
Upper surface	.000	.169	.238	.318	.348	-.051	-1.127	-1.341	Upper surface	.206	.261	.327	.354	.043	-1.120	-1.418	.000
	.030	.393	.323	.222	.028	-.266	-1.068	-1.345		.378	.306	.201	.025	-.235	-1.277	-1.422	.030
	.078	.232	.143	.038	-.109	-.292	-.853	-1.315		.212	.122	.012	-.125	-.308	-.761	-1.382	.078
	.150	.146	.064	-.027	-.148	-.277	-.688	-1.319		.125	.040	-.059	-.183	-.301	-.617	-1.237	.150
	.260	.074	.000	-.075	-.174	-.278	-.539	-1.303		.055	-.024	-.113	-.222	-.326	-.589	-1.133	.260
	.350	.027	-.040	-.109	-.189	-.279	-.470	-1.158		.006	-.067	-.147	-.245	-.378	-.578	-1.019	.350
	.450	-.004	-.065	-.122	-.192	-.268	-.409	-.880		-.026	-.091	-.162	-.249	-.385	-.590	-.852	.450
	.550	-.020	-.074	-.123	-.179	-.241	-.344	-.637		-.040	-.099	-.158	-.224	-.268	-.418	-.697	.550
	.660	-.025	-.069	-.107	-.150	-.199	-.270	-.438		-.044	-.091	-.138	-.191	-.240	-.372	-.597	.660
	.750	-.021	-.056	-.085	-.117	-.152	-.197	-.297		-.037	-.074	-.107	-.143	-.173	-.237	-.440	.750
Lower surface	.860	.012	-.014	-.030	-.050	-.070	-.100	-.174	Lower surface	.002	-.024	-.042	-.061	-.076	-.075	-.317	.860
	.930	.023	.003	-.004	-.013	-.025	-.042	-.115		.015	-.001	-.009	-.017	-.022	-.013	-.230	.930
	.032	-.892	-.725	-.395	-.146	.094	.339	.448		-.966	-.918	-.399	-.181	.057	.315	.435	.032
	.083	-.751	-.516	-.220	-.081	.060	.251	.375		-.729	-.502	-.237	-.103	.035	.239	.359	.083
	.160	-.746	-.408	-.190	-.066	.034	.191	.309		-.706	-.402	-.220	-.097	.009	.170	.292	.160
	.240	-.732	-.334	-.175	-.077	.001	.135	.241		-.734	-.393	-.226	-.117	-.028	.115	.225	.240
	.360	-.449	-.252	-.156	-.079	-.016	.099	.189		-.594	-.352	-.210	-.119	-.043	.080	.174	.360
	.450	-.234	-.195	-.124	-.063	-.008	.089	.164		-.456	-.272	-.166	-.095	-.031	.072	.149	.450
	.550	-.125	-.131	-.077	-.028	.015	.095	.154		-.262	-.163	-.100	-.047	.003	.084	.143	.550
	.660	-.061	-.072	-.030	.010	.043	.108	.150		-.106	-.085	-.041	-.002	.037	.102	.140	.660
M = 0.940; q = 750 lb/sq ft									M = 0.980; q = 758 lb/sq ft								
Upper surface	.000	.229	.275	.331	.362	.107	-1.003	-1.321	Upper surface	.263	.301	.349	.383	.167	-.856	-1.235	.000
	.030	.372	.296	.191	.033	-.203	-1.157	-1.373		.373	.302	.206	.064	-.148	-1.029	-1.319	.030
	.078	.201	.108	.001	-.126	-.298	-1.752	-1.329		.200	.113	.018	-.098	-.254	-.659	-1.227	.078
	.150	.112	.024	-.077	-.189	-.294	-1.541	-1.225		.108	.028	-.062	-.172	-.278	-.482	-1.157	.150
	.260	.039	-.049	-.146	-.230	-.320	-1.549	-.842		.027	-.056	-.118	-.204	-.310	-.499	-.804	.260
	.350	-.011	-.095	-.201	-.292	-.367	-1.564	-.754		-.030	-.122	-.196	-.261	-.343	-.512	-.685	.350
	.450	-.043	-.121	-.209	-.334	-.406	-1.568	-.703		-.075	-.165	-.243	-.312	-.379	-.521	-.638	.450
	.550	-.058	-.124	-.182	-.343	-.438	-1.608	-.680		-.090	-.180	-.261	-.346	-.436	-.565	-.655	.550
	.660	-.062	-.113	-.166	-.274	-.426	-1.585	-.649		-.123	-.188	-.278	-.343	-.416	-.550	-.649	.660
	.750	-.052	-.087	-.116	-.121	-.421	-1.592	-.642		-.121	-.214	-.296	-.366	-.434	-.559	-.663	.750
Lower surface	.860	-.004	-.026	-.042	-.049	-.071	-.283	-.446	Lower surface	-.083	-.166	-.247	-.333	-.404	-.526	-.634	.860
	.930	.012	.003	-.006	-.009	.005	-.122	-.316		-.052	-.054	-.099	-.171	-.244	-.381	-.514	.930
	.032	-.989	-.958	-.404	-.204	.028	.296	.436		-.900	-.970	-.398	-.209	.025	.295	.449	.032
	.083	-.673	-.493	-.237	-.119	.013	.223	.354		-.587	-.456	-.222	-.112	.013	.221	.364	.083
	.160	-.616	-.375	-.231	-.119	-.016	.151	.285		-.549	-.345	-.206	-.112	-.021	.150	.295	.160
	.240	-.600	-.371	-.258	-.158	-.059	.093	.216		-.491	-.339	-.229	-.154	-.080	.085	.221	.240
	.360	-.548	-.377	-.283	-.166	-.078	.053	.166		-.504	-.351	-.265	-.199	-.128	.038	.167	.360
	.450	-.482	-.382	-.276	-.128	-.060	.044	.138		-.483	-.359	-.283	-.219	-.147	.025	.141	.450
	.550	-.432	-.362	-.134	-.061	-.018	.057	.132		-.443	-.345	-.275	-.210	-.134	.038	.133	.550
	.660	-.374	-.241	-.033	-.007	.023	.072	.129		-.395	-.312	-.239	-.165	-.052	.050	.128	.660

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan statio - Concluded

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c
M = 1.050; q = 794 lb/sq ft									M = 1.125; q = 842 lb/sq ft								
Upper surface	.000	.320	.355	.391	.425	.233	-.718	+1.081	Upper surface	.366	.399	.430	.424	.269	-.513	-.844	.000
	.030	.417	.347	.249	.117	-.078	-.886	+1.164		.414	.338	.274	.141	-.103	-.696	-.941	.030
	.078	.247	.163	.062	-.043	-.183	-.598	+1.080		.245	.156	.090	-.009	-.158	-.571	-.862	.078
	.150	.159	.085	-.008	-.110	-.207	-.407	+1.018		.171	.088	.018	-.080	-.155	-.584	-.813	.150
	.260	.074	.010	-.067	-.153	-.235	-.417	.737		.101	.029	-.038	-.112	-.217	-.561	-.766	.260
	.350	.009	-.062	-.129	-.202	-.274	-.423	-.593		.033	-.033	.085	-.176	-.252	-.576	-.549	.350
	.450	-.034	-.107	-.180	-.246	-.310	-.435	-.553		-.015	-.078	-.125	-.197	-.268	-.397	-.495	.450
	.550	-.046	-.124	-.207	-.290	-.363	-.479	-.570		-.036	-.118	-.179	-.248	-.313	-.405	-.486	.550
	.660	-.076	-.144	-.213	-.282	-.345	-.469	-.568		-.055	-.121	-.171	-.240	-.302	-.400	-.480	.660
	.750	-.099	-.162	-.234	-.301	-.362	-.477	-.582		-.080	-.142	-.193	-.257	-.319	-.418	-.490	.750
Lower surface	.860	-.076	-.129	-.205	-.279	-.337	-.452	-.557	Lower surface	-.053	-.128	-.175	-.242	-.302	-.391	-.467	.860
	.930	-.079	-.117	-.166	-.229	-.283	-.358	-.500		-.044	-.116	-.167	-.230	-.285	-.346	-.447	.930
	.032	-.839	-.781	-.395	-.138	.077	.340	.491		-.801	-.716	-.557	-.082	.080	.352	.501	.032
	.083	-.499	-.386	-.171	-.053	.072	.271	.407		-.536	-.287	-.141	-.026	.105	.292	.425	.083
	.160	-.470	-.282	-.153	-.050	.039	.200	.342		-.397	-.204	-.114	.000	.081	.227	.363	.160
	.240	-.414	-.270	-.167	-.091	-.016	.133	.268		-.336	-.208	-.123	-.031	.032	.155	.293	.240
	.360	-.429	-.278	-.203	-.138	-.065	.083	.216		-.317	-.205	-.144	-.076	-.025	.104	.244	.360
	.450	-.410	-.288	-.222	-.159	-.084	.072	.189		-.301	-.215	-.170	-.105	-.048	.089	.228	.450
	.550	-.367	-.275	-.215	-.152	-.078	.089	.185		-.282	-.204	-.159	-.094	-.039	.092	.238	.550
	.660	-.323	-.245	-.184	-.116	-.033	.106	.183		-.256	-.185	-.143	-.072	-.015	.121	.249	.660
Upper surface	.750	-.267	-.190	-.129	-.057	.114	.172	.172	Upper surface	-.209	-.143	-.097	-.027	.037	.174	.249	.750
	.840	-.236	-.157	-.096	-.034	.023	.083	.128		-.171	-.104	-.058	.010	.064	.160	.215	.840
	.910	-.193	-.124	-.081	-.039	-.000	.034	.068		-.153	-.087	-.050	.007	.049	.120	.162	.910
	.000	.424	.439	.472	.475	.340	-.323	-.696									.000
	.030	.451	.391	.317	.174	-.024	-.539	-.798									.030
	.078	.279	.208	.136	.054	-.105	-.437	-.732									.078
	.150	.193	.128	.050	-.028	-.103	-.285	-.699									.150
	.260	.128	.057	-.001	-.082	-.157	-.316	-.674									.260
	.350	.066	.009	-.089	-.128	-.190	-.317	-.642									.350
	.450	.021	-.031	-.091	-.156	-.226	-.349	-.621									.450
Lower surface	.550	-.025	-.089	-.145	-.207	-.259	-.367	-.637									.550
	.660	-.036	-.091	-.149	-.206	-.256	-.360	-.629									.660
	.750	-.064	-.116	-.169	-.225	-.278	-.363	-.640									.750
	.860	-.051	-.101	-.153	-.208	-.257	-.349	-.631									.860
	.930	-.051	-.101	-.148	-.198	-.241	-.332	-.619									.930
	.032	-.741	-.665	-.473	-.090	.090	.360	.524									.032
	.083	-.674	-.484	-.087	-.009	.107	.309	.447									.083
	.160	-.299	-.162	-.078	.020	.100	.250	.382									.160
	.240	-.224	-.157	-.084	-.007	.057	.180	.307									.240
	.360	-.217	-.148	-.103	-.047	.007	.120	.245									.360

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 60-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c
M = 0.800; q = 618 lb/sq ft									M = 0.900; q = 701 lb/sq ft								
Upper surface	.000	-.423	-.104	.224	.460	.410	-.389	-.700	Upper surface	-.416	-.048	.249	.457	.413	-.269	-.727	.000
	.020	.418	.355	.253	.061	-.292	-.914	.796		.403	.339	.231	.043	-.349	-.427	-.936	.020
	.077	.290	.207	.104	-.044	-.258	-.844	.789		.274	.191	.081	-.070	-.315	-.264	-.895	.077
	.150	.206	.126	.036	-.086	-.244	-.765	.785		.191	.108	.010	-.119	-.300	-.143	-.884	.150
	.250	.128	.053	-.021	-.125	-.247	-.646	.772		.114	.039	-.047	-.161	-.314	-.638	-.845	.250
	.350	.076	.011	-.055	-.141	-.241	-.565	.736		.065	-.006	-.080	-.179	-.292	-.613	-.809	.350
	.450	.047	-.012	-.068	-.139	-.222	-.441	.689		.037	-.027	-.091	-.172	-.262	-.641	-.748	.450
	.550	.014	-.037	-.086	-.145	-.215	-.352	.657		.004	-.053	-.109	-.177	-.251	-.655	-.703	.550
	.640	.003	-.040	-.082	-.130	-.187	-.278	.620		-.005	-.054	-.102	-.159	-.216	-.659	-.649	.640
	.740	-.010	-.044	-.077	-.112	-.153	-.202	.584		-.015	-.055	-.091	-.132	-.169	-.616	-.591	.740
	.850	.022	-.005	-.027	-.047	-.071	-.112	.530		.020	-.011	-.035	-.058	-.075	-.639	-.524	.850
	.900	.033	.007	-.011	-.026	-.044	-.079	.510		.032	.003	-.017	-.034	-.042	-.613	-.500	.900
	.922	.035	.008	-.008	-.019	-.032	-.065	.506		.036	.003	-.013	-.022	-.049	-.605	-.489	.922
Lower surface	.040	-.721	-.607	-.425	-.148	.070	.305	.405	Lower surface	-.838	-.648	-.450	-.181	.042	.272	.379	.040
	.090	-.708	-.587	-.379	-.092	.055	.247	.351		-.817	-.619	-.414	-.118	.034	.224	.327	.090
	.150	-.701	-.575	-.359	-.082	.051	.208	.304		-.797	-.599	-.399	-.105	.033	.188	.283	.150
	.250	-.704	-.577	-.265	-.038	.054	.179	.254		-.777	-.612	-.299	-.059	.042	.144	.236	.250
	.340	-.733	-.560	-.161	-.046	.032	.142	.206		-.785	-.605	-.201	-.059	.021	.130	.189	.340
	.450	-.714	-.406	-.094	-.026	.037	.125	.171		-.788	-.453	-.120	-.036	.030	.117	.156	.450
	.550	-.644	-.210	-.060	-.006	.040	.112	.140		-.740	-.266	-.078	-.017	.035	.108	.125	.550
	.650	-.619	-.056	-.020	.022	.057	.113	.117		-.542	-.104	-.031	.014	.056	.114	.102	.650
	.800	-.002	.051	.030	.058	.078	.110	.061		-.039	.029	.027	.055	.082	.119	.047	.800
	.874	.103	.068	.044	.062	.074	.094	.002		.127	.054	.044	.063	.082	.109	-.008	.874
M = 0.940; q = 750 lb/sq ft									M = 0.980; q = 758 lb/sq ft								
Upper surface	.000	-.326	-.006	.241	.432	.422	-.114	-.651	Upper surface	-.220	.055	.255	.405	.416	.010	-.552	.000
	.020	.385	.308	.201	.024	-.300	1.261	-.934		.364	.282	.187	.038	-.226	1.123	1.364	.020
	.077	.253	.161	.050	-.098	-.316	1.104	-.924		.227	.128	.032	-.096	-.269	-.965	1.253	.077
	.150	.170	.081	-.020	-.159	-.320	1.027	-.905		.141	.041	-.050	-.156	-.282	-.902	1.202	.150
	.250	.096	.014	-.074	-.233	-.379	-.589	-.875		.057	-.032	-.130	-.225	-.352	-.562	1.156	.250
	.350	.047	-.027	-.102	-.269	-.400	-.564	-.840		.003	-.098	-.190	-.281	-.391	-.537	1.137	.350
	.450	.022	-.043	-.104	-.205	-.427	-.599	-.787		-.028	-.126	-.210	-.309	-.413	-.553	1.096	.450
	.550	.008	-.065	-.119	-.170	-.435	-.643	-.759		-.067	-.177	-.248	-.332	-.427	-.607	1.038	.550
	.640	-.017	-.063	-.112	-.161	-.414	-.630	-.719		-.077	-.195	-.270	-.348	-.418	-.614	-.864	.640
	.740	-.025	-.059	-.096	-.133	-.412	-.705	-.666		-.070	-.079	-.346	-.450	-.568	-.675	-.834	.740
	.850	.007	-.016	-.036	-.055	-.034	-.176	-.600		-.033	.024	-.045	-.266	-.428	-.638	-.764	.850
	.900	.015	-.006	-.017	-.029	-.011	-.098	-.574		-.025	.016	.016	-.076	-.212	-.619	-.675	.900
	.922	.014	-.006	-.012	-.019	-.001	-.071	-.561		-.029	.017	.030	-.028	-.132	-.532	-.604	.922
Lower surface	.040	-.817	-.669	-.527	-.211	-.010	.233	.363	Lower surface	-.746	-.619	-.519	-.278	-.077	.202	.346	.040
	.090	-.805	-.644	-.495	-.156	-.003	.189	.313		-.735	-.592	-.480	-.229	-.064	.164	.304	.090
	.150	-.806	-.626	-.412	-.136	-.004	.156	.267		-.733	-.579	-.425	-.225	-.082	.128	.260	.150
	.250	-.811	-.596	-.318	-.085	.014	.132	.222		-.744	-.561	-.403	-.203	-.074	.105	.219	.250
	.340	-.816	-.552	-.210	-.072	-.002	.097	.176		-.766	-.549	-.363	-.234	-.118	.083	.164	.340
	.450	-.756	-.438	-.126	-.040	.014	.085	.140		-.775	-.534	-.322	-.207	-.073	.043	.129	.450
	.550	-.676	-.294	-.080	-.021	.024	.075	.109		-.769	-.473	-.292	-.183	-.051	.023	.095	.550
	.650	-.539	-.176	-.031	.014	.048	.081	.091		-.679	-.364	-.228	-.120	-.007	.016	.074	.650
	.800	-.265	-.058	.029	.057	.084	.088	.045		-.390	-.172	-.009	.043	.037	.006	.036	.800
	.874	-.126	-.024	.044	.066	.096	.077	-.008		-.259	-.097	.045	.062	.039	-.021	-.006	.874

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BOD - Continued

(d) 60-percent-semispan station - Concluded

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$			$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c	
M = 1.050; q = 794 lb/sq ft									M = 1.105; q = 471 lb/sq ft										
Upper surface	.000	-.110	.128	.306	.446	.465	.104	-.409	Upper surface	.025	.256	.371	.525	.509	.232	-.201	.000		
	.020	.395	.330	.231	.092	-.164	-.964	-1.204		.416	.343	.277	.115	-.136	-.741	-.981	.020		
	.077	.258	.182	.086	-.038	-.193	-.826	-1.100		.280	.200	.127	.002	-.155	-.646	-.876	.077		
	.150	.173	.098	.011	-.097	-.208	-.771	-1.057		.198	.119	.056	-.036	-.157	-.617	-.840	.150		
	.250	.090	.017	-.068	-.175	-.272	-.508	-1.017		.119	.042	-.026	-.118	-.215	-.572	-.811	.250		
	.350	.028	-.033	-.126	-.216	-.318	-.455	-1.000		.054	-.022	-.083	-.171	-.248	-.385	-.501	.350		
	.450	-.002	-.072	-.158	-.249	-.339	-.457	-.965		.022	-.057	-.118	-.205	-.276	-.374	-.475	.450		
	.550	-.061	-.117	-.183	-.263	-.355	-.457	-.967		-.019	-.037	-.141	-.227	-.331	-.407	-.488	.550		
	.640	-.065	-.138	-.210	-.280	-.343	-.402	-.768		-.037	-.108	-.152	-.215	-.305	-.419	-.505	.640		
	.740	-.096	-.203	-.286	-.402	-.474	-.586	-.731		-.101	-.193	-.273	-.334	-.387	-.505	-.665	.740		
.850	-.070	-.140	-.237	-.321	-.405	-.553	-.677	-.058	-.144	-.199	-.296	-.369	-.472	-.581	.850				
.900	-.055	-.113	-.201	-.307	-.387	-.552	-.638	-.047	-.141	-.202	-.283	-.368	-.460	-.561	.900				
.922	-.052	-.098	-.170	-.278	-.364	-.548	-.587	-.051	-.142	-.205	-.284	-.374	-.468	-.547	.922				
Lower surface	.040	-.641	-.533	-.449	-.202	-.018	.241	.386	Lower surface	-.531	-.437	-.358	-.102	.049	.263	.416	.040		
	.090	-.628	-.506	-.407	-.156	-.003	.206	.345		-.508	-.397	-.327	-.066	.049	.231	.381	.090		
	.150	-.627	-.496	-.347	-.155	-.017	.174	.305		-.501	-.386	-.255	-.064	.032	.204	.344	.150		
	.250	-.635	-.475	-.330	-.136	-.012	.153	.266		-.490	-.344	-.232	-.051	.039	.177	.313	.250		
	.340	-.653	-.459	-.295	-.163	-.067	.113	.213		-.483	-.319	-.227	-.100	-.022	.125	.268	.340		
	.450	-.681	-.446	-.261	-.148	-.040	.097	.179		-.482	-.317	-.211	-.097	-.024	.131	.243	.450		
	.550	-.687	-.406	-.237	-.132	-.037	.076	.147		-.489	-.300	-.191	-.095	-.023	.121	.217	.550		
	.650	-.643	-.348	-.202	-.106	-.028	.068	.124		-.485	-.273	-.168	-.078	-.009	.122	.203	.650		
	.800	-.436	-.228	-.116	-.038	.012	.058	.088		-.373	-.202	-.104	-.021	.039	.131	.176	.800		
	.874	-.307	-.163	-.071	-.018	.010	.030	.045		-.292	-.169	-.080	-.007	.044	.107	.140	.874		
M = 1.000; q = 875 lb/sq ft																			
Upper surface	.000	.072	.234	.361	.486	.502	.291	-.111	Upper surface								.000		
	.020	.423	.367	.285	.155	-.051	-.570	-.834									.020		
	.077	.290	.220	.143	.036	-.098	-.510	-.740									.077		
	.150	.207	.141	.076	-.013	-.113	-.494	-.717									.150		
	.250	.131	.060	-.011	-.082	-.174	-.468	-.699									.250		
	.350	.067	.003	-.067	-.130	-.205	-.412	-.694									.350		
	.450	.036	-.033	-.102	-.157	-.215	-.347	-.673									.450		
	.550	.012	-.048	-.114	-.209	-.255	-.368	-.695									.550		
	.640	-.011	-.056	-.106	-.177	-.276	-.381	-.693									.640		
	.740	-.075	-.170	-.222	-.272	-.335	-.442	-.713									.740		
.850	-.042	-.104	-.185	-.254	-.314	-.423	-.676								.850				
.900	-.042	-.108	-.180	-.255	-.314	-.426	-.616								.900				
.922	-.044	-.113	-.181	-.261	-.320	-.434	-.561								.922				
Lower surface	.040	-.529	-.478	-.404	-.149	.024	.249	.408	Lower surface								.040		
	.090	-.490	-.438	-.330	-.072	.034	.220	.376									.090		
	.150	-.476	-.412	-.232	-.081	.034	.195	.339									.150		
	.250	-.441	-.332	-.185	-.055	.040	.179	.312									.250		
	.340	-.409	-.302	-.186	-.094	-.024	.108	.281									.340		
	.450	-.355	-.279	-.167	-.105	-.035	.107	.277									.450		
	.550	-.330	-.262	-.144	-.080	-.013	.132	.261									.550		
	.650	-.320	-.232	-.116	-.050	.011	.141	.252									.650		
	.800	-.283	-.168	-.062	.003	.069	.176	.238									.800		
	.874	-.252	-.138	-.038	.025	.084	.161	.204									.874		

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 80-percent-hemispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c
M = 0.800; q = 616 lb/sq ft																	
Upper surface	.036	.429	.381	.303	.156	-.161	-.652	-.497	Lower surface	.430	.381	.295	.151	-.193	-.438	-.575	.036
	.084	.346	.283	.198	.063	-.170	-.640	-.488		.346	.283	.190	.051	-.202	-.4316	-.551	.084
	.150	.250	.189	.104	-.017	-.189	-.614	-.484		.257	.189	.095	-.034	-.218	-.4237	-.543	.150
	.260	.177	.119	.048	-.050	-.191	-.585	-.476		.179	.120	.039	-.065	-.225	-.4175	-.529	.260
	.350	.115	.061	-.002	-.090	-.206	-.551	-.459		.115	.059	-.015	-.112	-.247	-.4099	-.515	.350
	.460	.062	.017	-.037	-.114	-.212	-.507	-.440		.061	.012	-.055	-.140	-.258	-.4044	-.502	.460
	.550	.023	-.010	-.056	-.121	-.202	-.462	-.423		.024	-.016	-.075	-.150	-.247	-.3999	-.492	.550
	.600	-.000	-.026	-.066	-.125	-.196	-.434	-.414		-.003	-.033	-.085	-.154	-.236	-.3900	-.486	.600
	.660	-.021	-.037	-.069	-.120	-.182	-.403	-.406		-.023	-.044	-.090	-.148	-.219	-.3828	-.481	.660
	.760	-.056	-.044	-.061	-.099	-.143	-.343	-.388		-.054	-.051	-.080	-.124	-.164	-.3588	-.468	.760
.860	-.120	-.059	-.049	-.071	-.100	-.280	-.374	-.114	-.063	-.064	-.089	-.108	-.3109	-.440	.860		
.900	-.158	-.068	-.040	-.058	-.078	-.255	-.369	-.153	-.076	-.054	-.070	-.079	-.2888	-.456	.900		
M = 0.900; q = 701 lb/sq ft																	
Upper surface	.079	-.462	-.486	-.407	-.167	.034	.259	.321	Lower surface	-.481	-.492	-.426	-.172	.034	.251	.313	.079
	.160	-.452	-.471	-.382	-.109	.048	.210	.259		-.473	-.481	-.376	-.121	.045	.205	.254	.160
	.250	-.446	-.463	-.387	-.079	.031	.163	.198		-.475	-.478	-.378	-.085	.031	.164	.194	.250
	.350	-.435	-.471	-.401	-.045	.039	.139	.156		-.468	-.492	-.378	-.049	.039	.147	.153	.350
	.450	-.426	-.480	-.346	-.021	.045	.122	.121		-.461	-.510	-.345	-.024	.046	.134	.119	.450
	.550	-.444	-.482	-.220	-.001	.051	.105	.082		-.477	-.521	-.253	-.004	.051	.122	.083	.550
	.650	-.447	-.478	-.169	.010	.061	.106	.077		-.481	-.521	-.212	.013	.064	.126	.079	.650
	.760	-.460	-.456	-.064	.031	.071	.092	.041		-.481	-.512	-.106	.037	.076	.120	.044	.760
	.860	-.440	-.402	-.001	.037	.067	.058	-.017		-.462	-.469	-.031	.046	.074	.103	-.014	.860
	.900																
M = 0.950; q = 788 lb/sq ft																	
Upper surface	.036	.416	.376	.294	.138	-.243	-.1271	-.755	Lower surface	.387	.313	.222	.112	-.099	-.1080	-.1325	.036
	.084	.335	.277	.187	.040	-.276	-.1147	-.640		.299	.209	.109	.002	-.184	-.0976	-.1261	.084
	.150	.250	.187	.091	-.044	-.321	-.1083	-.639		.213	.112	.004	-.109	-.258	-.0917	-.1197	.150
	.260	.173	.118	.035	-.070	-.346	-.1023	-.623		.138	.048	-.058	-.177	-.294	-.0878	-.1154	.260
	.350	.112	.058	-.021	-.117	-.391	-.086	-.611		.077	-.003	-.110	-.245	-.348	-.0847	-.1134	.350
	.460	.058	.010	-.062	-.153	-.398	-.057	-.591		.029	-.026	-.200	-.292	-.445	-.0752	-.1126	.460
	.550	.022	-.017	-.083	-.166	-.216	-.0575	-.572		-.000	-.048	-.227	-.324	-.455	-.0598	-.1129	.550
	.600	-.002	-.035	-.095	-.168	-.168	-.058	-.564		-.015	-.058	-.203	-.343	-.452	-.0602	-.1123	.600
	.660	-.020	-.044	-.099	-.165	-.175	-.0576	-.554		-.028	-.065	-.097	-.362	-.471	-.0623	-.1115	.660
	.760	-.050	-.051	-.088	-.135	-.172	-.0533	-.533		-.041	-.061	-.029	-.373	-.4512	-.0649	-.0838	.760
	.860	-.105	-.055	-.072	-.095	-.104	-.0517	-.517		-.078	-.063	-.031	-.028	-.411	-.0677	-.0746	.860
	.900	-.141	-.061	-.060	-.074	-.074	-.0513	-.513		-.109	-.068	-.021	.016	-.189	-.0694	-.0738	.900
M = 0.980; q = 878 lb/sq ft																	
Upper surface	.079	-.559	-.537	-.419	-.182	.015	.206	.293	Lower surface	-.678	-.708	-.746	-.652	-.110	.134	.259	.079
	.160	-.537	-.514	-.381	-.127	.031	.165	.236		-.642	-.672	-.674	-.335	-.067	.093	.200	.160
	.250	-.507	-.504	-.373	-.085	.023	.127	.177		-.617	-.647	-.617	-.264	-.055	.051	.146	.250
	.350	-.489	-.509	-.383	-.049	.035	.113	.138		-.594	-.642	-.508	-.117	-.033	.034	.113	.350
	.450	-.467	-.561	-.357	-.022	.045	.104	.110		-.563	-.666	-.360	-.035	-.012	.023	.088	.450
	.550	-.476	-.604	-.268	-.003	.053	.095	.073		-.525	-.703	-.214	.000	-.001	.008	.058	.550
	.650	-.486	-.610	-.228	.014	.067	.102	.072		-.508	-.706	-.164	.015	.018	.015	.060	.650
	.760	-.491	-.594	-.128	.039	.080	.099	.042		-.520	-.675	-.052	.050	.039	.010	.035	.760
	.860	-.471	-.541	-.053	.051	.080	.081	-.012		-.508	-.527	.019	.065	.046	-.011	-.007	.860
	.900																

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 80-percent-semispan station - C included

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 8^\circ$	$\alpha = 10^\circ$	
	M = 1.030; q = 794 lb/sq ft									
Upper surface	.036 .084 .150 .260 .350 .460 .550 .600 .660 .760 .860 .900	.394 .304 .214 .138 .071 .012 -.028 -.049 -.078 -.108 -.121 -.105	.341 .238 .143 .082 .016 -.060 -.099 -.123 -.152 -.175 -.196 -.190	.270 .161 .059 -.006 -.070 -.136 -.174 -.195 -.225 -.255 -.286 -.295	.163 .055 -.054 -.118 -.177 -.243 -.270 -.287 -.294 -.328 -.365 -.379	.093 -.125 -.193 -.230 -.274 -.336 -.377 -.389 -.393 -.436 -.467 -.472	-.923 -1.047 -1.047 -1.011 -.981 -.988 -.993 -.995 -.994 -.995 -.921 -.699	1.102 1.047 1.011 -.981 -.988 -.993 -.995 -.994 -.995 -.921 -.699		
Lower surface	.079 .160 .250 .350 .450 .550 .590 .690 .800	-.773 -.761 -.755 -.753 -.739 -.718 -.701 -.667 -.622	-.677 -.657 -.659 -.668 -.668 -.654 -.641 -.593 -.516	-.748 -.644 -.574 -.515 -.428 -.329 -.286 -.190 -.116	-.586 -.304 -.237 -.184 -.141 -.117 -.091 -.058 -.038	-.128 -.070 -.064 -.050 -.037 -.035 -.013 -.002 -.006	.179 .133 .096 .081 .071 .050 .059 .051 .025	.299 .243 .188 .158 .136 .106 .109 .088 .051		
	M = 1.000; q = 874 lb/sq ft									
Upper surface	.036 .084 .150 .260 .350 .460 .550 .600 .660 .760 .860 .900	.421 .334 .243 .171 .127 .068 .038 .016 -.014 -.048 -.081 -.091	.380 .284 .188 .116 .058 -.004 -.029 -.042 -.059 -.099 -.131 -.140	.323 .219 .124 .060 .004 -.062 -.078 -.102 -.128 -.163 -.187 -.201	.215 .119 .031 -.022 -.071 -.120 -.156 -.174 -.184 -.214 -.248 -.259	.059 -.015 -.087 -.117 -.159 -.204 -.237 -.255 -.274 -.297 -.319 -.324	-.480 -.431 -.422 -.426 -.438 -.464 -.487 -.494 -.500 -.496 -.443 -.438	-.795 -.732 -.698 -.673 -.666 -.668 -.677 -.681 -.683 -.687 -.695 -.700		
Lower surface	.079 .160 .250 .350 .450 .550 .590 .690 .800	-.821 -.773 -.732 -.705 -.680 -.667 -.649 -.428 -.345	-.787 -.728 -.683 -.649 -.600 -.369 -.327 -.249 -.185	-.669 -.628 -.561 -.207 -.193 -.186 -.174 -.139 -.102	-.514 -.207 -.169 -.162 -.140 -.123 -.099 -.060 -.018	-.113 -.069 -.066 -.054 -.037 -.028 -.006 -.027 -.061	.172 .151 .135 .135 .135 .128 .145 .157 .158	.372 .328 .281 .258 .251 .229 .241 .227 .201		

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(f) 95-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/c
M = 0.800; q = 618 lb/sq ft									M = 0.900; q = 701 lb/sq ft								
Upper surface	.080	.289	.259	.227	.107	-.119	-.492	-.339	Upper surface	.301	.267	.221	.097	-.151	-.685	-.400	.080
	.150	.228	.189	.151	.036	-.152	-.470	-.338		.239	.199	.146	.029	-.171	-.666	-.401	.150
	.250	.104	.071	.037	-.053	-.191	-.436	-.339		.113	.076	.029	-.074	-.235	-.615	-.403	.250
	.360	.033	.006	-.016	-.089	-.189	-.393	-.334		.036	.005	-.034	-.126	-.249	-.562	-.405	.360
	.450	-.026	-.044	-.057	-.110	-.182	-.353	-.328		-.036	-.058	-.085	-.151	-.220	-.520	-.406	.450
	.560	-.081	-.090	-.084	-.119	-.168	-.307	-.324		-.102	-.110	-.113	-.150	-.187	-.469	-.405	.560
	.650	-.108	-.107	-.080	-.103	-.143	-.267	-.320		-.140	-.130	-.105	-.123	-.155	-.421	-.404	.650
	.760																.760
	.800	-.151	-.144	-.075	-.078	-.103	-.223	-.319		-.197	-.169	-.091	-.087	-.108	-.350	-.405	.800
Lower surface	.110	-.209	-.239	-.620	-.245	-.014	.197	.225	Lower surface	-.223	-.256	-.589	-.282	-.007	.228	.218	.110
	.190	-.199	-.220	-.636	-.160	.014	.142	.156		-.215	-.239	-.587	-.179	.016	.168	.147	.190
	.260																.260
	.360	-.181	-.196	-.538	-.084	.001	.059	.052		-.209	-.217	-.536	-.095	-.003	.077	.037	.360
	.450	-.164	-.184	-.136	-.040	.015	.036	.011		-.207	-.203	-.333	-.043	.011	.041	-.015	.450
	.560	-.156	-.171	.109	.004	.039	.028	-.015		-.207	-.192	-.049	.010	.039	.027	-.051	.560
	.600	-.155	-.164	.120	.020	.044	.019	-.030		-.206	-.186	.029	.023	.044	.018	-.069	.600
	.710	-.156	-.157	.112	.046	.060	.014	-.052		-.203	-.178	.103	.053	.064	.010	-.094	.710
M = 0.940; q = 730 lb/sq ft									M = 0.980; q = 758 lb/sq ft								
Upper surface	.080	.308	.283	.222	.092	-.182	1.107	-.489	Upper surface	.291	.267	.206	.051	-.187	-.966	1.253	.080
	.150	.252	.217	.151	.023	-.210	-.860	-.481		.238	.205	.149	-.026	-.276	-.924	1.181	.150
	.250	.125	.093	.029	-.081	-.239	-.798	-.476		.115	.082	.048	-.131	-.317	-.884	1.162	.250
	.360	.046	.021	-.040	-.145	-.273	-.660	-.472		.036	.011	-.014	-.187	-.351	-.869	1.134	.360
	.450	-.034	-.043	-.102	-.200	-.316	-.657	-.471		-.043	-.060	-.075	-.259	-.411	-.865	1.116	.450
	.560	-.111	-.093	-.133	-.156	-.215	-.611	-.468		-.130	-.128	-.119	-.213	-.478	-.861	1.023	.560
	.650	-.154	-.114	-.121	-.126	-.134	-.538	-.467		-.174	-.145	-.098	-.021	-.495	-.839	-.776	.650
	.760																.760
	.800	-.227	-.161	-.094	-.086	-.104	-.436	-.465		-.249	-.192	-.069	-.023	-.109	-.851	-.727	.800
Lower surface	.110	-.284	-.294	-.593	-.270	.025	.186	.208	Lower surface	-.388	-.361	-.567	-.274	-.105	.079	.189	.110
	.190	-.275	-.284	-.579	-.174	.035	.136	.142		-.375	-.337	-.557	-.206	-.058	.049	.130	.190
	.260																.260
	.360	-.263	-.273	-.545	-.093	-.003	.041	.033		-.361	-.322	-.557	-.147	-.062	-.025	.033	.360
	.450	-.254	-.268	-.423	-.035	.010	-.001	-.026		-.352	-.323	-.483	-.106	-.056	-.074	-.021	.450
	.560	-.242	-.265	-.173	.017	.039	-.016	-.070		-.336	-.320	-.304	-.044	-.004	-.112	-.074	.560
	.600	-.237	-.268	-.057	.031	.045	-.026	-.091		-.328	-.315	-.216	-.011	.005	-.129	-.105	.600
	.710	-.230	-.276	.096	.059	.064	-.029	-.121		-.316	-.301	-.049	.046	.035	-.142	-.148	.710

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Concluded

(f) 75-percent-semispan station - Concluded

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/c	
	M = 1.050; q = 794 lb/sq ft									M = 1.125; q = 842 lb/sq ft								
Upper surface	.080 .150 .250 .360 .450 .560 .650 .760 .800	.293 .241 .120 .048 -.027 -.111 -.147 - - -.233	.232 .172 .052 -.018 -.098 -.208 -.277 - - -.300	.173 .106 -.009 -.061 -.130 -.242 -.322 - - -.434	.080 -.003 -.097 -.150 -.212 -.309 -.377 - - -.478	-.094 -.186 -.235 -.271 -.324 -.405 -.445 - - -.501	-.810 -.774 -.746 -.739 -.736 -.737 -.720 - - -.748	-1.084 -1.015 -1.007 -.991 -.982 -.979 -.949 - - -.965		.319 .271 .162 .098 .030 -.069 -.142 - - -.198	.257 .197 .089 .039 -.016 -.109 -.186 - - -.296	.208 .133 .045 -.006 -.059 -.145 -.218 - - -.328	.113 .020 -.050 -.094 -.147 -.239 -.290 - - -.388	-.024 -.121 -.167 -.199 -.239 -.308 -.362 - - -.427	-.593 -.556 -.553 -.549 -.554 -.561 -.552 - - -.578	-.864 -.807 -.804 -.785 -.776 -.773 -.751 - - -.766	.080 .150 .250 .360 .450 .560 .650 .760 .800	
Lower surface	.110 .190 .260 .360 .450 .560 .600 .710	-.503 -.479 - -.457 -.445 -.428 -.421 -.407	-.632 -.598 - -.570 -.564 -.568 -.565 -.549	-1.019 -.963 - -.637 -.416 -.230 -.174 -.112	-.807 -.490 - -.364 -.269 -.110 -.061 -.029	-.224 -.142 - -.153 -.122 -.056 -.042 -.032	.106 .077 - .013 -.023 -.064 -.082 -.100	.221 .168 - .082 .033 -.017 -.046 -.090		-.589 -.565 - -.533 -.514 -.494 -.482 -.471	-.696 -.654 - -.616 -.788 -.768 -.731 - - -.696	-.838 -.799 - -.749 -.717 -.538 -.434 -.227	-.700 -.506 - -.261 -.261 -.186 -.108 -.001	-.202 -.129 - -.132 -.103 -.020 -.021 .055	.174 .136 - .086 .082 .051 .032 .012	.292 .244 - .176 .141 .097 .071 .027	.110 .190 .260 .360 .450 .560 .600 .710	
	M = 1.200; q = 875 lb/sq ft																	
Upper surface	.080 .150 .250 .360 .450 .560 .650 .760 .800	.327 .284 .170 .125 .075 -.007 -.084 - -.193	.285 .228 .124 .077 .028 -.042 -.115 - -.229	.232 .161 .067 .021 -.027 -.093 -.160 - -.263	.162 .081 -.001 -.044 -.090 -.153 -.217 - -.316	.044 -.041 -.101 -.132 -.170 -.225 -.282 - -.360	-.410 -.379 -.411 -.416 -.425 -.441 -.444 - -.479	-.728 -.677 -.680 -.669 -.664 -.662 -.648 - -.660										
Lower surface	.110 .190 .260 .360 .450 .560 .600 .710	-.810 -.778 - -.757 -.735 -.725 -.711 -.670	-.785 -.745 - -.712 -.695 -.683 -.671 -.610	-.697 -.663 - -.629 -.607 -.574 -.521 -.288	-.598 -.555 - -.352 -.205 -.197 -.160 -.046	-.232 -.135 - -.143 -.139 -.098 -.048 -.054	.176 .139 - .098 .100 .106 .090 .074	.332 .280 - .220 .203 .172 .146 .101									.110 .190 .260 .360 .450 .560 .600 .710	

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING

(a) Station A

x/i	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/i	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/i
$M = 0.900; q = 500 \text{ lb/sq ft}$								$M = 0.900; q = 350 \text{ lb/sq ft}$								
.055		.002		.019	.034	.035	-.004	.104	.111	.093	.113	.059	.064	.054	.055	
.166	.043	.022	.005	-.006	-.017	-.031	-.032	.044	.021	.003	-.009	-.025	-.029	-.026	.166	
.277	.029	.005	-.008	-.017	-.027	-.036	-.041	.027	.003	-.012	-.022	-.033	-.027	-.018	.277	
.367	.166	.136	.103	.072	.046	.005	-.017	.183	.151	.119	.093	.065	.048	.051	.367	
.387	.114	.076	.034	.005	-.028	-.097	-.181	.132	.092	.056	.025	-.008	-.053	-.110	.387	
.415	.088	.040	-.008	-.048	-.095	-.194	-.310	.100	.050	.004	-.038	-.088	-.159	-.245	.415	
.443	.069	.019	-.036	-.080	-.132	-.239	-.370	.074	.020	-.033	-.084	-.138	-.226	-.324	.443	
.498	.031	-.019	-.072	-.119	-.170	-.276	-.378	.027	-.027	-.086	-.143	-.196	-.294	-.408	.498	
.553	.008	-.042	-.091	-.129	-.171	-.257	-.295	-.010	-.066	-.125	-.191	-.272	-.366	-.471	.553	
.581	-.016	-.056	-.101	-.132	-.164	-.237	-.267	-.029	-.080	-.129	-.188	-.279	-.420	-.528	.581	
.609	-.003	-.039	-.075	-.104	-.131	-.180	-.204	-.017	-.060	-.105	-.150	-.198	-.410	-.515	.609	
.636	-.007	-.039	-.064	-.089	-.108	-.143	-.176	-.020	-.055	-.090	-.119	-.143	-.397	-.488	.636	
.664	-.011	-.033	-.052	-.070	-.079	-.098	-.136	-.019	-.044	-.065	-.084	-.095	-.100	-.072	.664	
.692	.001	-.016	-.032	-.039	-.044	-.051	-.081	-.004	-.020	-.033	-.043	-.048	-.029	-.053	.692	
.719	.003	-.008	-.017	-.020	-.020	-.025	-.051	.002	-.010	-.016	-.018	-.019	-.000	-.041	.719	
.774															.774	
.830	.000	-.003	-.003	.001	.005	.009	-.003	-.008	-.005	-.003	.001	.004	.018	-.011	.830	
.871	-.007	-.008	.002	.002	.003	.003	-.004	-.012	-.008	-.005	-.001	.004	.009	-.012	.871	
.954	.022	.025	.031	.039	.045	.040	.033	.024	.029	.037	.043	.047	.043	.034	.954	
$M = 0.940; q = 560 \text{ lb/sq ft}$								$M = 0.980; q = 380 \text{ lb/sq ft}$								
.055	.070	.056	.035	.010	.000			.146	.128	.094	.077	.055	.028	.014	.055	
.166	.042	.017	.001	-.015	-.024	-.032	-.018	.048	.026	.008	-.003	-.013	-.020	-.005	.166	
.277	.021	-.004	-.015	-.030	-.035	-.024	-.006	.028	.002	-.012	-.021	-.027	-.012	.013	.277	
.367	.191	.161	.128	.102	.082	.072	.085	.214	.177	.155	.129	.118	.111	.124	.367	
.387	.143	.104	.067	.037	.010	-.026	-.067	.168	.132	.099	.074	.051	.014	-.023	.387	
.415	.106	.056	.011	-.033	-.069	-.135	-.200	.130	.083	.039	.002	-.030	-.090	-.154	.415	
.443	.078	.025	-.029	-.081	-.126	-.199	-.279	.098	.044	-.005	-.048	-.092	-.157	-.226	.443	
.498	.023	-.035	-.091	-.139	-.195	-.278	-.372	.038	-.017	-.067	-.118	-.163	-.238	-.330	.498	
.553	-.027	-.090	-.168	-.221	-.263	-.353	-.443	-.033	-.102	-.146	-.188	-.235	-.316	-.392	.553	
.581	-.048	-.107	-.186	-.269	-.323	-.403	-.497	-.056	-.145	-.197	-.244	-.285	-.366	-.450	.581	
.609	-.037	-.089	-.144	-.255	-.315	-.409	-.503	-.060	-.135	-.193	-.248	-.297	-.375	-.456	.609	
.636	-.043	-.077	-.112	-.223	-.329	-.428	-.515	-.080	-.155	-.216	-.266	-.312	-.398	-.477	.636	
.664	-.037	-.053	-.068	-.082	-.264	-.450	-.515	-.085	-.165	-.238	-.289	-.339	-.421	-.506	.664	
.692	-.019	-.024	-.031	-.030	-.049	-.261	-.384	-.097	-.136	-.215	-.271	-.323	-.423	-.522	.692	
.719	-.005	-.007	-.014	-.011	-.001	-.018	-.030	-.059	-.033	-.063	-.088	-.140	-.279	-.438	.719	
.774															.774	
.830	-.013	-.007	-.004	-.003	.009	.032	-.005	-.025	.001	.025	.036	.042	.020	.006	.830	
.871	-.018	-.013	-.005	-.002	.004	.020	-.005	-.024	.001	.017	.029	.038	.037	.023	.871	
.954	.021	.029	.036	.038	.044	.053	.045	.033	.041	.055	.063	.073	.087	.085	.954	

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRE SURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Co tinued

(a) Station A - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l
$M = 1.050; q = 397 \text{ lb/sq ft}$								$M = 1.125; q = 421 \text{ lb/sq ft}$							
.055	.186	.165	.135	.117	.099	.073	.065	.151	.129	.107	.092	.067	.039	.016	.055
.166	.087	.069	.054	.044	.031	.023	.022	.064	.045	.035	.021	.006	-.008	-.016	.166
.277	.033	.020	.012	.004	-.006	-.012	.057	.023	.013	-.001	-.005	-.013	-.025	-.032	.277
.367	.258	.215	.181	.164	.153	.167	.194	.066	.057	.048	.040	.035	.048	.099	.367
.387	.225	.179	.145	.123	.102	.083	.055	.140	.094	.081	.076	.061	.039	.040	.387
.415	.184	.132	.091	.052	.023	-.016	-.076	.178	.135	.103	.071	.040	-.019	-.056	.415
.443	.155	.096	.045	-.003	-.037	-.085	-.149	.153	.104	.065	.028	-.009	-.071	-.113	.443
.498	.094	.040	-.019	-.072	-.112	-.167	-.248	.102	.053	.007	-.031	-.074	-.141	-.200	.498
.553	.016	-.037	-.090	-.135	-.176	-.236	-.307	.044	-.010	-.053	-.088	-.129	-.197	-.249	.553
.581	-.023	-.081	-.143	-.187	-.219	-.286	-.363	-.001	-.051	-.092	-.131	-.173	-.243	-.291	.581
.609	-.017	-.077	-.140	-.195	-.233	-.298	-.368	-.005	-.060	-.108	-.146	-.186	-.246	-.289	.609
.636	-.038	-.099	-.161	-.209	-.250	-.319	-.399	-.013	-.072	-.119	-.160	-.199	-.268	-.328	.636
.664	-.058	-.115	-.180	-.233	-.273	-.344	-.420	-.034	-.084	-.126	-.169	-.213	-.287	-.343	.664
.692	-.065	-.110	-.171	-.230	-.268	-.353	-.439	-.039	-.093	-.136	-.171	-.217	-.296	-.361	.692
.719	-.076	-.092	-.117	-.163	-.175	-.264	-.396	-.048	-.083	-.121	-.151	-.187	-.257	-.347	.719
.774															.774
.830	-.067	-.062	-.043	-.041	-.046	-.068	-.061	-.047	-.053	-.046	-.039	-.039	-.031	-.021	.830
.871	-.091	-.076	-.059	-.057	-.057	-.069	-.051	-.068	-.064	-.054	-.037	-.032	-.025	-.012	.871
.954	-.133	-.121	-.087	-.056	-.048	-.034	-.043	-.063	-.065	-.053	-.031	-.012	.010	.040	.954
$M = 1.000; q = 457 \text{ lb/sq ft}$															
.055	.169	.151	.133	.101	.085	.060	.028								.055
.166	.077	.059	.047	.034	.016	.003	-.000								.166
.277	.030	.021	.014	.010	.009	-.008	-.015								.277
.367	.032	.064	.054	.037	.038	.047	.053								.367
.387	.041	.046	.043	.042	.038	.036	.034								.387
.415	.200	.151	.111	.077	.051	.000	-.040								.415
.443	.175	.131	.088	.053	.019	-.047	-.094								.443
.498	.134	.085	.040	-.005	-.046	-.111	-.168								.498
.553	.069	.025	-.017	-.059	-.096	-.163	-.213								.553
.581	.025	-.021	-.063	-.102	-.141	-.201	-.259								.581
.609	.014	-.029	-.074	-.117	-.150	-.215	-.266								.609
.636	.003	-.048	-.093	-.133	-.170	-.238	-.295								.636
.664	-.017	-.056	-.103	-.149	-.185	-.247	-.300								.664
.692	-.030	-.075	-.116	-.156	-.190	-.263	-.324								.692
.719	-.046	-.085	-.122	-.156	-.191	-.255	-.332								.719
.774															.774
.830	-.040	-.043	-.043	-.037	-.035	-.024	-.010								.830
.871	-.071	-.060	-.046	-.036	-.027	-.017	-.005								.871
.954	-.088	-.079	-.066	-.053	-.040	-.030	-.030								.954

TABLE V. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(b) Station B

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l	
M = 0.800; q = 308 lb/sq ft								M = 0.900; q = 350 lb/sq ft									
.166	.025	.014	.004	-.006	-.017	-.052	-.071	.025	.016	.003	-.007	-.018	-.046	-.061	.166		
.277	.001	-.006	-.018	-.026	-.034	-.061	-.081	-.001	-.011	-.020	-.030	-.037	-.054	-.058	.277		
.367	.096	.063	.029	.012	-.013	-.096	-.187	.115	.084	.038	.025	.010	-.051	-.106	.367		
.387	.212	.183	.142	.079	.022	-.093	-.218	.238	.203	.168	.117	.054	-.042	-.138	.387		
.443	.088	.034	-.024	-.081	-.153	-.285	-.448	.094	.039	-.023	-.082	-.150	-.277	-.400	.443		
.498	.031	-.022	-.079	-.130	-.188	-.320	-.468	.026	-.029	-.092	-.148	-.213	-.345	-.477	.498		
.553															.553		
.609	-.016	-.047	-.083	-.114	-.145	-.219	-.277	-.029	-.069	-.111	-.158	-.208	-.254	-.357	.609		
.664								.005	-.001	-.007	-.007	-.006	.007	-.048	.664		
.719	.003	-.002	-.008	-.011	-.011	-.016	-.056	.005	-.001	-.007	-.007	-.006	.007	-.048	.719		
.774								-.009	-.005	-.002	.000	.004	.014	-.015	.774		
.830	-.003	-.003	-.002	.002	.005	.006	.003	-.003	-.002	.001	.003	.006	.019	.003	.830		
.871	-.003	-.002	.001	.002	.009	.012	.013								.871		
M = 0.940; q = 365 lb/sq ft								M = 0.980; q = 380 lb/sq ft									
.166	.021	.011	.002	-.012	-.024	-.048	-.064	.031	.018	.009	-.001	-.012	-.034	-.061	.166		
.277	-.004	-.016	-.025	-.036	-.043	-.052	-.049	.004	-.013	-.020	-.027	-.032	-.038	-.033	.277		
.367	.127	.088	.044	.035	.023	-.024	-.064	.149	.122	.059	.063	.061	.021	-.018	.367		
.387	.247	.215	.187	.135	.072	-.012	-.098	.270	.234	.216	.173	.109	.033	-.052	.387		
.443	.096	.039	-.016	-.074	-.141	-.239	-.358	.114	.056	.008	-.044	-.112	-.200	-.302	.443		
.498	.018	-.039	-.092	-.152	-.222	-.327	-.434	.034	-.022	-.075	-.135	-.189	-.283	-.380	.498		
.553															.553		
.609	-.051	-.095	-.143	-.277	-.338	-.450	-.561	-.070	-.146	-.208	-.262	-.313	-.410	-.513	.609		
.664								-.066	-.036	-.051	-.067	-.113	-.220	-.305	.664		
.719	.002	-.001	-.002	-.002	.006	-.035	-.080								.719		
.774								-.033	-.002	.023	.033	.037	.017	-.018	.774		
.830	-.016	-.010	-.004	-.003	.006	.025	-.013	-.033	.007	.023	.031	.040	.031	-.003	.830		
.871	-.012	-.008	-.002	-.000	.007	.025	.006								.871		
M = 1.030; q = 397 lb/sq ft								M = 1.125; q = 481 lb/sq ft									
.166	.071	.064	.056	.045	.036	.003	-.043	.044	.039	.034	.026	.008	-.025	-.066	.166		
.277	.008	.005	.002	-.003	-.011	-.042	.009	-.000	-.003	-.006	-.005	-.020	-.048	-.078	.277		
.367	.205	.157	.042	.090	.102	.082	.056	-.063	-.019	-.047	-.058	-.059	-.046	-.026	.367		
.387	.320	.284	.267	.220	.156	.095	.021	.294	.223	.215	.175	.134	.047	-.005	.387		
.443	.173	.110	.058	-.005	-.053	-.127	-.217	.170	.113	.063	.016	-.029	-.112	-.185	.443		
.498	.090	.036	-.030	-.090	-.134	-.206	-.295	.099	.039	-.013	-.053	-.099	-.177	-.245	.498		
.553															.553		
.609	-.029	-.093	-.154	-.206	-.250	-.334	-.427	-.019	-.066	-.120	-.158	-.204	-.284	-.352	.609		
.664								-.053	-.074	-.091	-.103	-.125	-.151	-.178	.664		
.719	-.076	-.081	-.095	-.124	-.134	-.189	-.250								.719		
.774								-.061	-.051	-.046	-.038	-.043	-.044	-.037	.774		
.830	-.073	-.063	-.047	-.043	-.050	-.073	-.078	-.048	-.046	-.039	-.031	-.029	-.048	-.046	.830		
.871	-.062	-.061	-.055	-.052	-.055	-.085	-.086								.871		
M = 1.000; q = 437 lb/sq ft																	
.166	.058	.052	.046	.032	.017	-.015	-.049								.166		
.277	.017	.011	.007	.009	.002	-.028	-.049								.277		
.367	-.020	.010	.009	-.060	-.059	-.063	-.059								.367		
.387	.216	.082	.071	.156	.121	.055	-.007								.387		
.443	.191	.139	.092	.030	-.010	-.089	-.163								.443		
.498	.120	.077	.034	-.023	-.065	-.142	-.215								.498		
.553															.553		
.609	.008	-.035	-.078	-.120	-.158	-.239	-.319								.609		
.664															.664		
.719	-.059	-.075	-.094	-.111	-.126	-.147	-.173								.719		
.774															.774		
.830	-.061	-.056	-.051	-.051	-.046	-.042	-.036								.830		
.871	-.049	-.042	-.035	-.033	-.031	-.042	-.041								.871		

x, l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l
M = 0.800; q = 308 lb/sq ft								
.055	.048	.053	.059	.057	.054	.041	-.031	
.166	-.010	-.002	.000	.001	-.004	-.011	-.112	
.277	-.028	-.021	-.019	-.019	-.024	-.044	-.126	
.353								
.367	.365	.394	.366	.360	.291	.243	.161	
.692	.029	.031	.034	.040	.045	.052	.009	
.719	.008	.008	.010	.013	.022	.022	.009	
.774	.001	.000	.004	.006	.015	.020	.001	
.830	.009	.009	.011	.012	.020	.029	.019	
.871	.026	.024	.030	.028	.035	.043	.033	
.954	.029	.033	.034	.037	.040	.035	.037	
M = 0.940; q = 365 lb/sq ft								
.055	.061	.066	.069	.064	.056	.023	-.030	
.166	-.008	-.006	.001	-.007	-.013	-.043	-.100	
.277	-.029	-.027	-.025	-.032	-.034	-.062	-.101	
.353								
.367	.427	.416	.336	.361	.310	.299	.170	
.692	.001	.027	.035	.041	.031	-.046	.124	
.719	.020	.017	.015	.023	.033	-.001	-.039	
.774	.004	.004	.007	.010	.023	.035	-.024	
.830	.002	.006	.007	.006	.019	.041	-.013	
.871	.022	.022	.027	.028	.033	.053	.022	
.954	.033	.035	.039	.039	.038	.043	.047	
M = 1.040; q = 397 lb/sq ft								
.055	.117	.122	.126	.120	.116	.083	.036	
.166	.044	.047	.052	.052	.041	.012	-.056	
.277	-.007	.000	.006	.006	-.002	-.043	-.044	
.353								
.367	.479	.381	.107	.385	.341	.361	.362	
.692	-.093	-.076	-.077	-.076	-.061	-.069	-.123	
.719	-.088	-.072	-.069	-.076	-.071	-.097	-.122	
.774	-.080	-.057	-.038	-.040	-.047	-.083	-.114	
.830	-.058	-.050	-.034	-.036	-.043	-.081	-.101	
.871	-.029	-.032	-.024	-.028	-.034	-.056	-.059	
.954	-.102	-.095	-.076	-.063	-.072	-.083	-.118	
M = 1.000; q = 457 lb/sq ft								
.055	.102	.111	.115	.107	.100	.072	.008	
.166	.028	.036	.043	.043	.026	-.011	-.073	
.277	-.001	.011	.010	.013	.005	-.029	-.102	
.353								
.367	.271	.275	-.003	.258	.252	.224	.144	
.692	-.057	-.058	-.051	-.049	-.043	-.035	-.069	
.719	-.064	-.062	-.057	-.058	.053	-.048	-.051	
.774	-.055	-.051	-.045	-.048	-.048	-.059	-.077	
.830	-.042	-.036	-.034	-.038	-.041	-.057	-.083	
.871	-.004	-.002	-.000	-.009	-.013	-.022	-.038	
.954	-.084	-.077	-.071	-.068	-.069	-.087	-.116	

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station D

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/l	
M = 0.800; q = 308 lb/sq ft								M = 0.900; q = 350 lb/sq ft									
.166	-.012	-.002	.006	.019	.031	.058	.065	-.008	.000	.008	.017	.030	.061	.068	.166		
.277	-.031	-.025	-.005	.008	.015	.018	.028	-.028	-.025	-.005	.004	.006	.021	.033	.277		
.367	.032	.044	.095	.115	.139	.180	.217	.077	.072	.120	.132	.152	.199	.240	.367		
.387	-.143	-.078	-.024	.016	.062	.131	.204	-.103	-.053	-.009	.030	.069	.151	.227	.387		
.443	-.240	-.167	-.098	-.045	.015	.119	.224	-.238	-.173	-.105	-.046	.006	.124	.238	.443		
.498	-.231	-.166	-.103	-.051	.005	.099	.195	-.243	-.186	-.121	-.064	-.011	.099	.202	.498		
.553	-.205	-.155	-.100	-.050	.002	.115	.195	-.250	-.176	-.100	-.040	.008	.111	.190	.553		
.609	-.153	-.119	-.077	-.044	-.006	.057	.114	-.283	-.170	-.108	-.062	-.025	.052	.110	.609		
.664	-.081	-.067	-.045	-.022	.001	.037	.063	-.084	-.072	-.050	-.027	-.007	.040	.058	.664		
.719	-.028	-.017	-.012	-.006	.010	.025	.023	-.021	-.020	-.011	.000	.006	.031	.005	.719		
.774	.004	.006	.006	.017	.024	.032	.021	.001	.006	.010	.018	.020	.047	.001	.774		
.830	.011	.014	.014	.016	.020	.023	.010	.007	.013	.011	.015	.014	.031	-.005	.830		
.871	-.003	-.006	-.006	-.009	-.003	-.006	-.022	-.009	-.008	-.007	-.004	-.009	-.002	-.033	.871		
M = 0.940; q = 365 lb/sq ft								M = 0.980; q = 380 lb/sq ft									
.166	-.014	-.003	.008	.014	.029	.059	.076	-.005	.004	.012	.025	.040	.067	.075	.166		
.277	-.032	-.028	-.008	-.006	.001	.016	.037	-.006	-.020	-.001	.006	.007	.025	.052	.277		
.367	.095	.094	.128	.139	.158	.209	.256	.125	.138	.161	.173	.189	.232	.282	.367		
.387	-.077	-.035	.002	.039	.074	.158	.243	-.031	.003	.038	.071	.108	.186	.271	.387		
.443	-.218	-.167	-.106	-.051	.007	.126	.248	-.180	-.133	-.080	-.028	.028	.146	.271	.443		
.498	-.293	-.180	-.125	-.072	-.023	.096	.210	-.215	-.157	-.092	-.051	-.003	.109	.228	.498		
.553	-.237	-.230	-.141	-.078	-.013	.096	.196	-.256	-.210	-.150	-.109	-.060	.095	.210	.553		
.609	-.336	-.293	-.193	-.089	-.047	.033	.111	-.312	-.270	-.220	-.177	-.124	.021	.122	.609		
.664	-.309	-.108	-.047	-.032	-.015	.006	.044	-.349	-.301	-.246	-.181	-.097	.014	.055	.664		
.719	-.009	-.005	-.011	.000	.010	-.010	-.035	-.152	-.096	-.072	-.041	-.059	-.114	-.106	.719		
.774	.008	.007	.012	.018	.030	.034	-.022	-.008	.019	.034	.032	.020	-.040	-.116	.774		
.830	.001	.004	.009	.012	.021	.032	-.023	.006	.026	.037	.038	.034	.002	-.044	.830		
.871	-.013	-.014	-.010	-.012	-.006	-.007	-.049	.002	.011	.016	.010	.007	-.019	-.085	.871		
M = 1.040; q = 397 lb/sq ft								M = 1.105; q = 421 lb/sq ft									
.166	.037	.048	.063	.074	.090	.107	.111	.007	.021	.037	.052	.060	.081	.074	.166		
.277	.001	-.005	.023	.031	.033	.031	.086	-.015	-.015	.013	.026	.025	.024	.019	.277		
.367	.178	.137	.183	.198	.211	.278	.337	.071	-.010	.081	.079	.073	.038	.004	.367		
.387	.039	.071	.091	.117	.150	.242	.328	.011	.012	.049	.076	.095	.155	.269	.387		
.443	-.111	-.078	-.034	.018	.076	.201	.324	-.091	-.057	-.015	.037	.080	.189	.321	.443		
.498	-.142	-.105	-.047	-.005	.052	.163	.285	-.122	-.079	-.030	.022	.070	.179	.294	.498		
.553	-.189	-.149	-.095	-.050	.033	.147	.264	-.160	-.120	-.060	-.016	-.035	.140	.240	.553		
.609	-.239	-.201	-.161	-.117	-.061	.073	.179	-.198	-.159	-.116	-.065	-.024	.082	.213	.609		
.664	-.285	-.234	-.194	-.138	-.068	.049	.120	-.225	-.184	-.138	-.088	-.041	.076	.190	.664		
.719	-.162	-.127	-.109	-.096	-.070	-.062	-.047	-.144	-.121	-.098	-.073	-.055	-.008	.020	.719		
.774	-.076	-.053	-.028	-.034	-.040	-.067	-.078	-.060	-.052	-.044	-.031	-.032	-.033	-.032	.774		
.830	-.053	-.042	-.028	-.027	-.030	-.052	-.063	-.034	-.027	-.025	-.015	-.018	-.024	-.033	.830		
.871	-.064	-.076	-.078	-.082	-.098	-.142	-.165	-.050	-.062	-.066	-.070	-.084	-.109	-.139	.871		
M = 1.000; q = 457 lb/sq ft																	
.166	.027	.039	.052	.062	.063	.090	.085								.166		
.277	.015	.021	.018	.031	.035	.042	.034								.277		
.367	.058	.060	.065	.054	.048	.017	-.004								.367		
.387	.021	.041	.058	.073	.087	.120	.145								.387		
.443	-.066	-.029	.009	.049	.088	.196	.321								.443		
.498	-.088	-.049	.000	.044	.090	.195	.310								.498		
.553	-.115	-.080	-.030	.010	.060	.150	.260								.553		
.609	-.149	-.126	-.085	-.042	-.002	.085	.190								.609		
.664	-.197	-.164	-.119	-.077	-.031	.067	.194								.664		
.719	-.136	-.122	-.098	-.076	-.051	.000	.060								.719		
.774	-.066	-.060	-.048	-.043	-.035	-.020	-.013								.774		
.830	-.023	-.022	-.016	-.018	-.020	-.021	-.037								.830		
.871	-.051	-.050	-.061	-.072	-.085	-.115	-.143								.871		

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING

(a) Station A

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/l	
M = 0.800; q = 618 lb/sq ft								M = 0.900; q = 701 lb/sq ft									
.055	.066	.056	.042	.017				.111	.103	.100	.097		.104		.074	.056	
.166	.050	.027	.012	-.001	-.014	-.028	-.034	.047	.023	.009	-.006	.002	-.017	-.017	-.017	.166	
.277	.033	.010	-.004	-.016	-.027	-.036	-.030	.027	.003	-.010	-.023	-.011	-.020	.000	.000	.277	
.367	.171	.136	.104	.074	.043	.009	.011	.185	.147	.119	.090	.085	.059	.087	.367		
.387	.124	.082	.046	.007	-.026	-.093	-.155	.138	.094	.059	.025	.015	-.039	-.076	.387		
.415	.091	.042	-.001	-.047	-.094	-.140	-.299	.101	.050	.005	-.041	-.063	-.150	-.226	.415		
.443	.071	.018	-.028	-.076	-.130	-.236	-.363	.075	.018	-.032	-.083	-.113	-.217	-.308	.443		
.498	.054	-.001	-.050	-.102	-.155	-.246	-.341	.045	-.014	-.069	-.127	-.162	-.243	-.365	.498		
.553	.030	-.018	-.062	-.109	-.155	-.223	-.264	.009	-.048	-.104	-.173	-.232	-.323	-.432	.553		
.581	-.011	-.053	-.089	-.125	-.165	-.233	-.272	-.031	-.081	-.127	-.184	-.254	-.404	-.515	.581		
.609	.008	-.029	-.061	-.094	-.124	-.163	-.197	-.012	-.056	-.096	-.143	-.165	-.384	-.480	.609		
.636	-.005	-.035	-.058	-.082	-.104	-.134	-.170	-.021	-.056	-.083	-.116	-.119	-.404	-.484	.636		
.664	-.005	-.028	-.045	-.059	-.077	-.093	-.128	-.018	-.043	-.059	-.079	-.069	-.087	-.074	.664		
.692	.005	-.012	-.022	-.031	-.043	-.044	-.074	-.001	-.018	-.026	-.038	-.022	-.007	-.028	.692		
.719	.008	-.004	-.010	-.015	-.020	-.017	-.042	.005	-.007	-.011	-.016	.004	.017	-.013	.719		
.774															.774		
.830	.000	-.003	-.001	.003	.003	.010	.000	-.007	-.007	-.003	-.001	.022	.028	.004	.830		
.871	-.005	-.006	-.001	.005	.005	.007	.004	-.014	-.010	-.004	.000	.024	.020	.007	.871		
.954	.024	.029	.035	.042	.043	.042	.036	.023	.028	.037	.040	.065	.054	.048	.954		
M = 0.940; q = 730 lb/sq ft								M = 0.980; q = 758 lb/sq ft									
.055	.045	.020	.006	-.008	-.016	.060	.049	.112	.115	.102	.108	.089	.056	.044	.055		
.166	.025	-.002	-.015	-.028	-.032	-.027	.002	.051	.028	.012	.000	-.010	-.022	-.012	.166		
.277	.196	.158	.130	.103	.083	.073	.112	.028	.002	-.013	-.023	-.028	-.017	.019	.277		
.367	.150	.105	.071	.041	.018	-.020	-.050	.216	.182	.153	.130	.113	.106	.154	.367		
.387	.110	.057	.013	-.030	-.066	-.131	-.198	.172	.133	.100	.073	.051	.019	-.004	.387		
.415	.079	.020	-.030	-.075	-.121	-.202	-.277	.130	.080	.038	.001	-.033	-.089	-.150	.415		
.443	.043	-.019	-.077	-.125	-.178	-.256	-.349	.096	.042	-.008	-.049	-.093	-.163	-.230	.443		
.498	.007	-.047	-.105	-.188	-.264	-.312	-.404	.053	-.003	-.054	-.105	-.191	-.220	-.307	.498		
.553	-.005	-.073	-.150	-.200	-.241	-.326	-.418	-.016	-.080	-.130	-.174	-.219	-.292	-.369	.553		
.581	-.047	-.105	-.188	-.264	-.312	-.404	-.499	-.062	-.142	-.197	-.241	-.287	-.371	-.452	.581		
.609	-.029	-.082	-.141	-.249	-.302	-.395	-.489	-.058	-.130	-.188	-.241	-.290	-.365	-.446	.609		
.636	-.039	-.073	-.114	-.211	-.324	-.423	-.519	-.084	-.157	-.216	-.264	-.312	-.398	-.481	.636		
.664	-.033	-.053	-.068	-.072	-.244	-.445	-.505	-.091	-.166	-.234	-.288	-.337	-.422	-.505	.664		
.692	-.011	-.019	-.028	-.024	-.036	-.252	-.436	-.094	-.142	-.207	-.270	-.323	-.425	-.522	.692		
.719	.005	-.003	-.008	-.005	.005	-.002	-.020	-.052	-.031	-.037	-.084	-.129	-.291	-.453	.719		
.774															.774		
.830	-.010	-.008	-.005	.001	.009	.037	.003	-.023	.001	.022	.035	.040	.028	.012	.830		
.871	-.015	-.011	-.006	.000	.007	.024	.001	-.019	.001	.017	.030	.039	.042	.035	.871		
.954	.028	.032	.038	.042	.047	.055	.047	.031	.043	.053	.064	.074	.088	.091	.954		

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l
$M = 1.050; q = 7.34 \text{ lb/sq ft}$								$M = 1.175; q = 8.42 \text{ lb/sq ft}$							
.055	.149	.152	.130	.128	.124	.102	-.026	.069	.103	.028	.097	.078	.068	.054	.055
.166	.091	.073	.060	.044	.037	.021	.014	.063	.049	.038	.017	.002	-.004	-.016	.166
.277	.033	.024	.012	-.001	-.003	-.021	.056	.027	.014	.002	-.009	-.019	-.025	-.025	.277
.367	.260	.217	.188	.159	.152	.164	.215	.074	.06	.050	.038	.029	.050	.140	.367
.387	.226	.182	.150	.121	.105	.086	.062	.144	.103	.088	.071	.054	.041	.056	.387
.415	.186	.132	.088	.051	.025	-.018	-.083	.173	.133	.101	.065	.030	-.020	-.055	.415
.443	.151	.092	.043	-.003	-.036	-.089	-.159	.149	.093	.062	.017	-.019	-.078	-.112	.443
.498	.110	.052	-.007	-.056	-.097	-.147	-.235	.115	.051	.016	-.032	-.075	-.120	-.187	.498
.553	.034	-.022	-.073	-.120	-.158	-.217	-.294	.056	.000	-.040	-.088	-.127	-.179	-.231	.553
.581	-.027	-.085	-.142	-.185	-.219	-.290	-.376	-.006	-.058	-.095	-.143	-.186	-.246	-.293	.581
.609	-.015	-.073	-.136	-.188	-.226	-.290	-.369	-.005	-.062	-.104	-.152	-.194	-.242	-.287	.609
.636	-.044	-.101	-.161	-.211	-.247	-.321	-.408	-.022	-.082	-.125	-.173	-.211	-.273	-.330	.636
.664	-.064	-.118	-.180	-.235	-.269	-.346	-.430	-.039	-.090	-.130	-.183	-.226	-.287	-.342	.664
.692	-.066	-.113	-.172	-.229	-.266	-.356	-.449	-.042	-.097	-.135	-.182	-.228	-.294	-.365	.692
.719	-.078	-.092	-.112	-.153	-.173	-.274	-.416	-.050	-.091	-.122	-.160	-.197	-.266	-.358	.719
.774															.774
.830	-.074	-.063	-.047	-.048	-.049	-.070	-.073	-.053	-.050	-.047	-.041	-.041	-.032	-.027	.830
.871	-.092	-.077	-.062	-.057	-.054	-.069	-.053	-.071	-.060	-.050	-.038	-.033	-.025	-.017	.871
.954	-.127	-.118	-.090	-.064	-.051	-.038	-.047	-.068	-.070	-.058	-.039	-.022	-.004	.010	.954
$M = 1.000; q = 8.74 \text{ lb/sq ft}$															
.055															.055
.166	.075	.057	.046	.033	.021	-.001	-.003								.166
.277	.039	.022	.014	.006	.006	-.012	-.010								.277
.367	.080	.070	.056	.041	.037	.046	.072								.367
.387	.046	.035	.037	.040	.042	.033	.046								.387
.415	.175	.135	.111	.076	.045	-.002	-.042								.415
.443	.164	.121	.080	.044	.012	-.054	-.104								.443
.498	.143	.094	.049	.001	-.040	-.099	-.154								.498
.553	.083	.036	-.008	-.051	-.086	-.150	-.203								.553
.581	.018	-.026	-.062	-.107	-.144	-.206	-.270								.581
.609	.018	-.028	-.073	-.118	-.152	-.210	-.264								.609
.636	-.008	-.057	-.094	-.133	-.171	-.241	-.305								.636
.664	-.019	-.063	-.109	-.157	-.195	-.254	-.303								.664
.692	-.031	-.075	-.111	-.154	-.190	-.261	-.334								.692
.719	-.047	-.086	-.118	-.155	-.191	-.264	-.343								.719
.774															.774
.830	-.049	-.053	-.050	-.047	-.040	-.030	-.015								.830
.871	-.079	-.071	-.054	-.043	-.029	-.019	-.012								.871
.954	-.088	-.080	-.067	-.056	-.043	-.034	-.037								.954

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(c) Station C

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	x/l			
M = 0.800; q = 618 lb/sq ft								M = 0.900; q = 701 lb/sq ft											
.055	.049	.056	.062	.062	.046	.009	-.057	.054	.060	.066	.063	.080	.026	-.035	.055	.055			
.166	-.003	.004	.011	.009	-.004	-.043	-.110	-.003	.002	.007	.002	.011	-.035	-.093	.166	.166			
.277	-.019	-.013	-.006	-.008	-.020	-.061	-.122	-.019	-.017	-.014	-.018	-.007	-.048	-.098	.277	.277			
.353															.353	.353			
.367	.306	.307	.309	.303	.292	.251	.177	.331	.322	.318	.309	.328	.300	.261	.367	.367			
.692	.034	.032	.039	.046	.050	.058	.024	.031	.031	.039	.043	.069	.063	.007	.692	.692			
.719	.013	.011	.013	.020	.024	.031	.020	.016	.011	.015	.019	.046	.056	.033	.719	.719			
.774	.006	.004	.007	.010	.011	.021	.005	.001	.043	.008	.008	.035	.048	.009	.774	.774			
.830	.022	.024	.025	.025	.027	.045	.036	.017	.010	.021	.019	.046	.063	.039	.830	.830			
.871	.035	.032	.035	.037	.037	.051	.041	.030	.019	.033	.033	.056	.065	.048	.871	.871			
.954	.033	.034	.038	.041	.039	.037	.038	.033	.035	.040	.040	.059	.050	.050	.954	.954			
M = 0.940; q = 730 lb/sq ft								M = 0.980; q = 758 lb/sq ft											
.055	.059	.062	.067	.064	.044	.022	-.036	.071	.077	.081	.079	.077	.037	-.019	.055	.055			
.166	-.003	-.001	.003	.001	-.008	-.040	-.098	.001	.066	.012	.007	-.001	-.034	-.086	.166	.166			
.277	-.020	-.022	-.018	-.023	-.029	-.055	-.098	-.017	-.015	-.015	-.019	-.026	-.049	-.081	.277	.277			
.353															.353	.353			
.367	.344	.331	.326	.317	.320	.309	.278	.363	.350	.343	.335	.340	.333	.315	.367	.367			
.692	.006	.030	.041	.048	.041	-.034	.127	-.113	-.111	-.096	-.093	-.086	-.129	-.191	.692	.692			
.719	.023	.023	.020	.027	.039	.009	.034	-.085	-.018	-.028	-.037	-.055	-.141	-.179	.719	.719			
.774	.009	.008	.009	.013	.026	.042	-.013	-.014	.012	.034	.034	.019	-.045	-.149	.774	.774			
.830	.017	.019	.019	.020	.029	.063	.013	.013	.011	.046	.045	.041	.017	-.043	.830	.830			
.871	.031	.029	.032	.032	.041	.064	.033	.032	.016	.054	.057	.061	.052	.019	.871	.871			
.954	.037	.036	.040	.041	.043	.047	.046	.048	.015	.057	.061	.062	.070	.063	.954	.954			
M = 1.030; q = 794 lb/sq ft								M = 1.125; q = 842 lb/sq ft											
.055	.112	.116	.123	.119	.112	.080	.024	.082	.013	.094	.090	.081	.049	-.009	.055	.055			
.166	.041	.051	.058	.053	.046	.007	-.063	.019	.012	.037	.032	.017	-.017	-.087	.166	.166			
.277	-.007	.007	.012	.007	.004	-.041	-.049	-.006	.017	.009	.007	-.008	-.042	-.115	.277	.277			
.353															.353	.353			
.367	.392	.368	.356	.343	.353	.372	.363	.272	.212	.270	.265	.257	.226	.139	.367	.367			
.692	-.094	-.078	-.075	-.073	-.062	-.073	-.131	-.066	-.010	-.057	-.053	-.050	-.036	-.077	.692	.692			
.719	-.092	-.074	-.070	-.072	-.069	-.096	-.130	-.065	-.018	-.057	-.056	-.056	-.054	-.068	.719	.719			
.774	-.085	-.058	-.038	-.039	-.049	-.089	-.129	-.059	-.014	-.044	-.043	-.047	-.056	-.081	.774	.774			
.830	-.045	-.039	-.023	-.030	-.032	-.076	-.102	-.029	-.012	-.016	-.023	-.025	-.045	-.064	.830	.830			
.871	-.024	-.029	-.023	-.027	-.030	-.052	-.062	-.005	-.015	-.005	-.007	-.011	-.015	-.028	.871	.871			
.954	-.105	-.095	-.078	-.070	-.075	-.085	-.107	-.052	-.019	-.051	-.053	-.058	-.063	-.056	.954	.954			
M = 1.200; q = 873 lb/sq ft																			
.055	.098	.103	.111	.107	.099	.065	-.002								.055	.055			
.166	.031	.037	.045	.043	.029	-.013	-.081								.166	.166			
.277	.007	.013	.016	.012	.005	-.028	-.109								.277	.277			
.353															.353	.353			
.367	.257	.259	.260	.257	.249	.217	.123								.367	.367			
.692	-.063	-.061	-.053	-.052	-.042	-.034	-.056								.692	.692			
.719	-.070	-.066	-.060	-.061	-.056	-.055	-.046								.719	.719			
.774	-.065	-.059	-.046	-.047	-.050	-.062	-.088								.774	.774			
.830	-.036	-.035	-.023	-.033	-.037	-.057	-.083								.830	.830			
.871	-.007	-.010	-.006	-.011	-.013	-.022	-.045								.871	.871			
.954	-.093	-.082	-.073	-.072	-.073	-.088	-.114								.954	.954			

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station D

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l
M = 0.800; q = 618 lb/sq ft								M = 0.900; q = 701 lb/sq ft								
.166	.016	.026	.039	.051	.054	.066	.074	.016	.025	.037	.041	.072	.078	.091	.166	
.277	-.011	-.003	.008	.019	.022	.028	.036	-.010	-.006	.003	.006	.035	.037	.052	.277	
.367	.024	.055	.091	.121	.148	.185	.225	.061	.084	.114	.134	.178	.215	.258	.367	
.387	-.139	-.082	-.029	.019	.054	.129	.200	-.106	-.062	-.016	.026	.085	.154	.234	.387	
.443	-.237	-.164	-.100	-.040	.010	.114	.220	-.238	-.174	-.108	-.052	.024	.128	.241	.443	
.498	-.228	-.163	-.103	-.046	-.000	.099	.196	-.244	-.187	-.123	-.068	.007	.104	.208	.498	
.553	-.204	-.149	-.097	-.049	-.008	.077	.156	-.296	-.228	-.143	-.084	-.013	.076	.165	.553	
.609	-.151	-.115	-.076	-.038	-.008	.058	.115	-.288	-.218	-.143	-.086	-.007	.059	.122	.609	
.664	-.081	-.064	-.041	-.019	-.003	.038	.084	-.084	-.073	-.048	-.030	.011	.043	.065	.664	
.719	-.021	-.017	-.006	.007	.010	.029	.030	-.019	-.017	-.004	.001	.030	.043	.026	.719	
.774	.007	.009	.016	.023	.023	.037	.028	.005	.008	.014	.019	.046	.056	.026	.774	
.830	.017	.018	.023	.027	.028	.032	.025	.011	.014	.019	.021	.043	.050	.024	.830	
.871	.001	-.003	-.001	.001	-.002	-.003	-.017	-.006	-.008	-.005	-.007	.013	.009	-.015	.871	
M = 0.940; q = 730 lb/sq ft								M = 0.980; q = 758 lb/sq ft								
.166	.015	.021	.031	.040	.052	.068	.083	.022	.030	.038	.047	.059	.077	.096	.166	
.277	-.009	-.011	-.003	.004	.011	.028	.046	-.004	-.003	-.000	.006	.014	.034	.061	.277	
.367	.085	.100	.124	.145	.170	.216	.261	.117	.132	.151	.172	.193	.239	.289	.367	
.387	-.079	-.043	-.002	.035	.075	.154	.237	-.041	-.007	.028	.063	.099	.177	.266	.387	
.443	-.221	-.166	-.107	-.053	.005	.121	.238	-.191	-.140	-.085	-.033	.022	.137	.260	.443	
.498	-.239	-.182	-.127	-.074	-.023	.091	.203	-.217	-.161	-.106	-.056	-.008	.101	.220	.498	
.553	-.285	-.236	-.184	-.117	-.056	.054	.154	-.261	-.211	-.143	-.088	-.037	.052	.167	.553	
.609	-.333	-.289	-.201	-.091	-.046	.030	.104	-.312	-.268	-.218	-.175	-.127	.013	.143	.609	
.664	-.302	-.211	-.046	-.031	-.018	.003	.038	-.355	-.303	-.246	-.188	-.108	-.018	.046	.664	
.719	-.003	-.003	-.001	.007	.016	-.001	-.031	-.145	-.097	-.049	-.037	-.081	-.114	-.167	.719	
.774	.013	.011	.016	.023	.034	.045	-.011	-.001	.025	.041	.038	.023	-.035	-.121	.774	
.830	.009	.010	.016	.022	.030	.047	-.003	.013	.033	.044	.046	.042	.017	-.021	.830	
.871	-.007	-.011	-.006	-.006	-.006	.001	-.041	.006	.014	.016	.014	.008	-.010	-.070	.871	
M = 1.030; q = 794 lb/sq ft								M = 1.125; q = 842 lb/sq ft								
.166	.063	.074	.085	.093	.105	.116	.119	.034	.049	.060	.071	.079	.090	.099	.166	
.277	.003	.018	.028	.033	.044	.043	.091	.004	.014	.021	.031	.031	.037	.031	.277	
.367	.167	.173	.183	.197	.224	.286	.334	.072	.078	.081	.086	.076	.048	.026	.367	
.387	.029	.053	.082	.109	.149	.235	.312	-.006	.025	.042	.068	.089	.152	.265	.387	
.443	-.117	-.084	-.037	.013	.069	.193	.306	-.091	-.053	-.022	.036	.079	.186	.313	.443	
.498	-.147	-.108	-.057	-.005	.046	.155	.267	-.124	-.073	-.036	.020	.071	.178	.289	.498	
.553	-.189	-.149	-.105	-.062	-.011	.101	.213	-.151	-.101	-.065	-.016	.027	.126	.243	.553	
.609	-.239	-.205	-.158	-.118	-.064	.061	.163	-.195	-.152	-.115	-.061	-.019	.083	.203	.609	
.664	-.289	-.233	-.193	-.142	-.075	.043	.105	-.224	-.173	-.138	-.088	-.042	.074	.181	.664	
.719	-.163	-.128	-.105	-.084	-.069	-.063	-.053	-.139	-.113	-.097	-.073	-.051	-.002	.024	.719	
.774	-.075	-.050	-.026	-.031	-.039	-.070	-.085	-.059	-.045	-.041	-.032	-.031	-.028	-.035	.774	
.830	-.050	-.040	-.023	-.020	-.021	-.042	-.041	-.029	-.019	-.015	-.009	-.012	-.016	-.026	.830	
.871	-.065	-.075	-.075	-.085	-.097	-.142	-.180	-.053	-.057	-.065	-.073	-.087	-.111	-.143	.871	
M = 1.200; q = 873 lb/sq ft																
.166	.045	.056	.068	.078	.084	.096	.105								.166	
.277	.019	.025	.033	.035	.040	.047	.043								.277	
.367	.062	.064	.068	.066	.062	.033	.014								.367	
.387	.006	.028	.046	.063	.080	.112	.125								.387	
.443	-.077	-.042	-.004	.036	.083	.183	.324								.443	
.498	-.096	-.055	-.008	.035	.084	.188	.312								.498	
.553	-.115	-.078	-.034	.007	.051	.149	.257								.553	
.609	-.152	-.122	-.073	-.033	.006	.090	.197								.609	
.664	-.200	-.161	-.115	-.076	-.041	.050	.189								.664	
.719	-.141	-.120	-.095	-.075	-.053	-.000	.067								.719	
.774	-.071	-.062	-.051	-.045	-.036	-.023	-.013								.774	
.830	-.024	-.020	-.013	-.014	-.014	-.022	-.034								.830	
.871	-.053	-.056	-.064	-.079	-.087	-.115	-.157								.871	

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Concluded

(e) Station E

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	x/l							
M = 0.800; q = 618 lb/sq ft								M = 0.900; q = 701 lb/sq ft															
.055	.028	.044	.065	.090	.115	.173	.242	.039	.047	.069	.093	.137	.189	.261	.055								
.166	-.007	.000	.015	.031	.047	.093	.151	-.009	-.003	.011	.024	.063	.102	.165	.166								
.277	-.022	-.017	-.006	.012	.025	.070	.133	-.020	-.021	-.009	.000	.037	.076	.143	.277								
.367	-.020	.002	.031	.059	.084	.148	.224	.012	.026	.048	.067	.113	.167	.248	.367								
.387	-.112	-.076	-.039	.000	.032	.114	.203	-.084	-.058	-.027	.003	.059	.130	.228	.387								
.443	-.207	-.150	-.098	-.047	-.004	.090	.193	-.214	-.161	-.106	-.059	.011	.104	.213	.443								
.498	-.209	-.152	-.098	-.044	-.003	.093	.186	-.232	-.182	-.120	-.068	.002	.098	.200	.498								
.553	-.188	-.139	-.089	-.040	-.002	.082	.163	-.283	-.213	-.133	-.077	-.007	.083	.172	.553								
.609	-.139	-.106	-.067	-.030	-.000	.068	.128	-.271	-.162	-.101	-.058	.002	.069	.135	.609								
.664	-.060	-.042	-.016	.009	.027	.075	.111	-.067	-.055	-.026	-.003	.041	.080	.113	.664								
.719	-.037	-.031	-.020	-.006	.002	.027	.038	-.033	-.032	-.020	-.011	.022	.039	.030	.719								
.774	-.000	-.000	.006	.013	.017	.031	.030	-.003	-.000	.004	.010	.037	.050	.022	.774								
.830	.010	.006	.012	.016	.015	.025	.024	.003	.001	.006	.010	.033	.041	.020	.830								
.871	-.020	-.023	-.025	-.033	-.034	-.044	-.044	-.027	-.023	-.030	-.034	-.037	-.042	-.048	.871								
.954	.061	.056	.057	.056	.048	.043	.033	.060	.057	.054	.072	.059	.048	.048	.954								
M = 0.940; q = 750 lb/sq ft								M = 0.980; q = 758 lb/sq ft															
.055	.048	.060	.078	.096	.122	.184	.256	.059	.075	.091	.110	.135	.197	.271	.055								
.166	-.007	-.006	.009	.024	.044	.092	.155	-.004	.004	.015	.031	.050	.098	.165	.166								
.277	-.017	-.023	-.013	-.001	.016	.065	.134	-.011	-.015	-.010	.003	.018	.069	.146	.277								
.367	.034	.041	.058	.076	.102	.165	.247	.063	.071	.084	.103	.125	.183	.266	.367								
.387	-.060	-.042	-.017	.010	.044	.128	.227	-.023	-.008	.013	.039	.068	.149	.252	.387								
.443	-.200	-.156	-.109	-.061	-.011	.096	.210	-.171	-.130	-.085	-.041	.006	.114	.232	.443								
.498	-.230	-.176	-.126	-.075	-.025	.085	.193	-.209	-.156	-.104	-.056	-.014	.095	.212	.498								
.553	-.270	-.227	-.174	-.109	-.046	.062	.159	-.243	-.209	-.151	-.107	-.062	.057	.174	.553								
.609	-.312	-.270	-.192	-.086	-.036	.042	.119	-.294	-.254	-.200	-.159	-.111	.026	.129	.609								
.664	-.297	-.106	-.026	-.007	.014	.044	.086	-.310	-.265	-.234	-.156	-.086	.023	.095	.664								
.719	-.010	-.016	-.015	-.006	.003	-.000	-.017	-.184	-.123	-.058	-.039	-.053	-.098	-.070	.719								
.774	.010	.003	.008	.013	.025	.034	-.014	.006	.025	.037	.032	.013	-.040	-.111	.774								
.830	.004	.000	.005	.010	.017	.036	-.009	.016	.027	.033	.035	.030	.007	-.013	.830								
.871	-.026	-.031	-.032	-.034	-.035	-.032	-.072	-.004	-.003	-.005	-.014	-.024	-.045	-.087	.871								
.954	.064	.059	.060	.059	.056	.051	.038	.081	.083	.076	.073	.068	.064	.041	.954								
M = 1.050; q = 794 lb/sq ft								M = 1.125; q = 842 lb/sq ft															
.055	.101	.115	.132	.149	.172	.237	.307	.072	.093	.104	.127	.150	.212	.280	.055								
.166	.037	.047	.065	.078	.096	.137	.189	.008	.023	.035	.058	.075	.121	.177	.166								
.277	-.006	.005	.018	.025	.047	.076	.173	-.007	.002	.009	.026	.038	.079	.125	.277								
.367	.120	.115	.121	.131	.156	.231	.311	-.011	-.011	-.009	-.001	.004	.032	.067	.367								
.387	.045	.049	.067	.083	.116	.205	.298	.001	.009	.008	.011	.012	.030	.134	.387								
.443	-.098	-.074	-.035	.006	.054	.170	.278	-.073	-.042	-.024	.020	.059	.161	.281	.443								
.498	-.139	-.107	-.055	-.008	.041	.149	.259	-.109	-.066	-.030	.026	.069	.171	.281	.498								
.553	-.175	-.138	-.096	-.051	-.004	.109	.222	-.137	-.093	-.058	-.007	.034	.132	.251	.553								
.609	-.222	-.188	-.143	-.100	-.048	.073	.178	-.178	-.123	-.098	-.044	.001	.101	.218	.609								
.664	-.244	-.197	-.156	-.106	-.042	.081	.152	-.183	-.133	-.102	-.051	-.005	.107	.221	.664								
.719	-.225	-.170	-.141	-.107	-.074	-.045	-.015	-.208	-.163	-.137	-.096	-.061	.024	.071	.719								
.774	-.074	-.056	-.032	-.042	-.048	-.073	-.071	-.059	-.053	-.050	-.040	-.037	-.024	-.012	.774								
.830	-.057	-.049	-.034	-.029	-.029	-.044	-.045	-.029	-.027	-.024	-.020	-.020	-.010	.003	.830								
.871	-.084	-.101	-.104	-.117	-.129	-.156	-.162	-.066	-.081	-.092	-.100	-.107	-.107	-.105	.871								
.954	-.031	-.042	-.044	-.058	-.081	-.103	-.122	.033	.001	-.014	-.037	-.056	-.071	-.075	.954								
M = 1.200; q = 873 lb/sq ft																							
.055	.085	.103	.121	.137	.161	.225	.303									.055							
.166	.025	.036	.051	.067	.086	.131	.193									.166							
.277	.009	.015	.026	.034	.047	.089	.144									.277							
.367	-.008	-.006	-.006	.002	.015	.034	.076									.367							
.387	-.005	-.003	-.001	-.004	.001	.026	.070									.387							
.443	-.055	-.025	.003	.030	.069	.159	.289									.443							
.498	-.094	-.053	-.009	.033	.079	.177	.301									.498							
.553	-.110	-.072	-.028	.013	.057	.152	.268									.553							
.609	-.146	-.125	-.080	-.039	.010	.109	.220									.609							
.664	-.166	-.125	-.076	-.028	.023	.089	.225									.664							
.719	-.196	-.165	-.125	-.093	-.055	.025	.122									.719							
.774	-.075	-.075	-.068	-.062	-.049	-.020	.023									.774							
.830	-.022	-.019	-.014	-.015	-.011	.008	.023									.830							
.871	-.067	-.078	-.083	-.090	-.091	-.093	-.091									.871							
.954	-.029	-.037	-.045	-.058	-.067	-.078	-.087									.954							

TABLE VII.- WING SECTION DATA

α , deg	$\frac{y}{b/2} = 0.12$						$\frac{y}{b/2} = 0.25$						$\frac{y}{b/2} = 0.40$					
	c_n		c_m		$\Delta\alpha$, deg		c_n		c_m		$\Delta\alpha$, deg		c_n		c_m			
	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm
M = 0.800																		
-4	-0.2516	-0.2531	0.0162	0.0160	0.03	0.06	-0.2869	-0.2922	-0.0044	-0.0019	0.07	0.14	-0.3645	-0.3712	-0.0245	-0.0218		
-2	-0.1457	-0.1567	0.0040	0.0024	0.02	0.05	-0.1682	-0.1572	-0.0082	-0.0073	0.05	0.10	-0.2265	-0.2065	-0.0245	-0.0217		
0	-0.0110	-0.0225	-0.0124	-0.0110	0.01	0.02	-0.0111	-0.0221	-0.0153	-0.0132	0.02	0.04	-0.0334	-0.0485	-0.0270	-0.0266		
2	0.0861	0.0920	-0.0239	-0.0238	-0.01	-0.01	0.0931	0.1039	-0.0211	-0.0215	-0.01	-0.03	0.0822	0.0942	-0.0337	-0.0335		
4	0.2000	0.2030	-0.0551	-0.0555	-0.02	-0.04	0.2223	0.2270	-0.0291	-0.0291	-0.04	-0.06	0.2428	0.2402	-0.0389	-0.0387		
8	0.4348	0.4372	-0.0980	-0.0995	-0.04	-0.08	0.4714	0.4755	-0.0432	-0.0432	-0.09	-0.19	0.5355	0.5379	-0.0410	-0.0432		
12	0.6732	0.6734	-0.0719	-0.0728	-0.06	-0.11	0.7408	0.7556	-0.0542	-0.0651	-0.12	-0.24	0.9909	0.9618	-0.1040	-0.0799		
M = 0.900																		
-4	-0.2692	-0.2799	0.0277	0.0297	0.04	0.08	-0.3011	-0.3200	0.0055	0.0075	0.08	0.17	-0.3812	-0.4113	-0.0182	-0.0129		
-2	-0.1538	-0.1486	0.0090	0.0079	0.03	0.06	-0.1766	-0.1673	-0.0046	-0.0029	0.06	0.13	-0.2409	-0.2260	-0.0222	-0.0232		
0	-0.0172	-0.0221	-0.0120	-0.0110	0.01	0.02	-0.0187	-0.0194	-0.0158	-0.0141	0.02	0.04	-0.0390	-0.0436	-0.0302	-0.0293		
2	0.0953	0.0985	-0.0286	-0.0283	-0.01	-0.02	0.1074	0.1129	-0.0258	-0.0251	-0.02	-0.04	0.1000	0.1056	-0.0386	-0.0383		
4	0.2186	0.2214	-0.0454	-0.0465	-0.02	-0.05	0.2445	0.2484	-0.0368	-0.0373	-0.06	-0.11	0.2667	0.2618	-0.0451	-0.0457		
8	0.4889	0.4900	-0.0899	-0.0903	-0.06	-0.12	0.5395	0.5499	-0.0732	-0.0738	-0.13	-0.27	0.6099	0.6171	-0.0666	-0.0659		
12	0.7053	0.7254	-0.1092	-0.1136	-0.07	-0.14	0.7997	0.7948	-0.0981	-0.1013	-0.15	-0.30	0.9506	0.9756	-0.1163	-0.1040		
M = 0.940																		
-4	-0.3000	-0.3095	0.0548	0.0565	0.04	0.09	-0.3252	-0.3364	0.0243	0.0242	0.10	0.20	-0.4172	-0.4345	0.0056	0.0098		
-2	-0.1713	-0.1707	0.0237	0.0238	0.03	0.07	-0.1946	-0.1860	0.0069	0.0089	0.08	0.15	-0.2630	-0.2540	-0.0120	-0.0128		
0	-0.0234	-0.0236	-0.0106	-0.0099	0.01	0.02	-0.0244	-0.0218	-0.0144	-0.0132	0.02	0.04	-0.0462	-0.0452	-0.0320	-0.0302		
2	0.0975	0.1063	-0.0343	-0.0348	-0.01	-0.02	0.1111	0.1265	-0.0319	-0.0333	-0.02	-0.05	0.0995	0.1189	-0.0438	-0.0449		
4	0.2479	0.2445	-0.0680	-0.0671	-0.03	-0.06	0.2704	0.2700	-0.0561	-0.0542	-0.07	-0.14	0.3013	0.2972	-0.0680	-0.0673		
8	0.5212	0.5074	-0.1201	-0.1184	-0.07	-0.14	0.5578	0.5504	-0.0951	-0.0915	-0.16	-0.31	0.6462	0.6291	-0.0966	-0.0928		
12	0.7326	0.7416	-0.1403	-0.1434	-0.08	-0.15	0.8262	0.7979	-0.1241	-0.1156	-0.17	-0.33	0.9534	0.9292	-0.1319	-0.1184		
M = 0.960																		
-4	-0.2811	-0.2826	0.0486	0.0481	0.05	0.11	-0.3332	-0.3336	0.0378	0.0384	0.12	0.23	-0.4309	-0.4229	0.0263	0.0288		
-2	-0.1497	-0.1513	0.0195	0.0195	0.04	0.07	-0.1804	-0.1753	0.0132	0.0142	0.09	0.17	-0.2489	-0.2428	-0.0017	-0.0027		
0	-0.0254	-0.0262	-0.0080	-0.0074	0.01	0.02	-0.0262	-0.0261	-0.0115	-0.0103	0.02	0.05	-0.0529	-0.0520	-0.0303	-0.0281		
2	0.0957	0.0895	-0.0335	-0.0313	-0.01	-0.02	0.1128	0.1077	-0.0341	-0.0318	-0.03	-0.06	0.1175	0.1057	-0.0579	-0.0551		
4	0.2196	0.2182	-0.0605	-0.0599	-0.04	-0.07	0.2565	0.2550	-0.0615	-0.0601	-0.09	-0.15	0.2938	0.2822	-0.0844	-0.0815		
8	0.4762	0.4729	-0.1097	-0.1103	-0.08	-0.15	0.5314	0.5335	-0.1016	-0.1017	-0.18	-0.35	0.6185	0.6103	-0.1105	-0.1101		
12	0.7287	0.7236	-0.1503	-0.1489	-0.11	-0.22	0.8219	0.8016	-0.1467	-0.1373	-0.25	-0.49	0.9274	0.9323	-0.1399	-0.1397		
M = 1.050																		
-4	-0.2578	-0.2587	0.0416	0.0413	0.06	0.11	-0.3013	-0.3041	0.0310	0.0306	0.13	0.26	-0.3931	-0.3976	0.0251	0.0252		
-2	-0.1477	-0.1431	0.0183	0.0172	0.04	0.07	-0.1766	-0.1639	0.0111	0.0109	0.09	0.17	-0.2416	-0.2260	-0.0038	-0.0072		
0	-0.0237	-0.0268	-0.0090	-0.0073	0.01	0.02	-0.0229	-0.0249	-0.0126	-0.0104	0.03	0.05	-0.0555	-0.0531	-0.0306	-0.0290		
2	0.0921	0.0884	-0.0324	-0.0311	-0.01	-0.03	0.1125	0.1112	-0.0357	-0.0347	-0.03	-0.06	0.1122	0.1069	-0.0558	-0.0548		
4	0.2077	0.2074	-0.0570	-0.0560	-0.04	-0.07	0.2440	0.2442	-0.0589	-0.0576	-0.08	-0.16	0.2749	0.2686	-0.0800	-0.0791		
8	0.4933	0.4495	-0.1055	-0.1046	-0.08	-0.15	0.5084	0.5093	-0.1004	-0.1003	-0.18	-0.34	0.5915	0.5860	-0.1107	-0.1098		
12	0.6953	0.6915	-0.1449	-0.1440	-0.12	-0.22	0.7775	0.7720	-0.1392	-0.1361	-0.27	-0.49	0.8886	0.8986	-0.1386	-0.1421		
M = 1.125																		
-4	-0.2381	-0.2295	0.0353	0.0325	0.06	0.11	-0.2812	-0.2665	0.0305	0.0296	0.13	0.25	-0.3625	-0.3514	0.0250	0.0164		
-2	-0.1283	-0.1084	0.0121	0.0077	0.04	0.07	-0.1479	-0.1194	0.0073	0.0037	0.09	0.15	-0.2077	-0.1754	-0.0076	-0.0152		
0	-0.0232	-0.0202	-0.0094	-0.0101	0.01	0.02	-0.0207	-0.0167	-0.0153	-0.0136	0.03	0.05	-0.0510	-0.0533	-0.0327	-0.0348		
2	0.0865	0.1031	-0.0311	-0.0339	-0.01	-0.03	0.1065	0.1258	-0.0345	-0.0368	-0.03	-0.07	0.1034	0.1236	-0.0560	-0.0594		
4	0.1944	0.2116	-0.0525	-0.0549	-0.03	-0.07	0.2289	0.2490	-0.0551	-0.0582	-0.08	-0.17	0.2565	0.2746	-0.0783	-0.0814		
8	0.4221	0.4291	-0.0960	-0.0967	-0.08	-0.15	0.4797	0.4861	-0.0957	-0.0966	-0.18	-0.34	0.5626	0.5687	-0.1168	-0.1155		
12	0.6481	0.6494	-0.1380	-0.1372	-0.11	-0.22	0.7265	0.7344	-0.1340	-0.1307	-0.26	-0.50	0.8498	0.8593	-0.1490	-0.1491		
M = 1.200																		
-4	-0.2147	-0.2223	0.0298	0.0308	0.05	0.11	-0.2430	-0.2548	0.0229	0.0265	0.11	0.25	-0.3121	-0.3308	0.0151	0.0114		
-2	-0.1234	-0.1231	0.0110	0.0113	0.04	0.07	-0.1450	-0.1398	0.0070	0.0067	0.09	0.17	-0.2029	-0.2047	-0.0078	-0.0109		
0	-0.0209	-0.0215	-0.0084	-0.0074	0.01	0.03	-0.0208	-0.0172	-0.0138	-0.0146	0.03	0.06	-0.0552	-0.0551	-0.0291	-0.0311		
2	0.0777	0.0781	-0.0271	-0.0266	-0.01	-0.02	0.0991	0.1022	-0.0344	-0.0348	-0.02	-0.04	0.0907	0.0927	-0.0504	-0.0510		
4	0.1763	0.1811	-0.0464	-0.0465	-0.03	-0.06	0.2143	0.2159	-0.0592	-0.0530	-0.07	-0.14	0.2267	0.2319	-0.0698	-0.0703		
8	0.3882	0.3935	-0.0857	-0.0853	-0.07	-0.14	0.4523	0.4516	-0.0934	-0.0905	-0.17	-0.32	0.5141	0.5134	-0.1099	-0.1091		
12	0.6063	0.6206	-0.1287	-0.1286	-0.11	-0.22	0.6804	0.7067	-0.1299	-0.1314	-0.25	-0.50	0.8052	0.8269	-0.1510	-0.1514		

TABLE VII.- WING SECTION DATA - Concluded

α , deg	$\frac{y}{b/2} = 0.60$								$\frac{y}{b/2} = 0.80$								$\frac{y}{b/2} = 0.95$							
	$\Delta\alpha$, deg		c_n		c_m		$\Delta\alpha$, deg		c_n		c_m		$\Delta\alpha$, deg		c_n		c_m							
	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm						
	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm						
M = 0.800																								
-4	0.15	0.31	-0.5389	-0.5353	0.0204	0.0192	0.24	0.51	-0.4765	-0.5071	0.0634	0.0743	0.27	0.57	-0.1680	-0.1696	-0.0056	-0.0072						
-2	.13	.25	-.5403	-.5164	-.0120	-.0179	.24	.44	-.5133	-.4981	.0864	.0778	.27	.52	-.1599	-.1670	-.0096	-.0069						
0	.04	.09	-.0853	-.1065	-.0297	-.0303	.06	.10	-.2065	-.2292	-.0293	-.0176	.07	-.02	-.2430	-.2009	.0162	-.0620						
2	-.04	-.06	.0633	.0782	-.0350	-.0356	-.08	-.19	.0150	.0500	-.0524	-.0387	-.14	-.31	.0116	.0084	-.0448	-.0470						
4	-.11	-.21	.2632	.2414	-.0404	-.0407	-.20	-.39	.2254	.2155	-.0497	-.0484	-.27	-.54	.1791	.1751	-.0475	-.0466						
8	-.22	-.46	.6025	.5758	-.0476	-.0504	-.38	-.79	.5792	.5875	-.0959	-.0896	-.48	-1.00	.3528	.4001	-.0473	-.0516						
12	-.28	-.56	.7852	.8282	-.1375	-.1415	-.47	-.91	.5482	.5390	-.0906	-.0877	-.57	-1.12	.3631	.3593	-.0569	-.0569						
M = 0.900																								
-4	0.17	0.38	-0.5464	-0.5865	0.0130	0.0215	0.27	0.63	-0.4758	-0.5350	0.0625	0.0183	0.31	0.71	-0.1946	-0.1861	-0.0045	-0.0073						
-2	.16	.51	-.5616	-.5378	-.0112	-.0135	.29	.57	-.5410	-.5325	.0982	.0926	.34	.66	-.1680	-.1755	-.0113	-.0085						
0	.06	.09	-.0991	-.1035	-.0311	-.0319	.07	.09	-.2261	-.2303	-.0259	-.0159	.09	-.06	-.2478	-.1845	.0187	-.0743						
2	-.06	-.12	.0822	.0913	-.0388	-.0393	-.12	-.26	.0392	.0496	-.0418	-.0461	-.20	-.42	.0270	.0217	-.0510	-.0539						
4	-.14	-.25	.2746	.2704	-.0434	-.0448	-.26	-.46	.2637	.2468	-.0537	-.0545	-.36	-.64	.2164	.2018	-.0489	-.0500						
8	-.32	-.64	.6574	.6865	-.0452	-.0412	-.50	-1.01	.7573	.7705	-.0536	-.0468	-.64	-1.28	.5216	.5655	-.0813	-.0804						
12	-.35	-.70	.8269	.8599	-.1378	-.1379	-.59	-1.17	.6089	.6080	-.1058	-.1091	-.73	-1.46	.4137	.4074	-.0675	-.0672						
M = 0.940																								
-4	0.22	0.48	-0.6059	-0.6341	0.0573	0.0581	0.36	0.77	-0.5204	-0.5588	0.0708	0.0834	0.40	0.86	-0.2238	-0.2187	-0.0075	-0.0091						
-2	.20	.40	-.5685	-.5516	.0066	.0010	.37	.77	-.5620	-.5889	.1035	.1125	.47	.97	-.2697	-.2652	.0227	.0217						
0	.06	.09	-.1032	-.1062	-.0328	-.0341	.09	.09	-.2446	-.2355	-.0210	-.0120	.12	-.09	-.2598	-.1773	.0212	-.0870						
2	-.06	-.14	.0813	.1060	-.0386	-.0409	-.12	-.30	.0358	.0599	-.0357	-.0438	.20	-.48	.0239	.0363	-.0500	-.0557						
4	-.18	-.34	.3137	.3115	-.0556	-.0558	-.31	-.60	.3092	.2919	-.0570	-.0570	-.41	-.80	.2407	.2293	-.0521	-.0507						
8	-.40	-.80	.7498	.7252	-.0882	-.0904	-.65	-1.34	.8712	.8112	-.1127	-.0840	-.82	-1.69	.4877	.6837	-.0700	-.0865						
12	-.40	-.81	.8763	.8977	-.1432	-.1551	-.67	-1.57	.6771	.6852	-.1227	-.1252	-.84	-1.71	.4472	.4572	-.0722	-.0739						
M = 0.980																								
-4	0.29	0.58	-0.6349	-0.6503	0.0826	0.0800	0.48	0.97	-0.6172	-0.6190	0.0933	0.0960	0.56	1.12	-0.3004	-0.2942	0.0074	0.0061						
-2	.24	.46	-.5687	-.5555	.0215	.0131	.43	.84	-.6333	-.6234	.114	.1019	.53	1.02	-.2626	-.2791	.0142	.0155						
0	.10	.12	-.1105	-.1181	-.0343	-.0357	.04	.12	-.2406	-.2470	-.056	-.0370	.04	0	-.2293	-.2612	.0212	-.0430						
2	-.05	-.12	.1135	.1018	-.0484	-.0637	-.24	-.42	.0777	.0548	-.086	-.0807	-.35	-.62	.0501	.0221	-.0477	-.0460						
4	-.25	-.45	.3290	.3145	-.0952	-.0909	-.51	-.80	.3612	.3037	-.125	-.0950	-.73	-1.03	.3559	.2271	-.1123	-.0441						
8	-.49	-.94	.7318	.7087	-.1251	-.1259	-.95	-1.77	.8673	.8020	-.170	-.1582	-1.26	-2.43	.8545	.8135	-.1585	-.1692						
12	-.67	-1.28	1.1514	1.1175	-.1985	-.1818	-1.21	-2.30	1.1449	1.1365	-.213	-.2131	-1.61	-3.00	1.0529	.9468	-.1907	-.1357						
M = 1.030																								
-4	0.35	0.70	-0.5774	-0.5866	0.0781	0.0798	0.62	1.23	-0.7288	-0.7401	0.117	0.1229	0.75	1.50	-0.4285	-0.4080	0.0351	0.0319						
-2	.24	.49	-.5574	-.5296	.0210	.0158	.43	.91	-.6098	-.5755	.0853	.0763	.51	1.18	-.5318	-.4659	.0093	.0514						
0	.08	.11	-.1082	-.1146	-.0349	-.0343	.11	.05	-.2723	-.2595	-.0443	-.0522	.09	-.26	-.3849	-.2546	-.0115	-.1123						
2	-.10	-.20	.1090	.1112	-.0714	-.0706	-.26	-.15	.0405	.0312	-.096	-.0962	-.47	-.95	.0152	-.0086	-.1241	-.1368						
4	-.24	-.46	.3117	.3040	-.1001	-.0966	-.49	-.95	.2995	.2809	-.117	-.1181	-.73	-1.43	.2804	.2520	-.1276	-.1256						
8	-.49	-.93	.7084	.6852	-.1360	-.1324	-.92	-1.73	.8016	.7380	-.160	-.1582	-1.26	-2.43	.7757	.7269	-.1605	-.1543						
12	-.72	-1.30	1.1246	1.0611	-.2156	-.1803	-1.35	-2.41	1.1464	1.0244	-.257	-.2162	-1.81	-3.28	1.0606	1.0087	-.2121	-.2043						
M = 1.125																								
-4	0.37	0.69	-0.5114	-0.4862	0.0700	0.0635	0.68	1.25	-0.7003	-0.6699	0.1165	0.0990	0.87	1.59	-0.5580	-0.5149	0.0671	0.0593						
-2	.26	.45	-.5297	-.5272	.0141	.0066	.49	.85	-.5514	-.4275	.0653	.0294	.62	1.12	-.5726	-.6459	.0425	.0566						
0	.07	.13	-.0584	-.0504	-.0350	-.0345	.09	.12	-.2663	-.2379	-.0235	-.0562	.01	-.09	-.3021	-.3547	-.0715	-.0718						
2	-.06	-.21	.0880	.1214	-.0694	-.0684	-.21	-.51	.0008	.0424	-.0812	-.0863	-.41	-.96	-.0692	-.0182	-.1102	-.1334						
4	-.23	-.48	.2767	.2983	-.0956	-.0962	-.49	-.98	.2544	.2635	-.110	-.1140	-.75	-1.49	.2247	.2329	-.1563	-.1323						
8	-.50	-.94	.6486	.6397	-.1356	-.1316	-.94	-1.77	.7431	.7023	-.1605	-.1582	-1.28	-2.41	.6763	.6338	-.1490	-.1410						
12	-.71	-1.37	1.0129	.9929	-.2100	-.1913	-1.33	-2.57	1.0489	1.0327	-.235	-.2359	-1.79	-3.45	.9415	.9050	-.1932	-.1849						
M = 1.200																								
-4	0.31	0.73	-0.4012	-0.4261	0.0400	0.0465	0.55	1.34	-0.5793	-0.5650	0.0578	0.0676	0.68	1.81	-0.5926	-0.7350	0.0430	0.1050						
-2	.25	.48	-.2791	-.2693	.0077	.0024	.46	.86	-.4705	-.4845	.092	.0078	.63	1.16	-.6343	-.6411	.0738	.0763						
0	.08	.15	-.0916	-.0863	-.0378	-.0395	.09	.19	-.2475	-.2531	-.0597	-.0394	.04	-.06	-.3350	-.3546	-.0398	-.0461						
2	-.06	-.13	.0847	.0935	-.0673	-.0674	-.17	-.34	-.0378	-.0392	-.070	-.0679	-.34	-.69	-.1031	-.0950	-.0978	-.0461						
4	-.21	-.41	.2509	.2564	-.0926	-.0938	-.44	-.85	.1677	.1844	-.105	-.0981	-.70	-1.34	.1809	.1668	-.1400	-.1290						
8	-.46	-.89	.5990	.5913	-.1373	-.1348	-.89	-1.70	.6374	.6066	-.165	-.1566	-1.22	-2.35	.5809	.5411	-.1388	-.1340						
12	-.69	-1.37	.9487	.9582	-.2108	-.2068	-1.28	-2.55	.9558	.9467	-.217	-.2209	-1.72	-3.43	.8668	.8463	-.1803	-.1775						

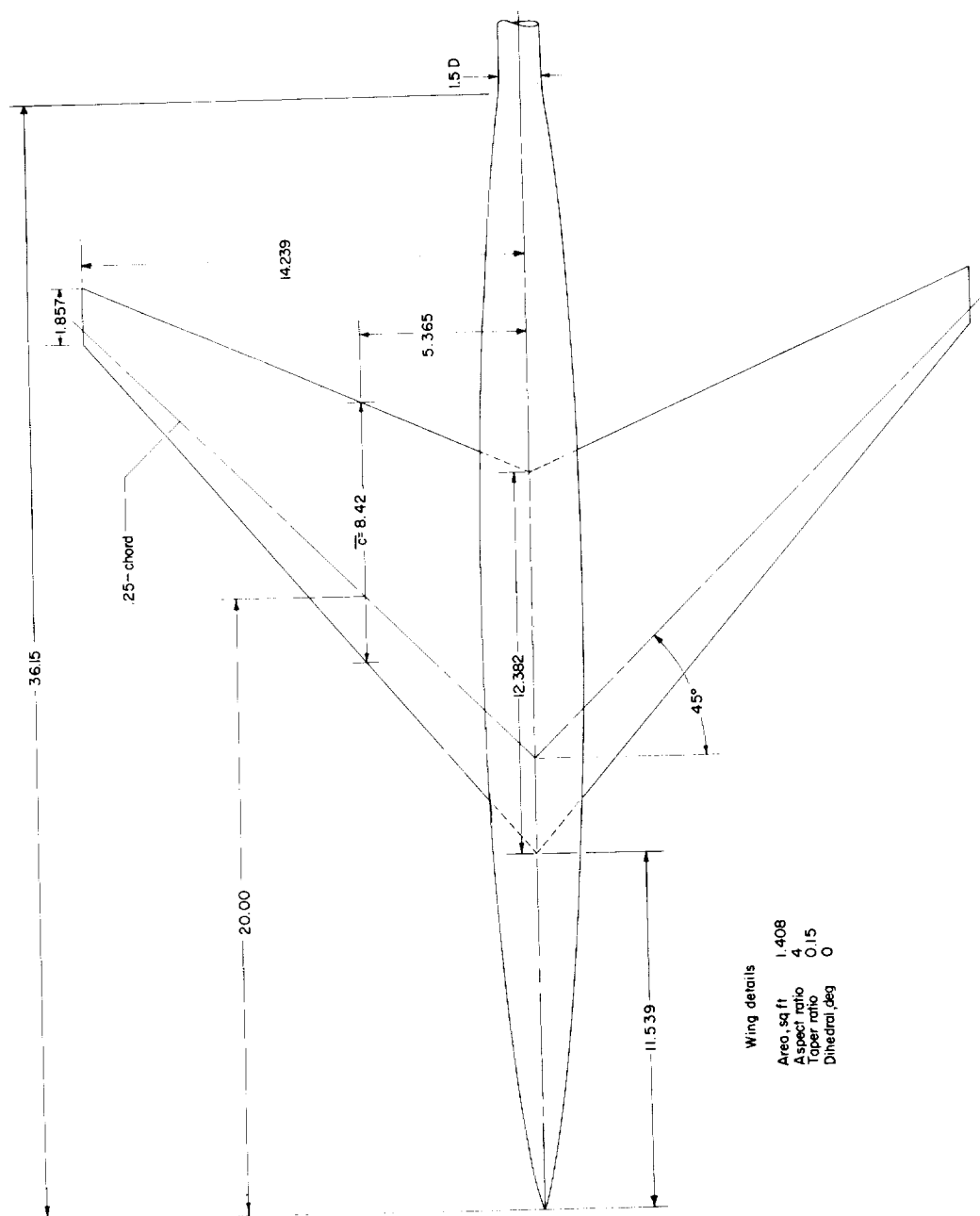


Figure 1.- Details of wing-body combination. All dimensions are in inches unless otherwise noted.

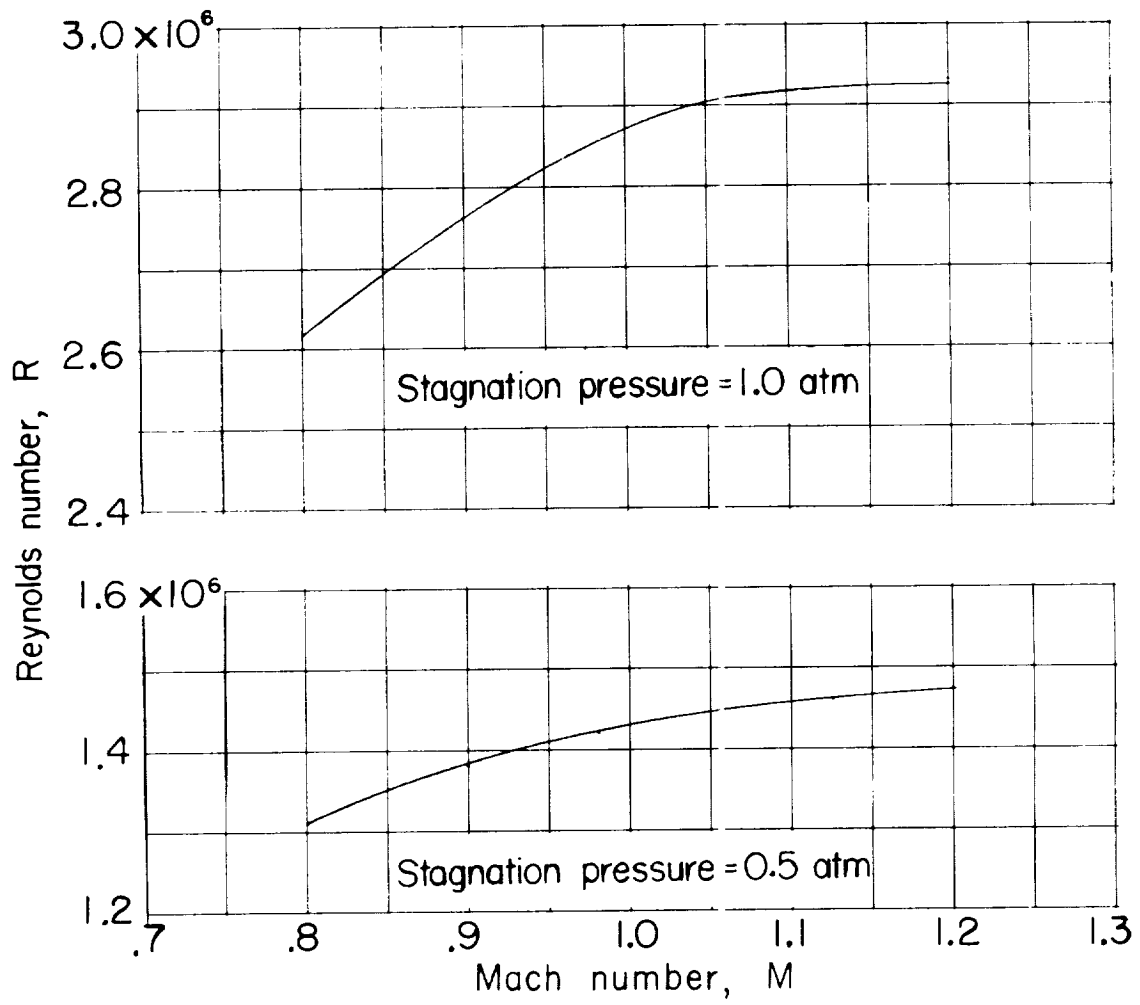


Figure 2.- Variation with Mach number of average Reynolds number based on wing mean aerodynamic chord.

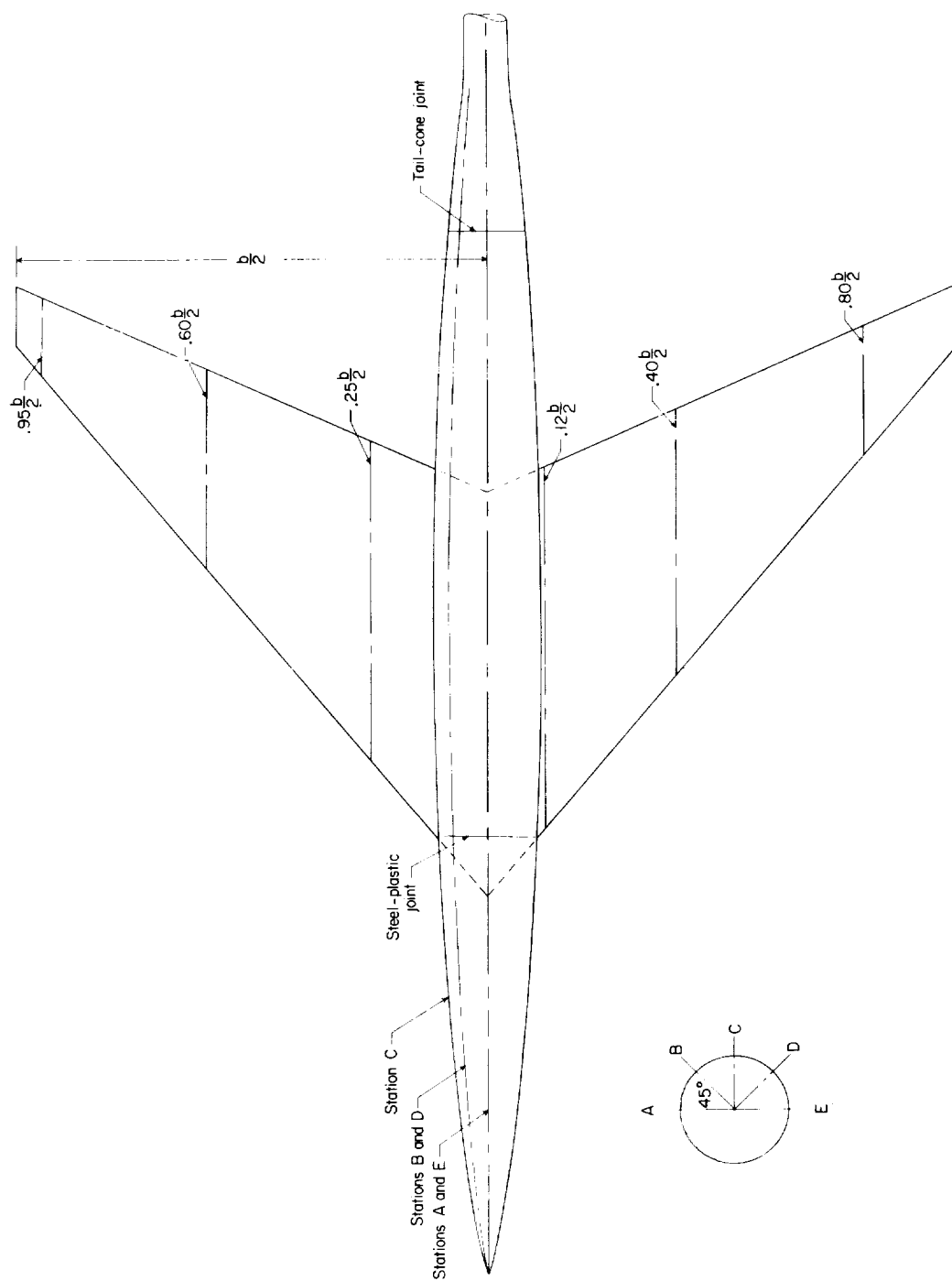
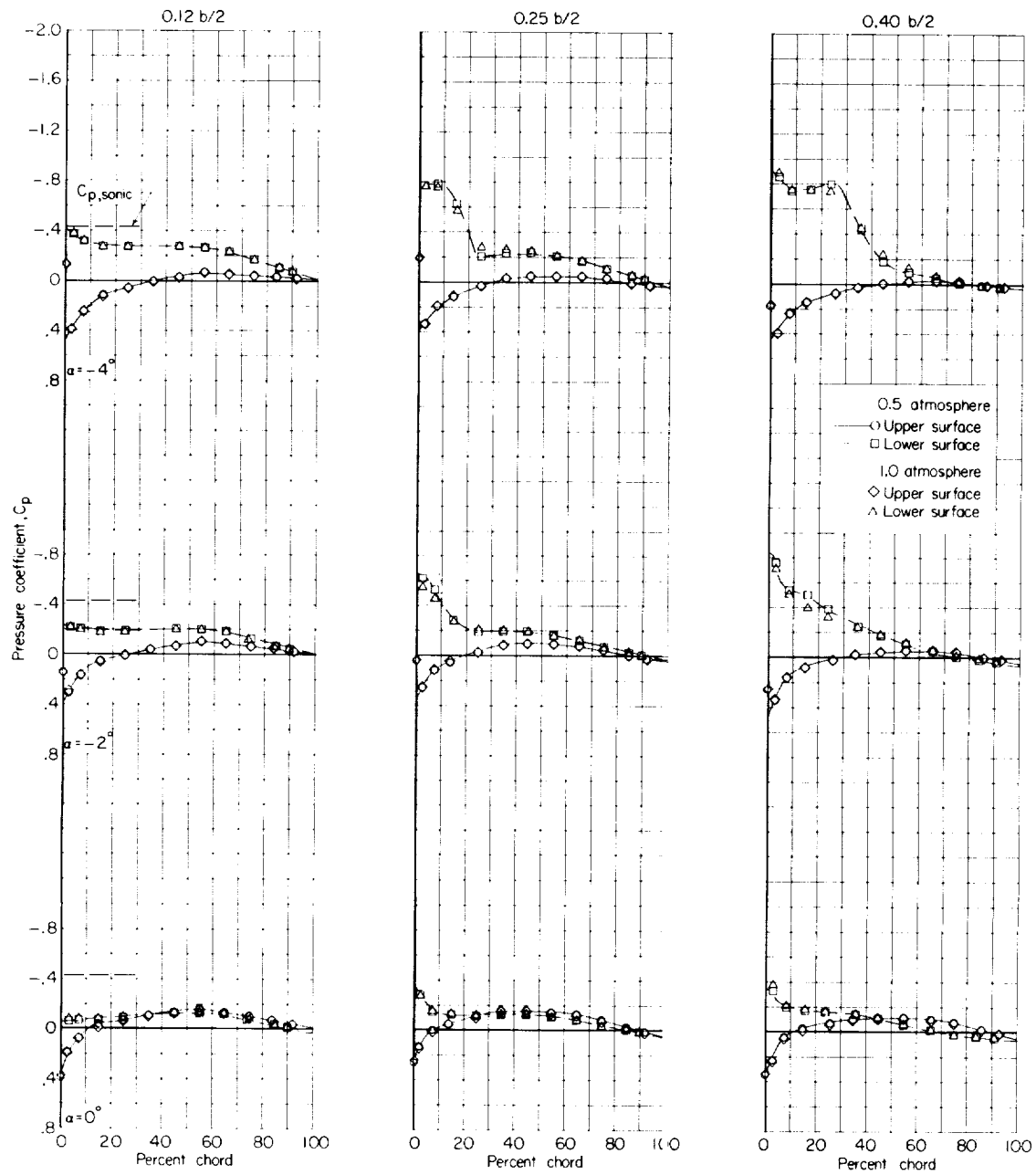
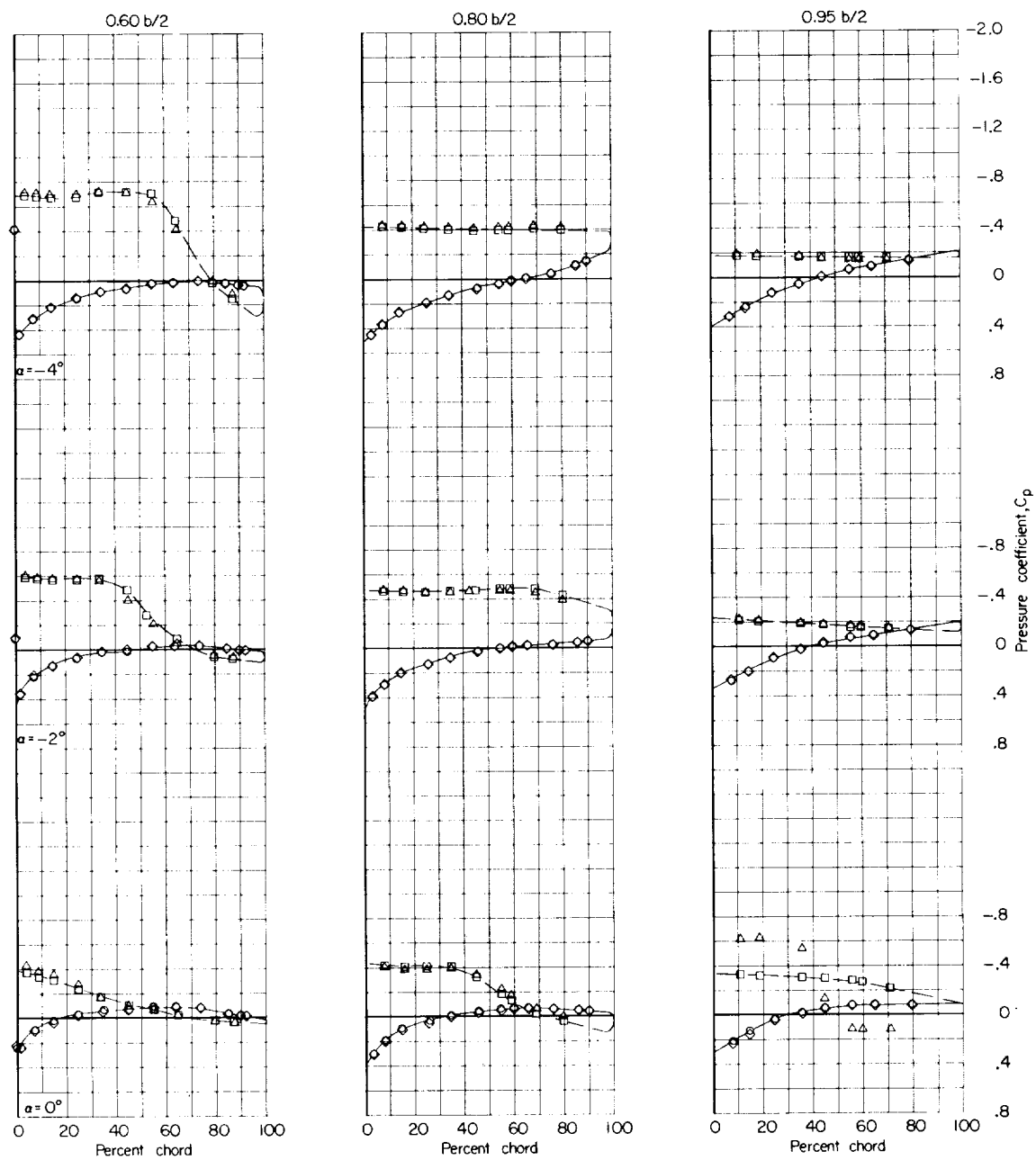


Figure 3.- A sketch of the location of pressure orifices on the wing and body.



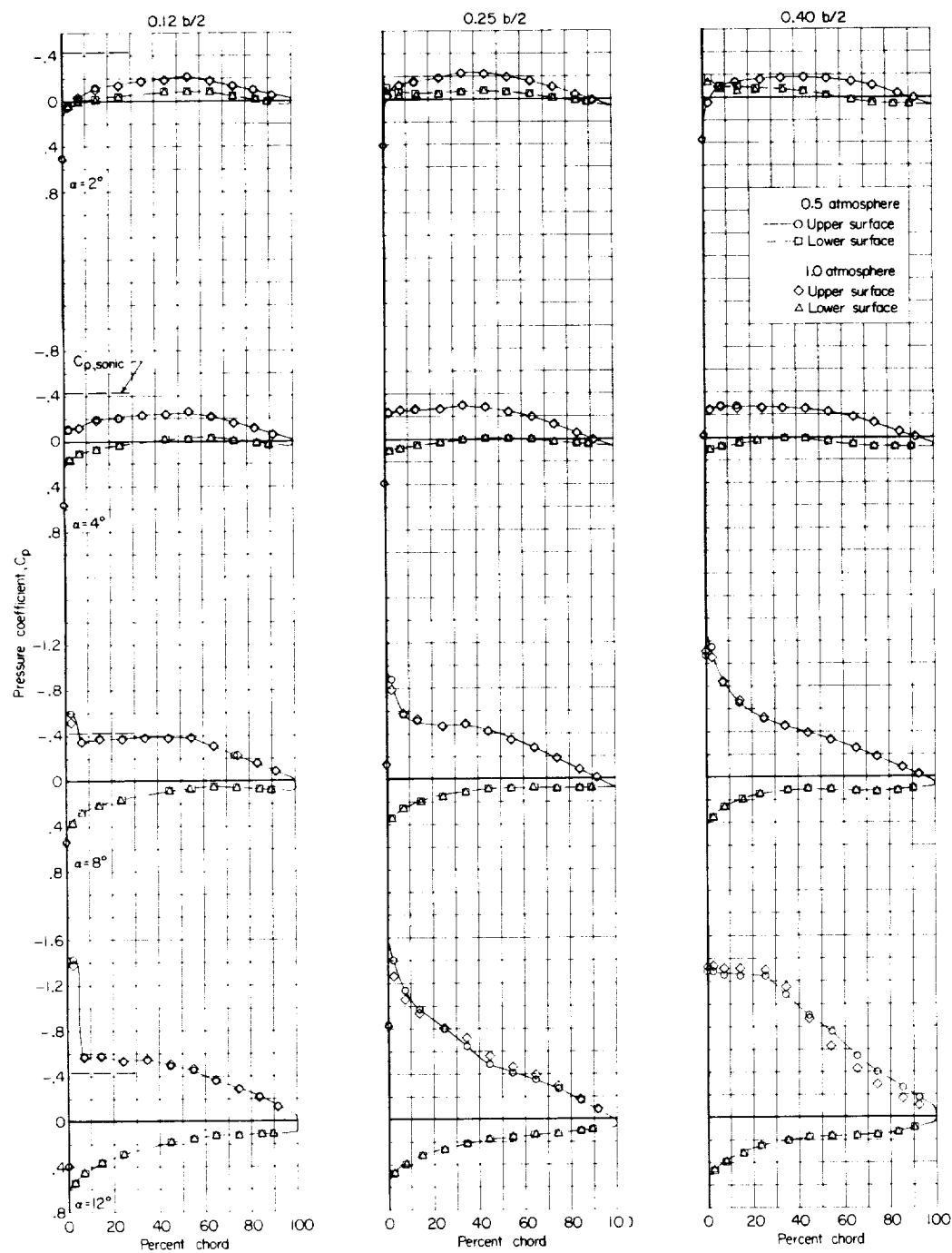
(a) $M = 0.800$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Pressure measurements on the wing in the presence of the body.



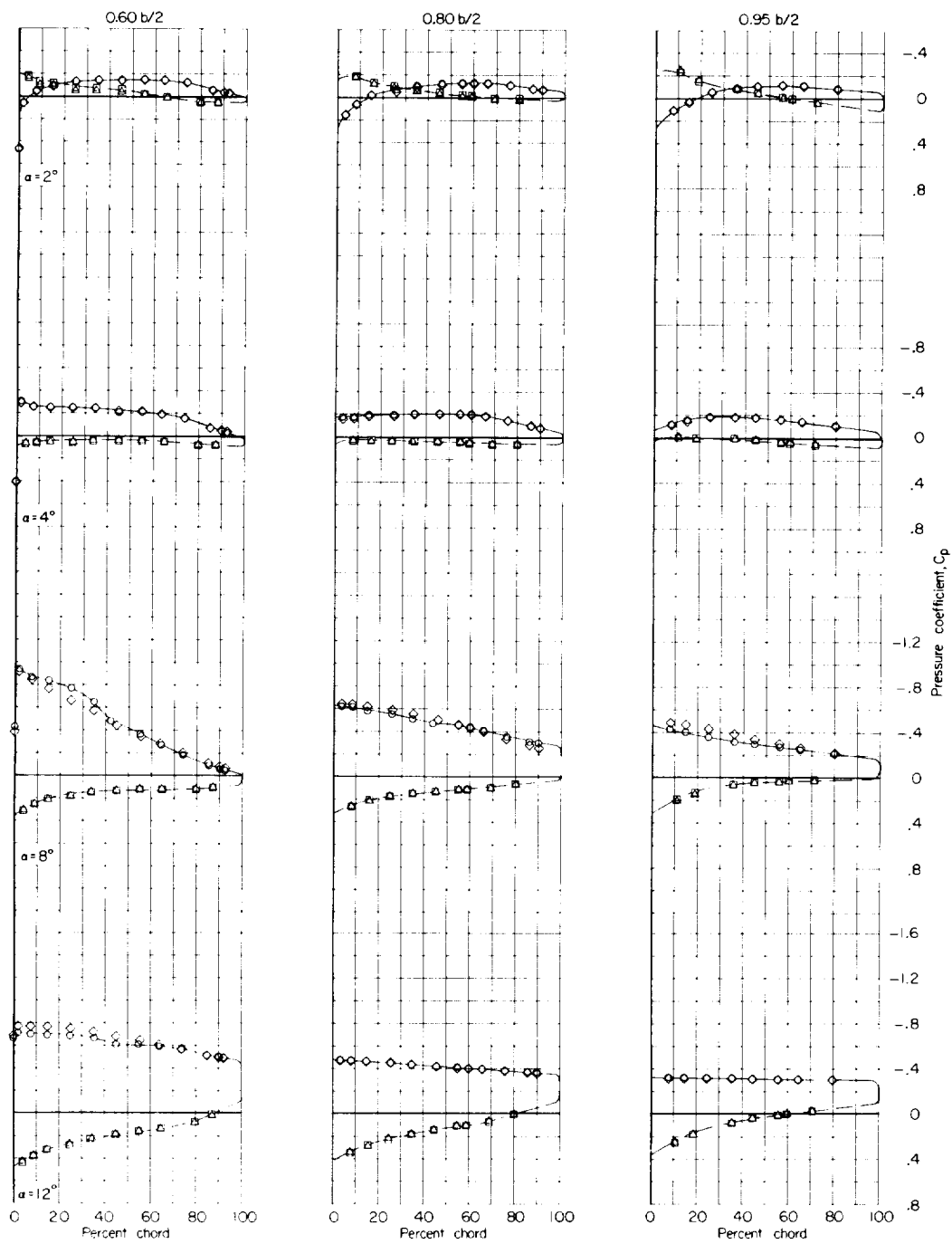
(a) Concluded.

Figure 4.- Continued.



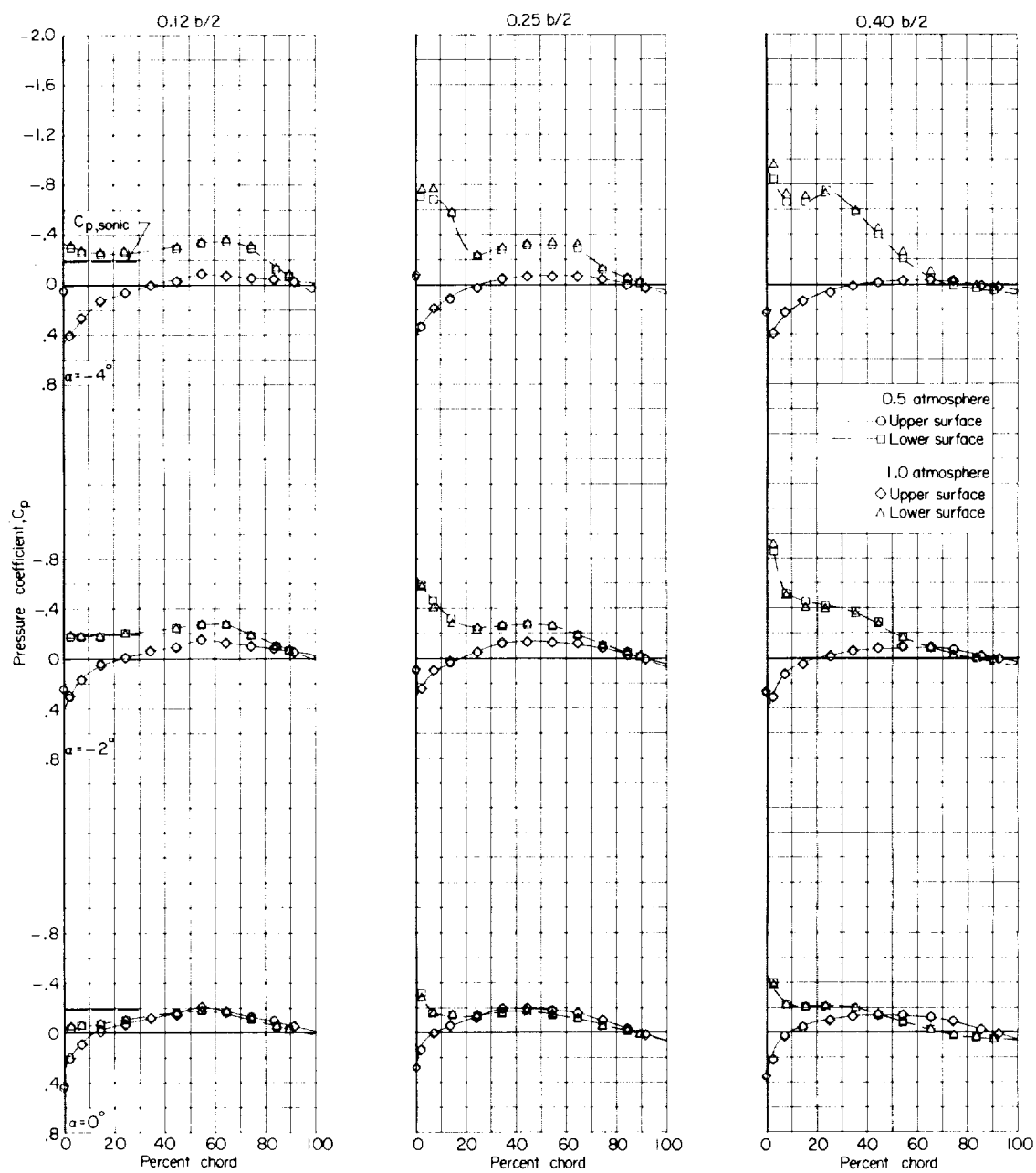
(b) $M = 0.800$; $\alpha = 2^\circ, 4^\circ, 8^\circ$, and 12° .

Figure 4.- Continued.



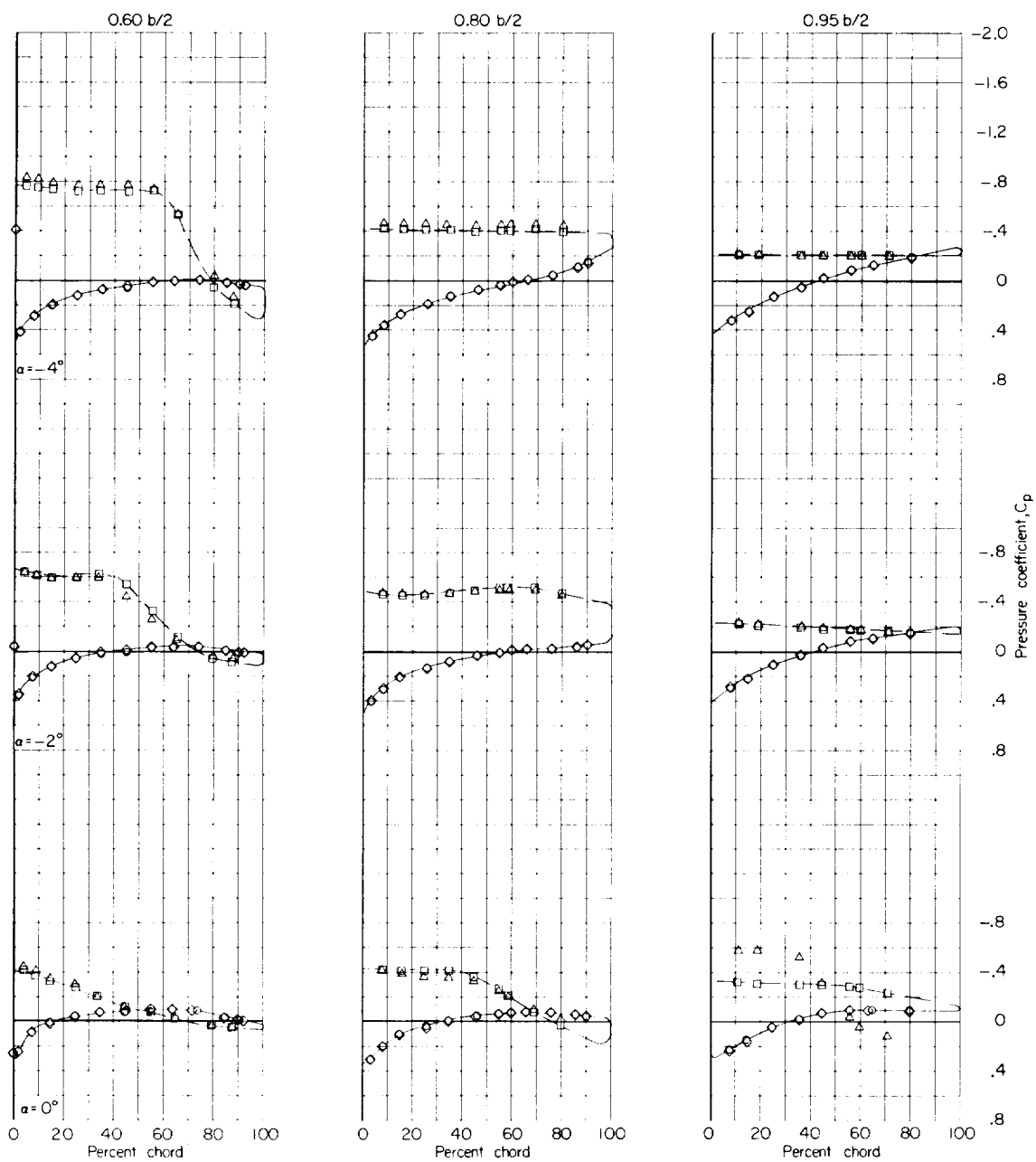
(b) Concluded.

Figure 4.- Continued.



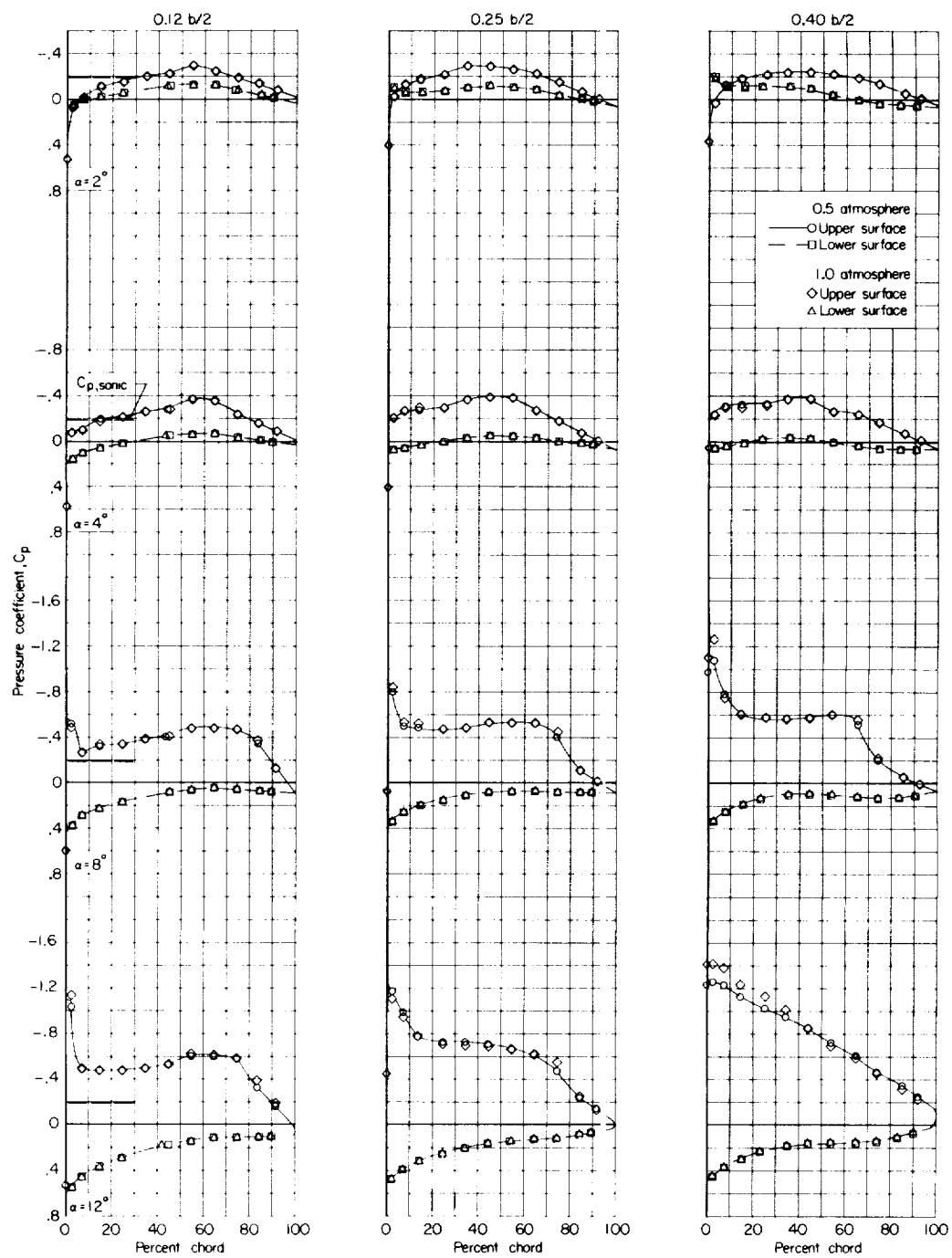
(c) $M = 0.900$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



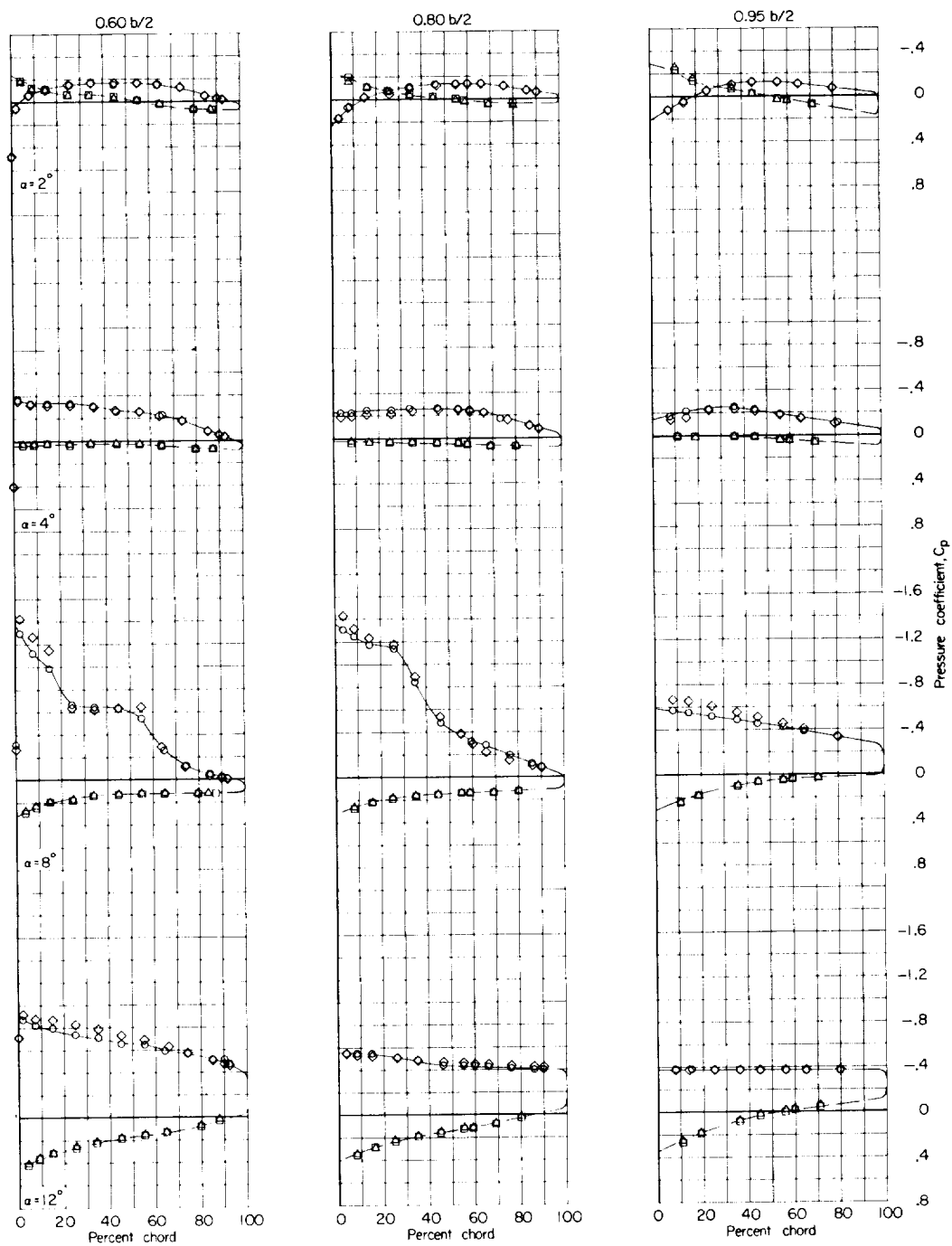
(c) Concluded.

Figure 4.- Continued.



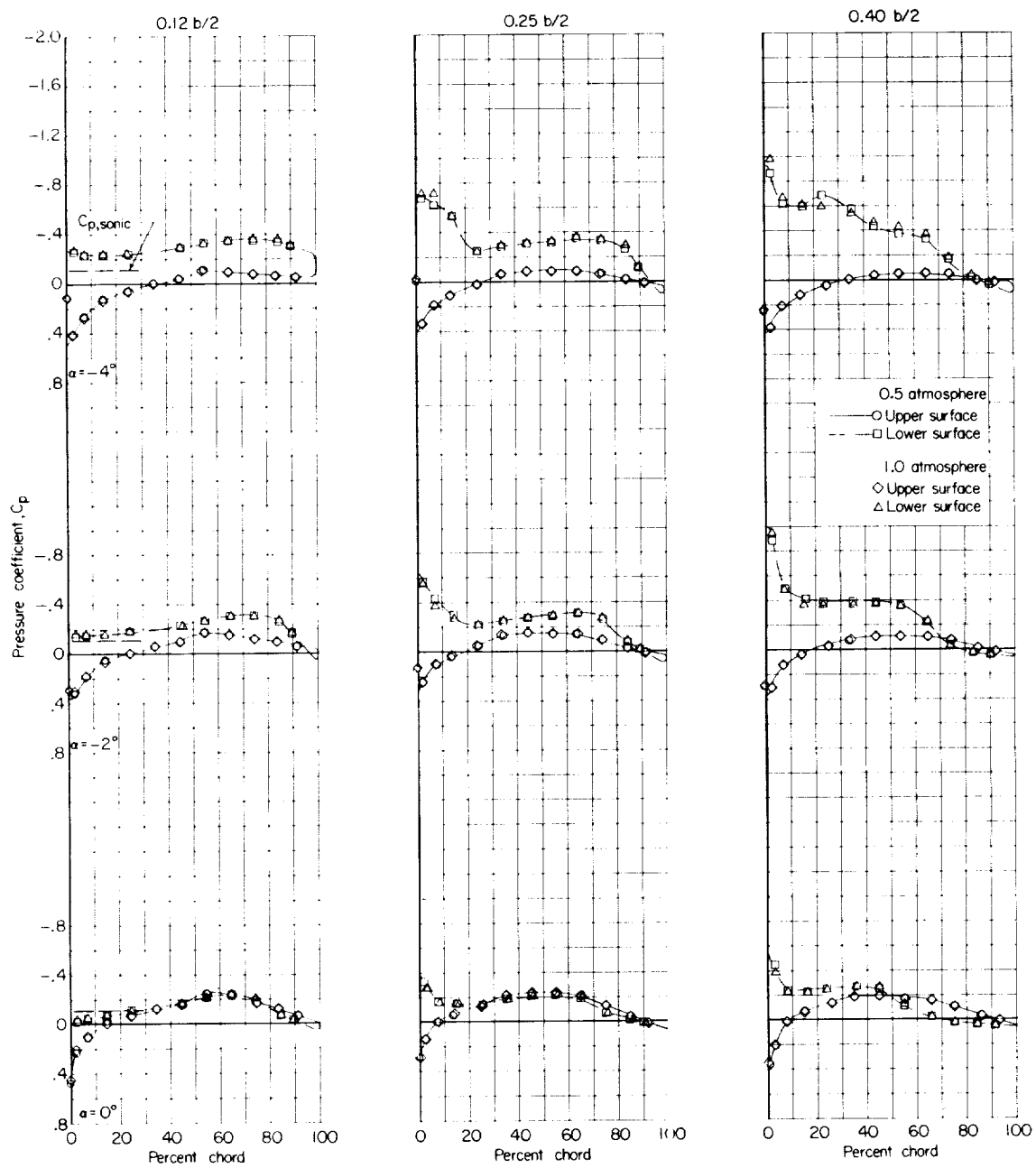
(d) $M = 0.900$; $\alpha = 2^\circ, 4^\circ, 8^\circ$, and 12° .

Figure 4.- Continued.



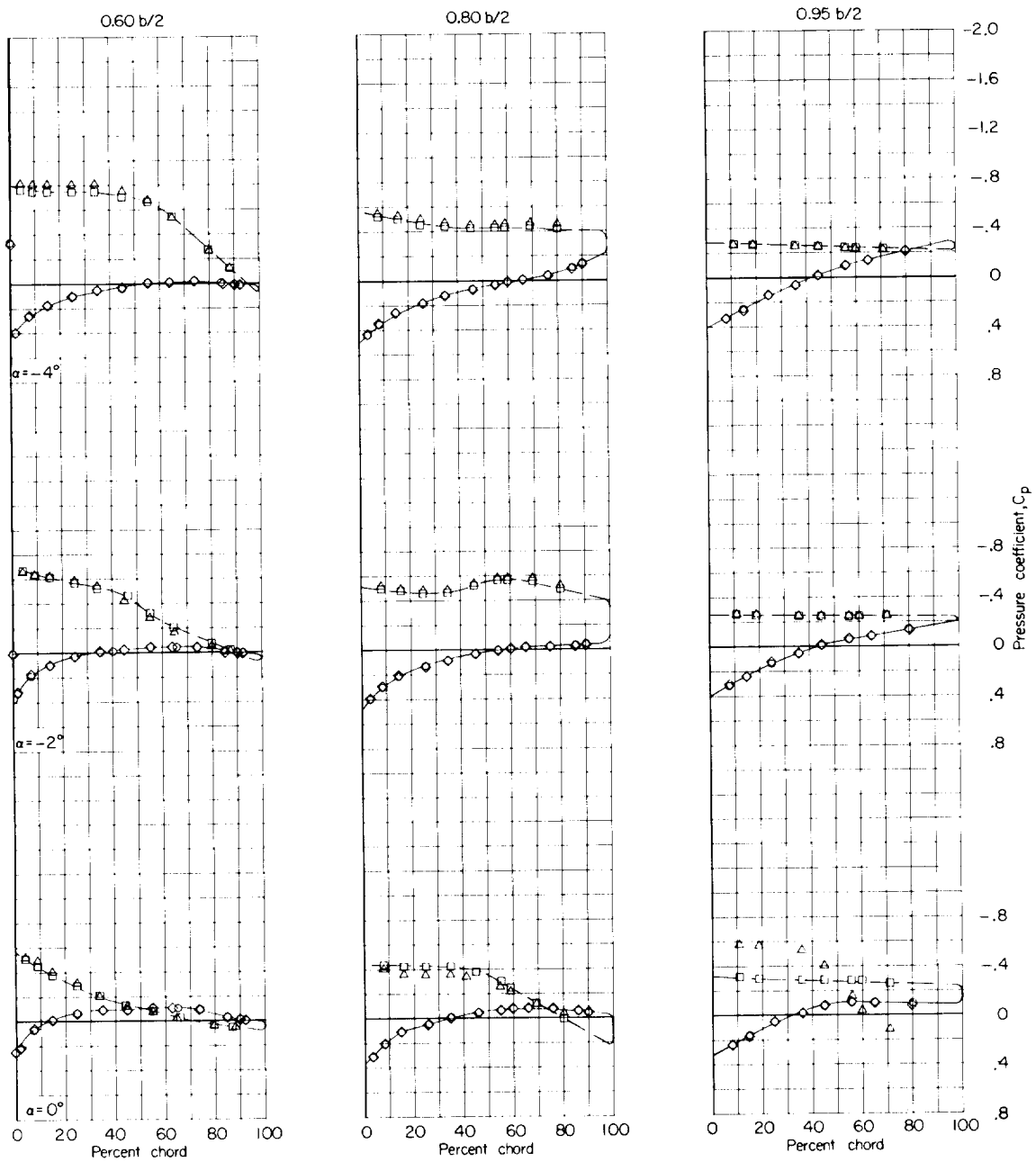
(d) Concluded.

Figure 4.- Continued.



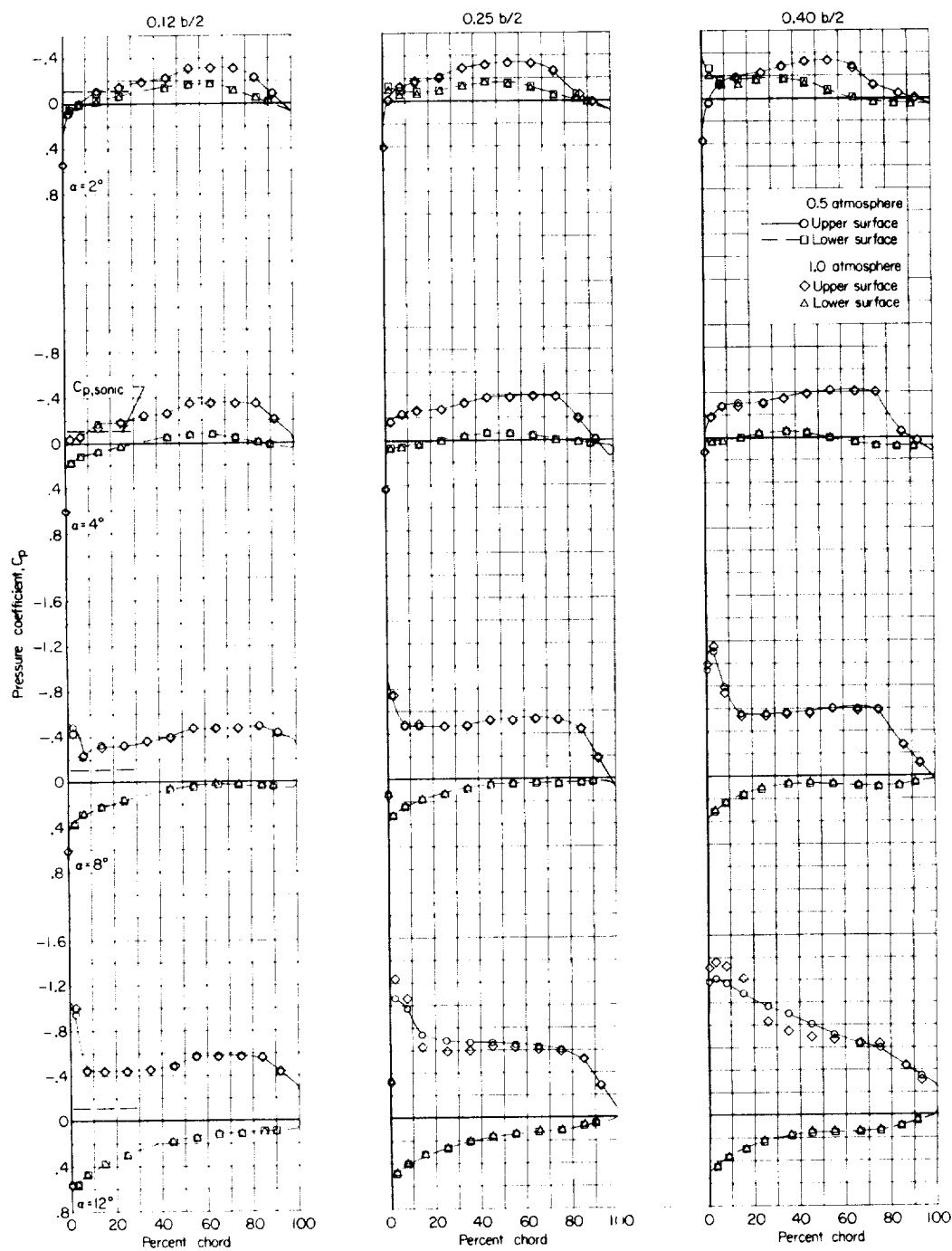
(e) $M = 0.940$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



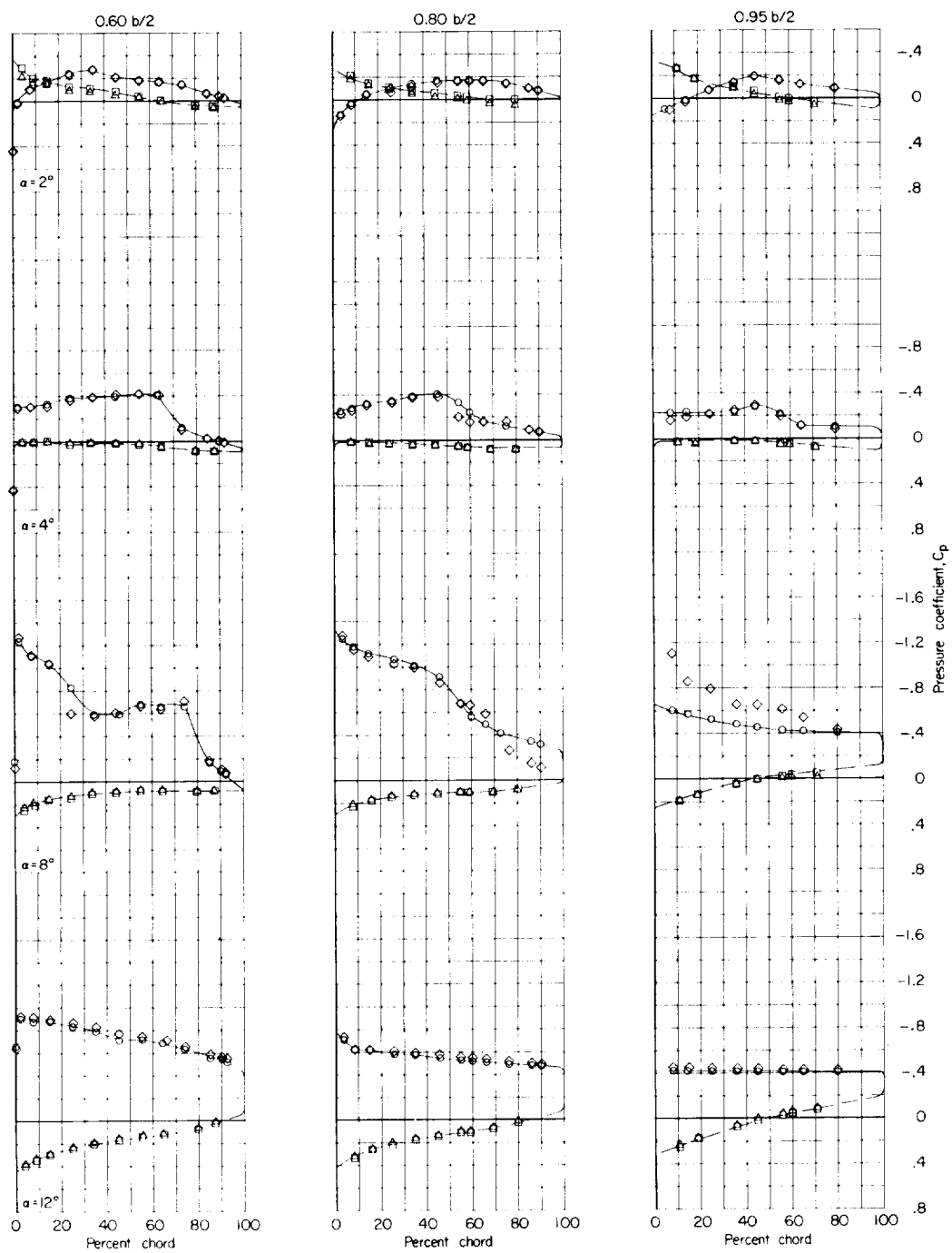
(e) Concluded.

Figure 4.- Continued.



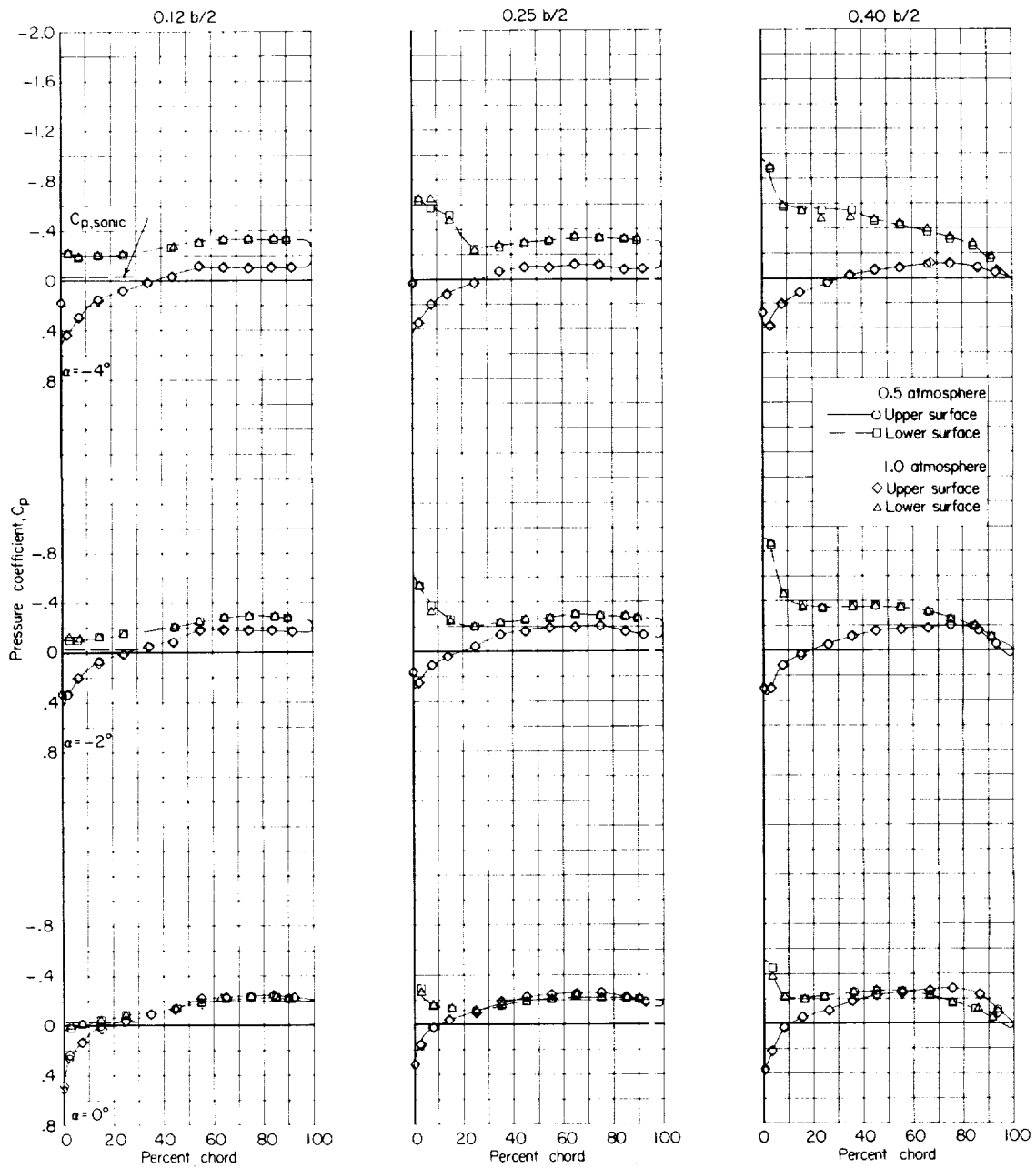
(f) $M = 0.940$; $\alpha = 2^\circ, 4^\circ, 8^\circ, \text{ and } 12^\circ$.

Figure 4.- Continued.



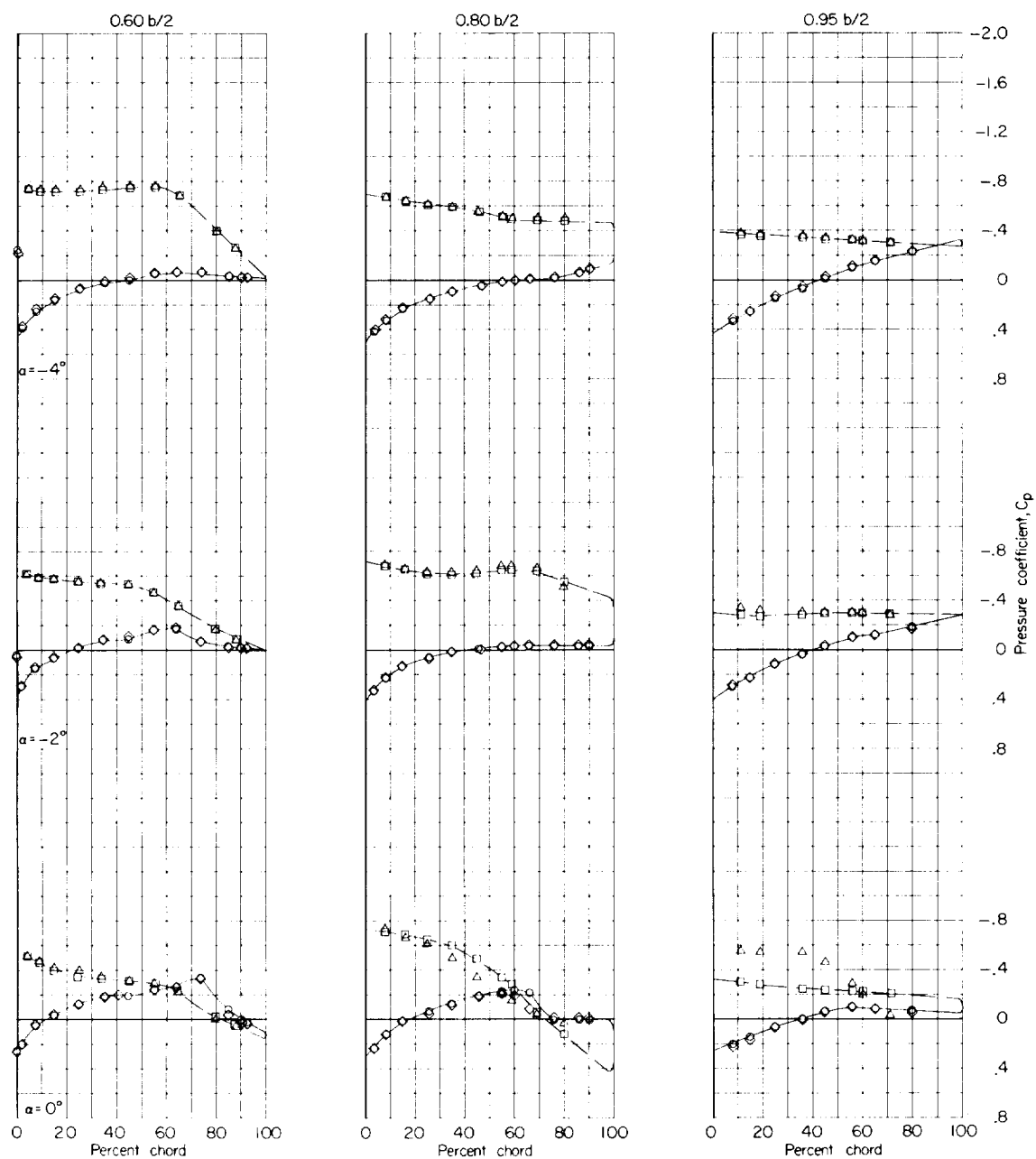
(f) Concluded.

Figure 4.- Continued.



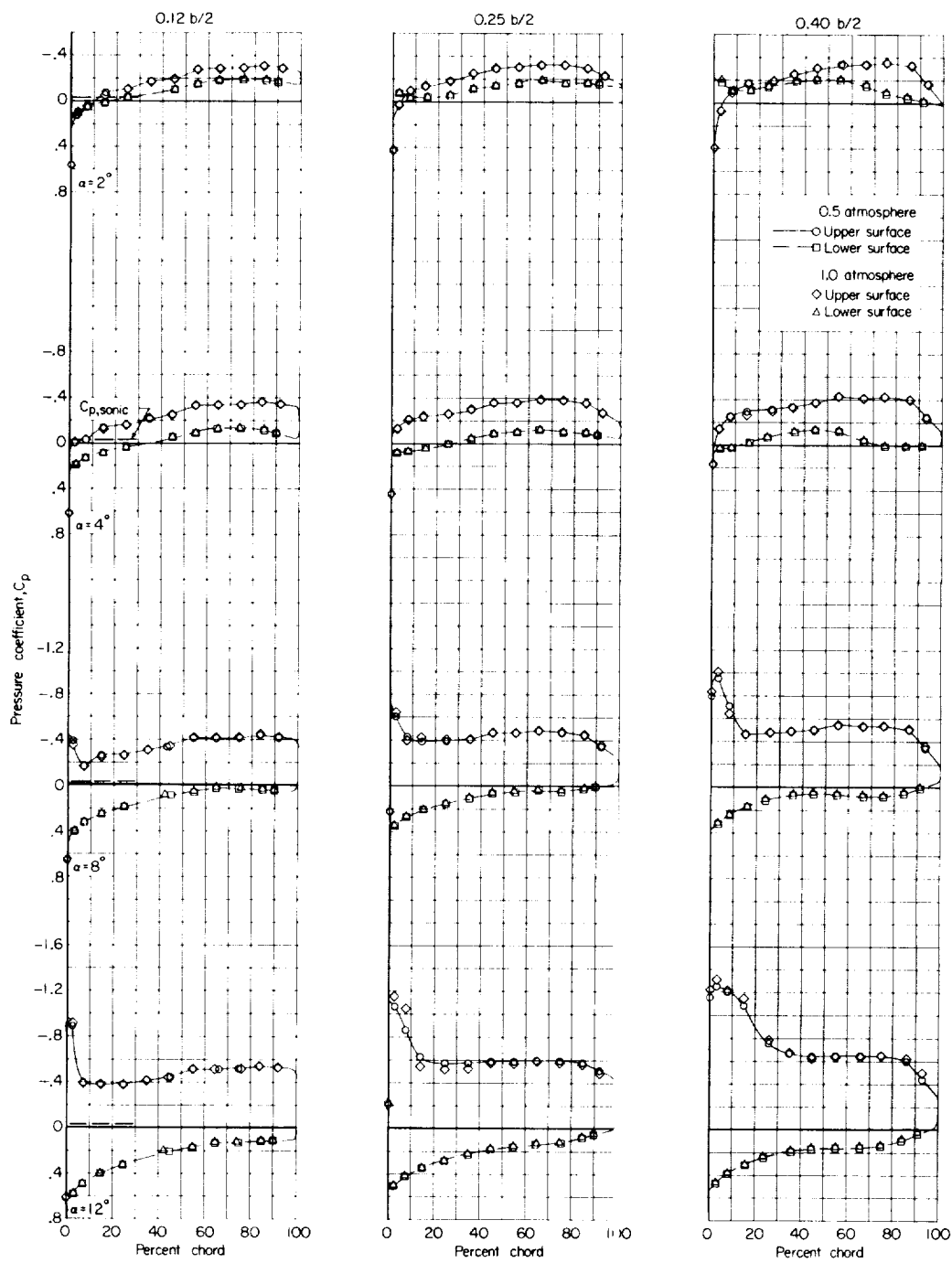
(g) $M = 0.980$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



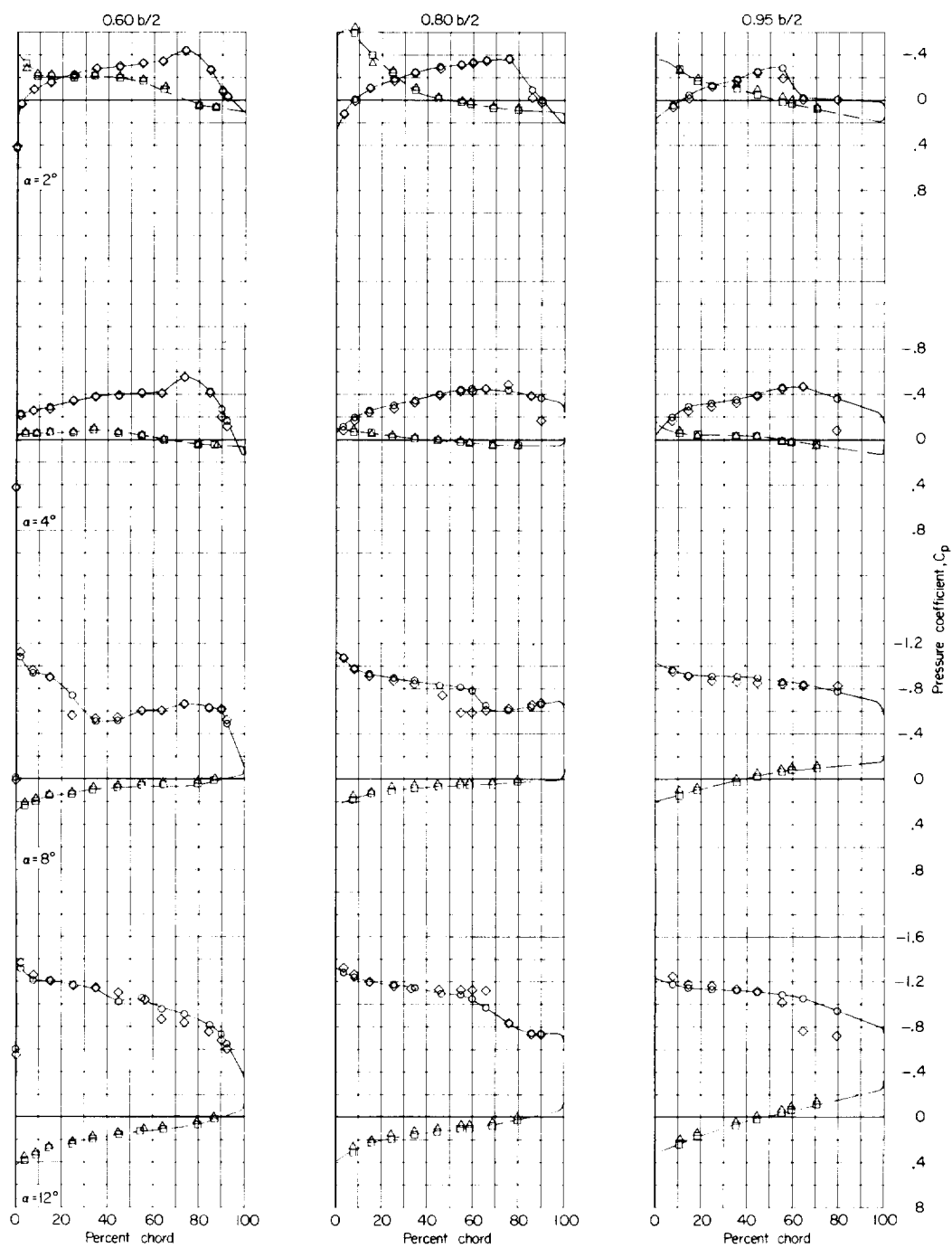
(g) Concluded.

Figure 4.- Continued.



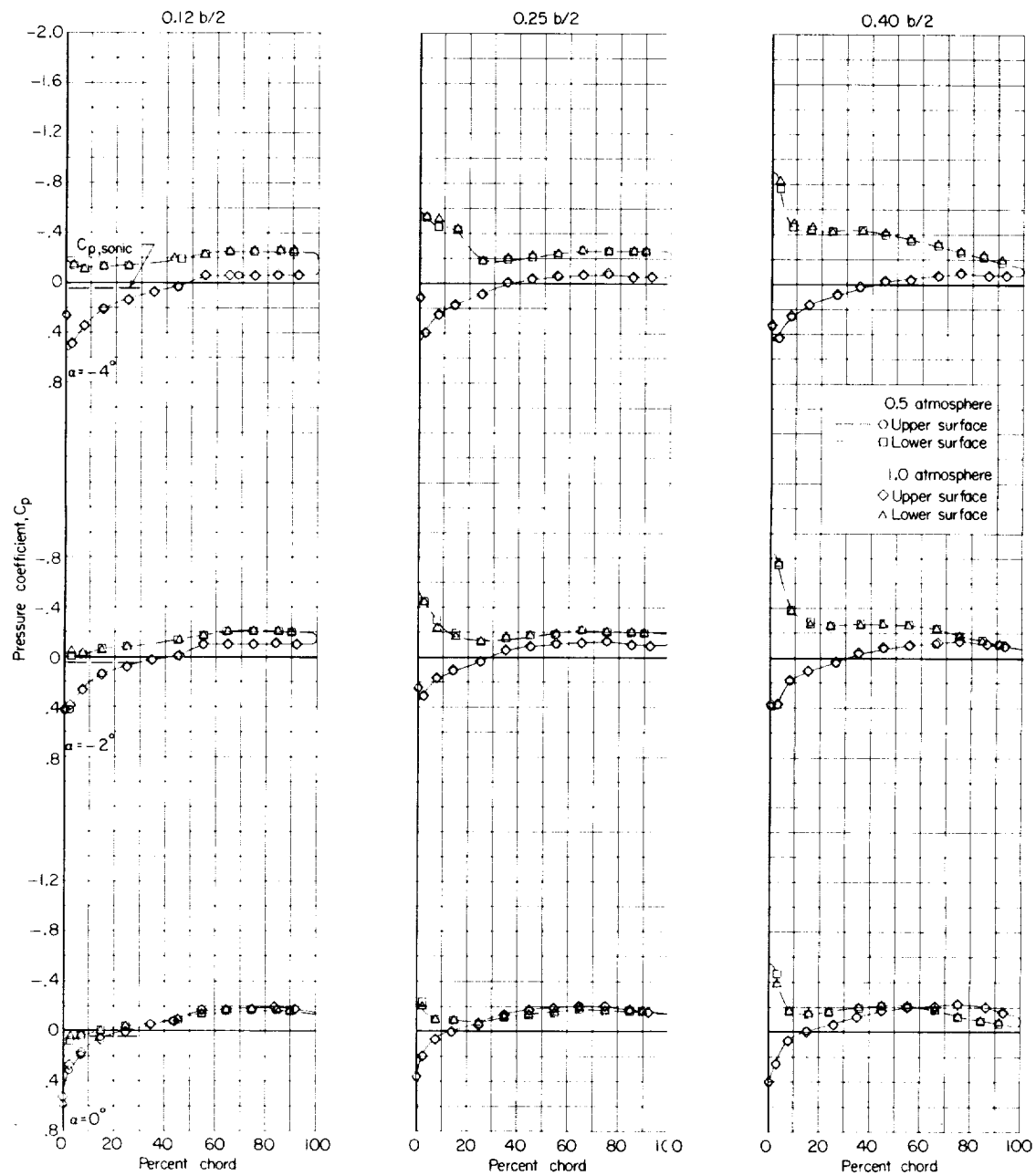
(h) $M = 0.980$; $\alpha = 2^\circ$, 4° , 8° , and 12° .

Figure 4.- Continued.



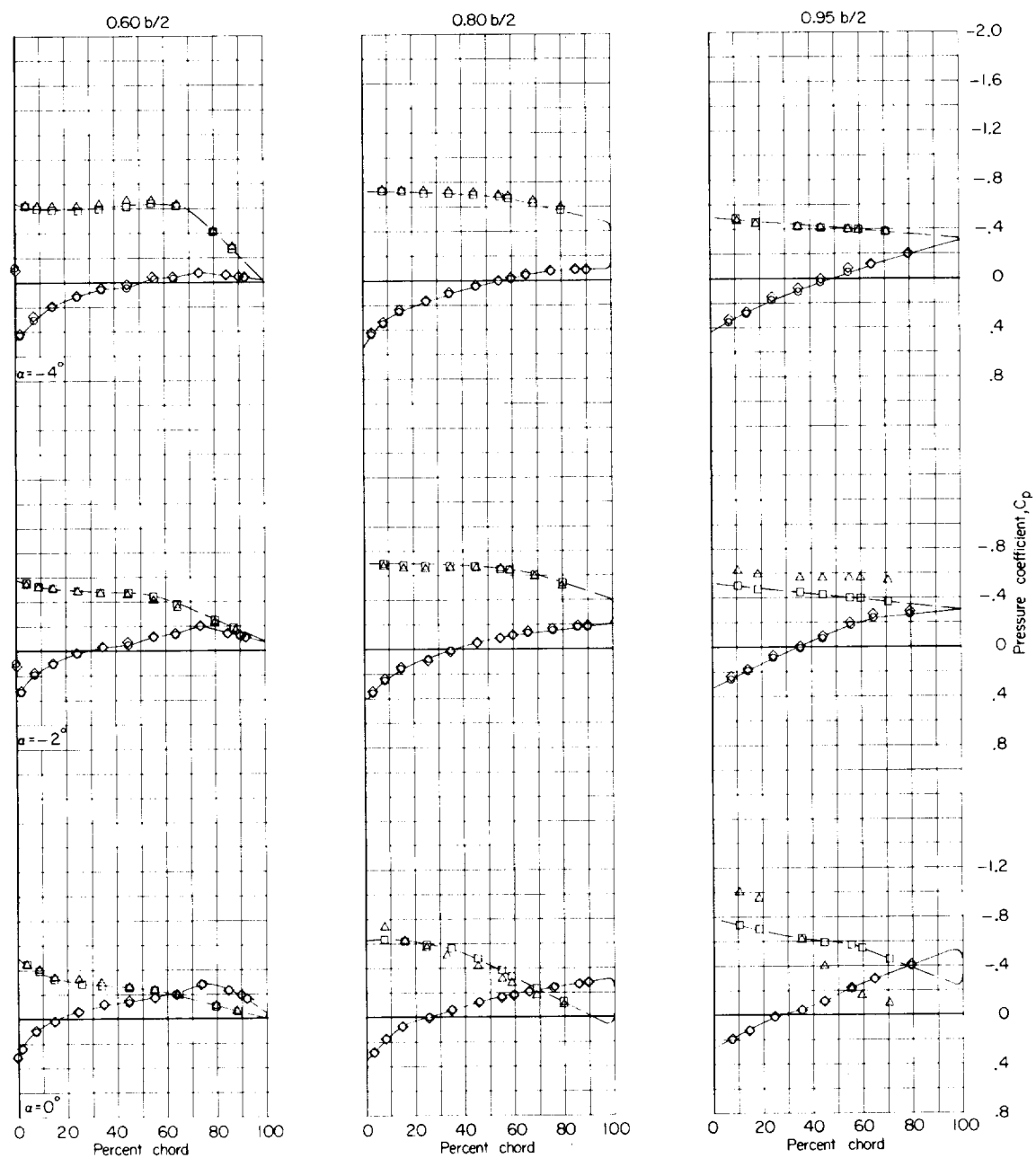
(h) Concluded.

Figure 4.- Continued.



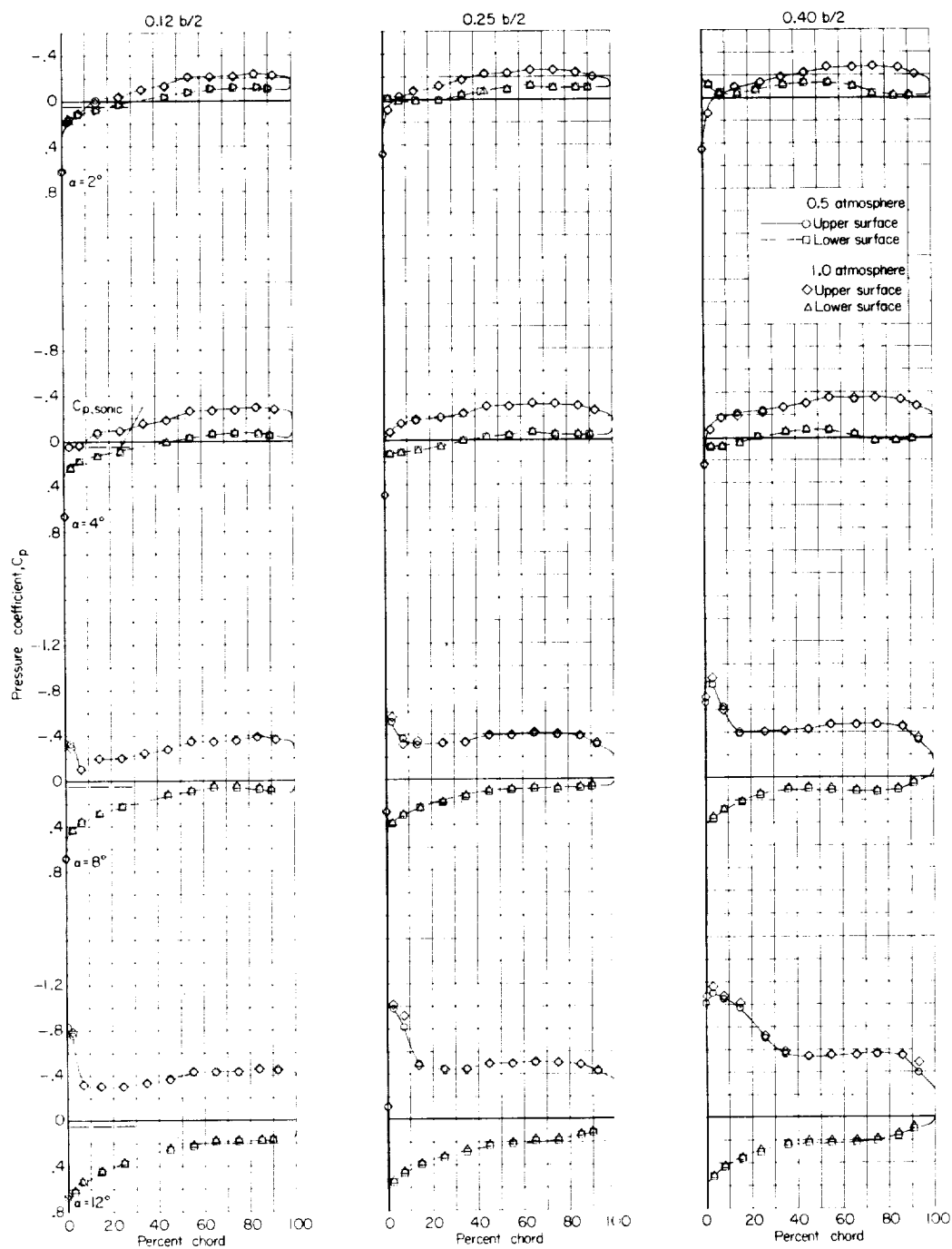
(i) $M = 1.030$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



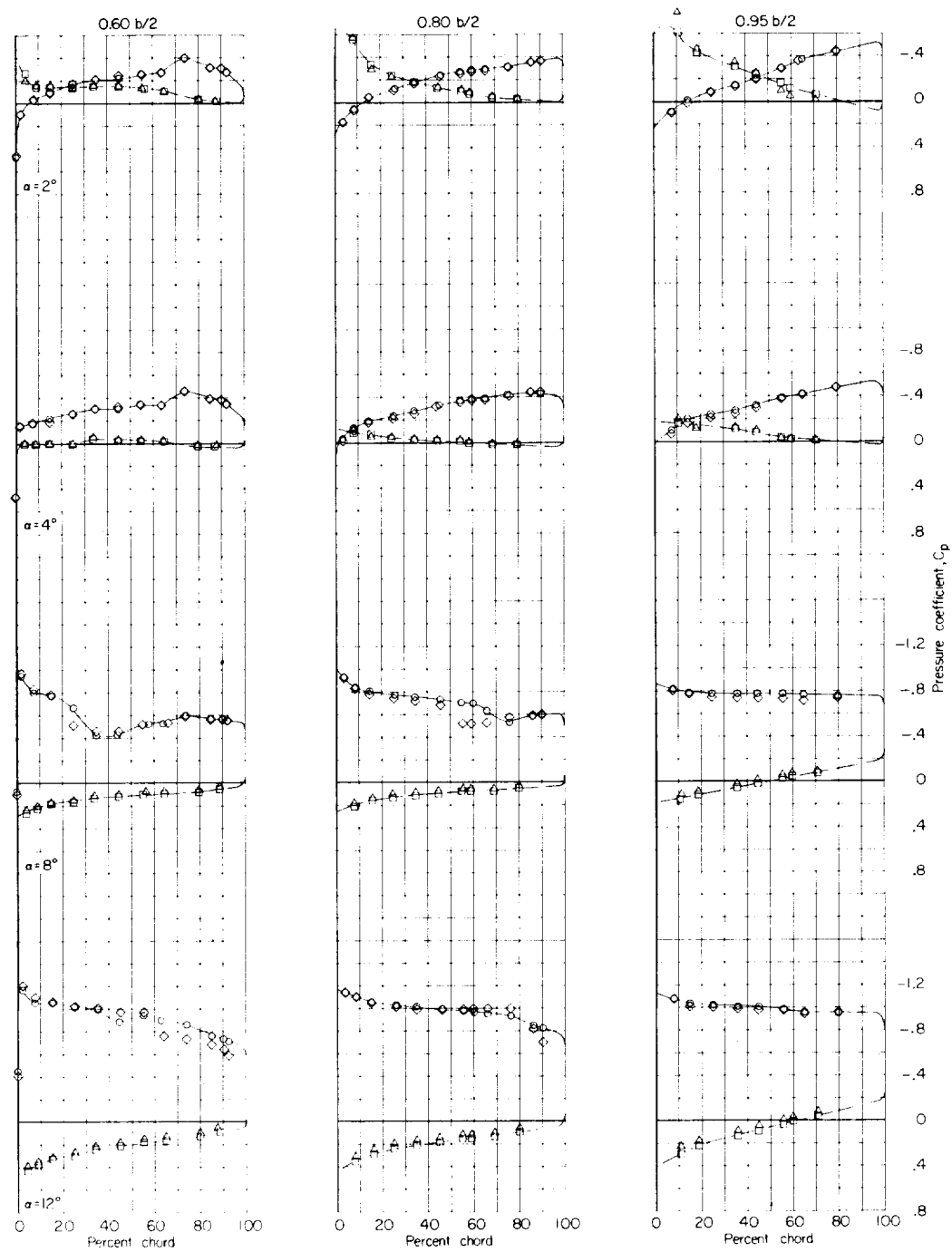
(i) Concluded.

Figure 4.- Continued.



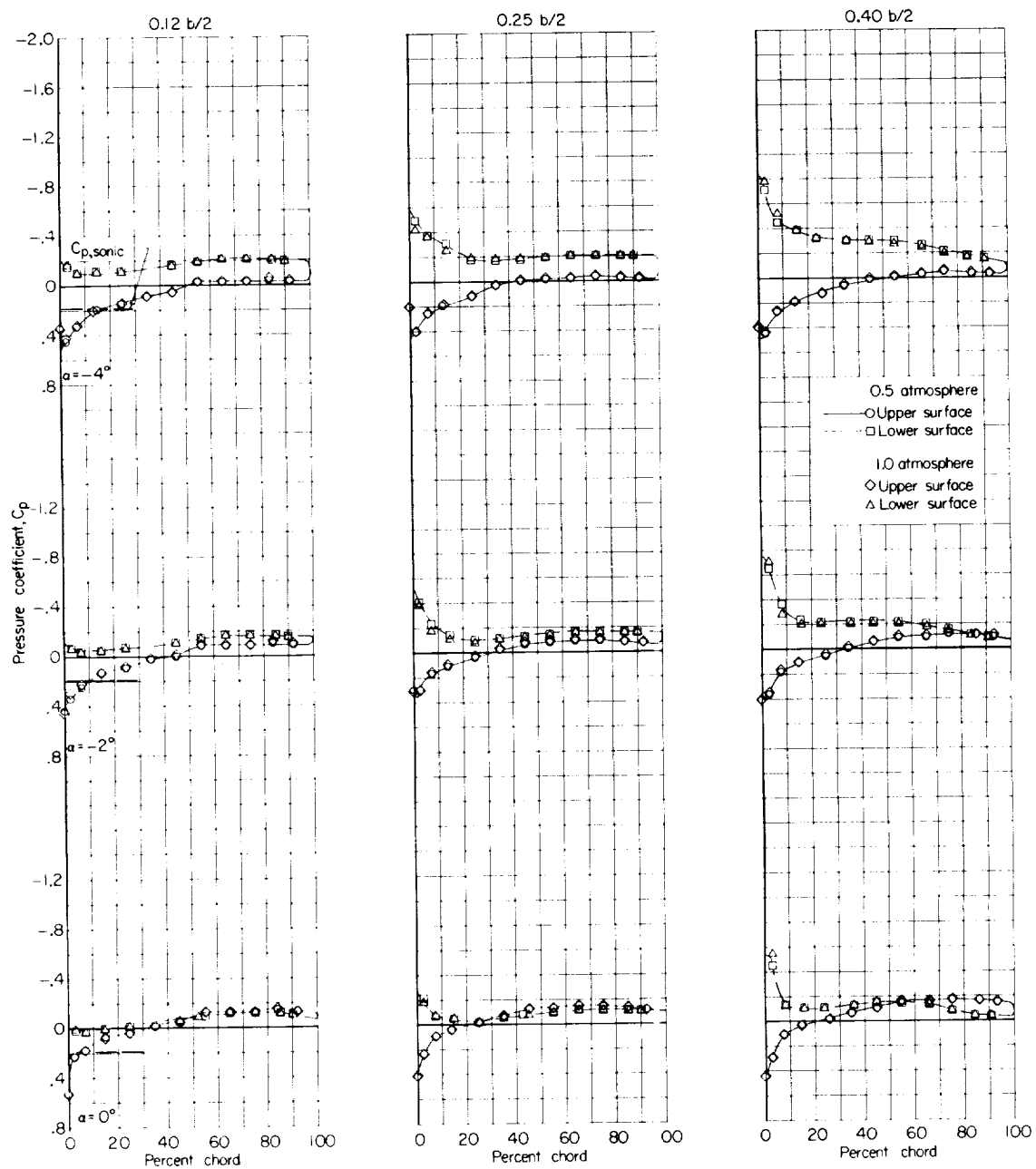
(j) $M = 1.030$; $\alpha = 2^\circ, 4^\circ, 8^\circ$, and 12° .

Figure 4.- Continued.



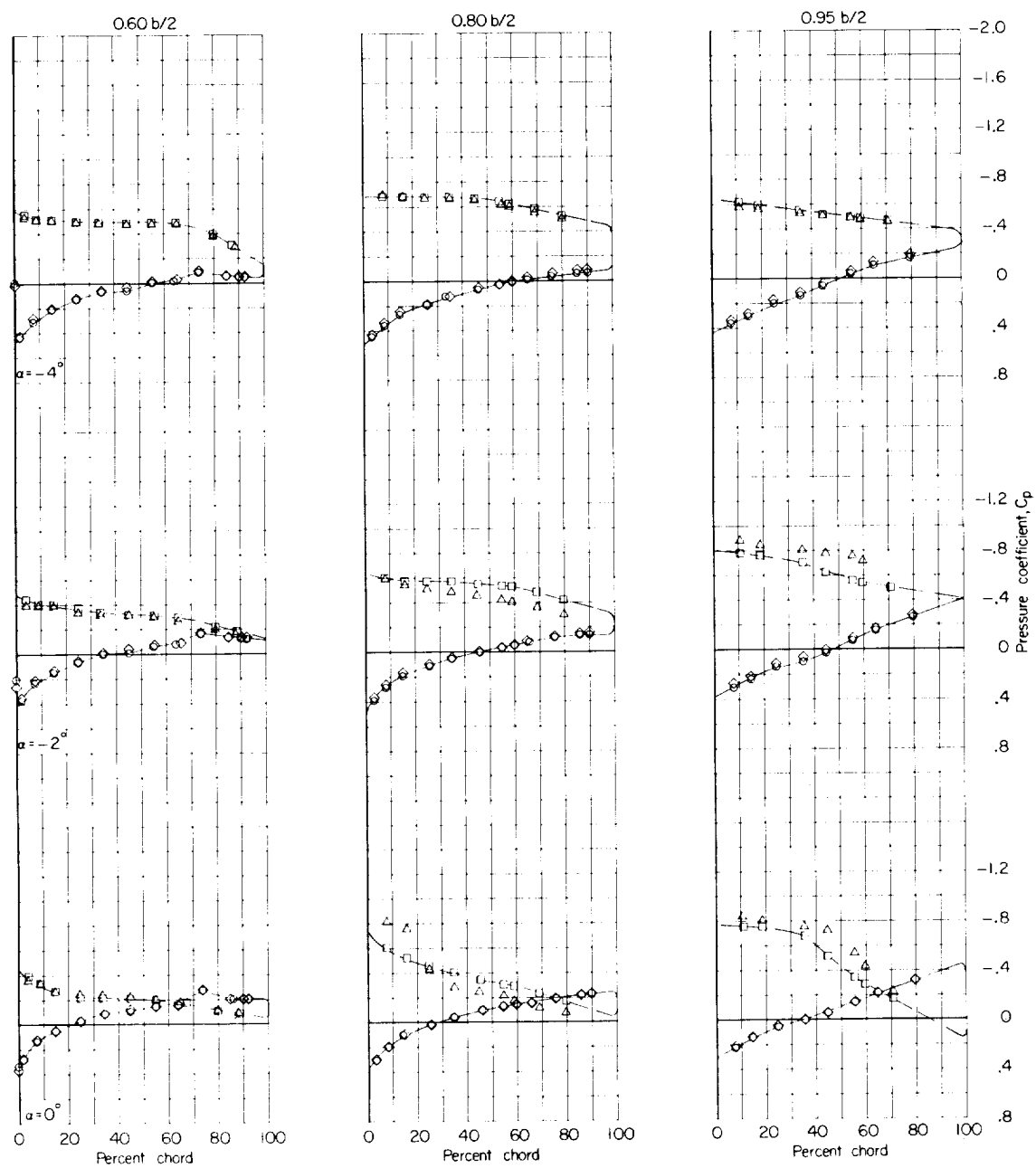
(j) Concluded.

Figure 4.- Continued.



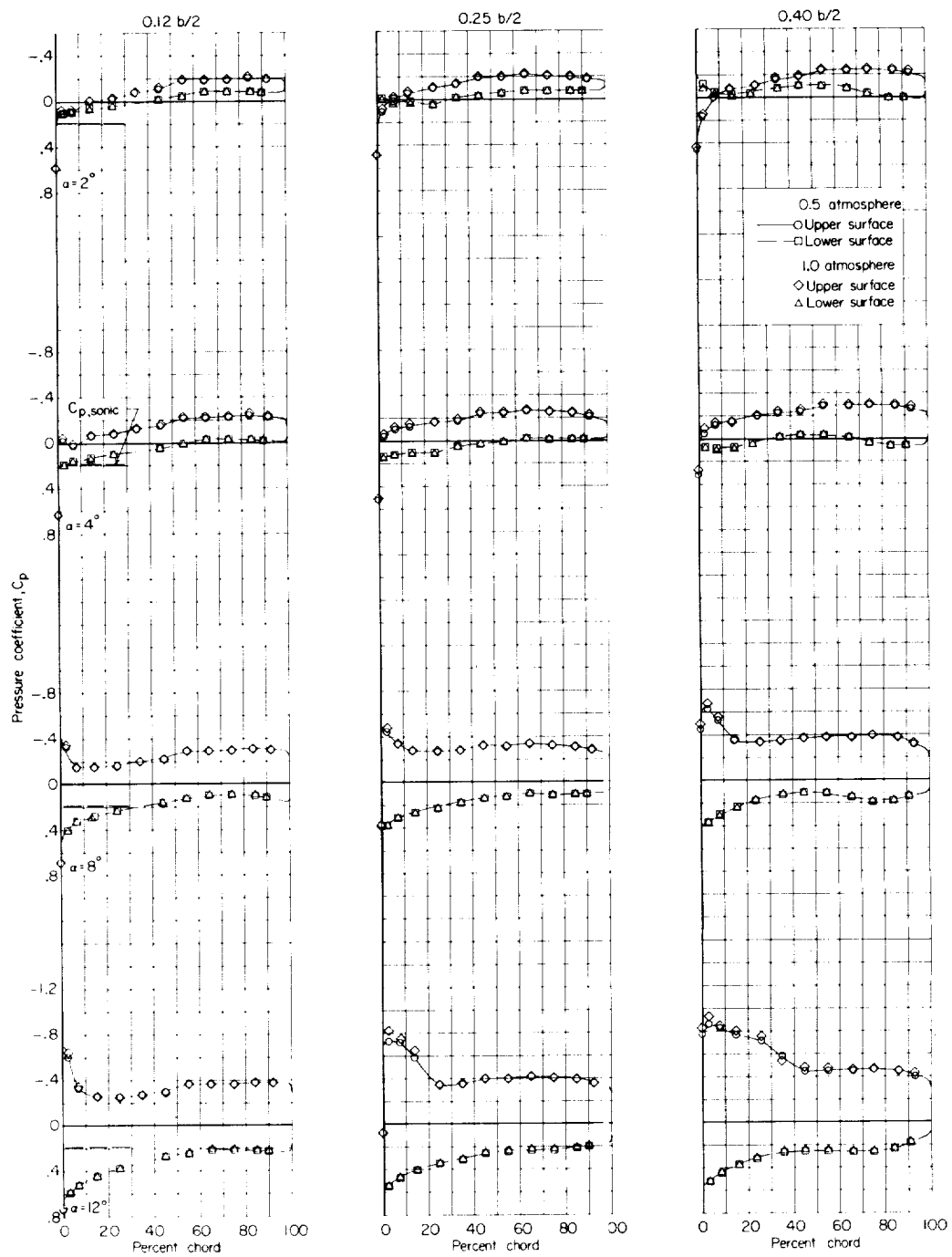
(k) $M = 1.125$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



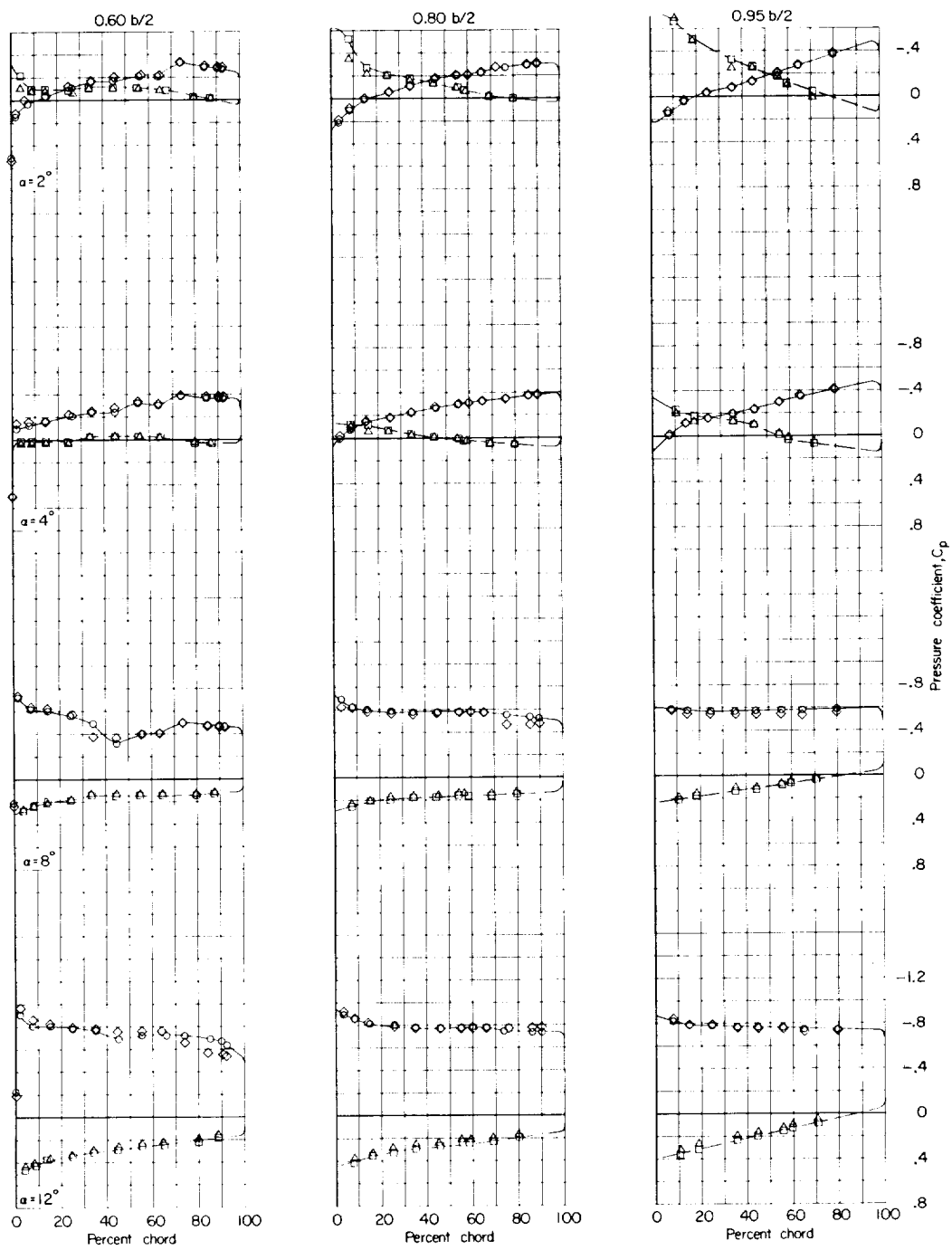
(k) Concluded.

Figure 4.- Continued.



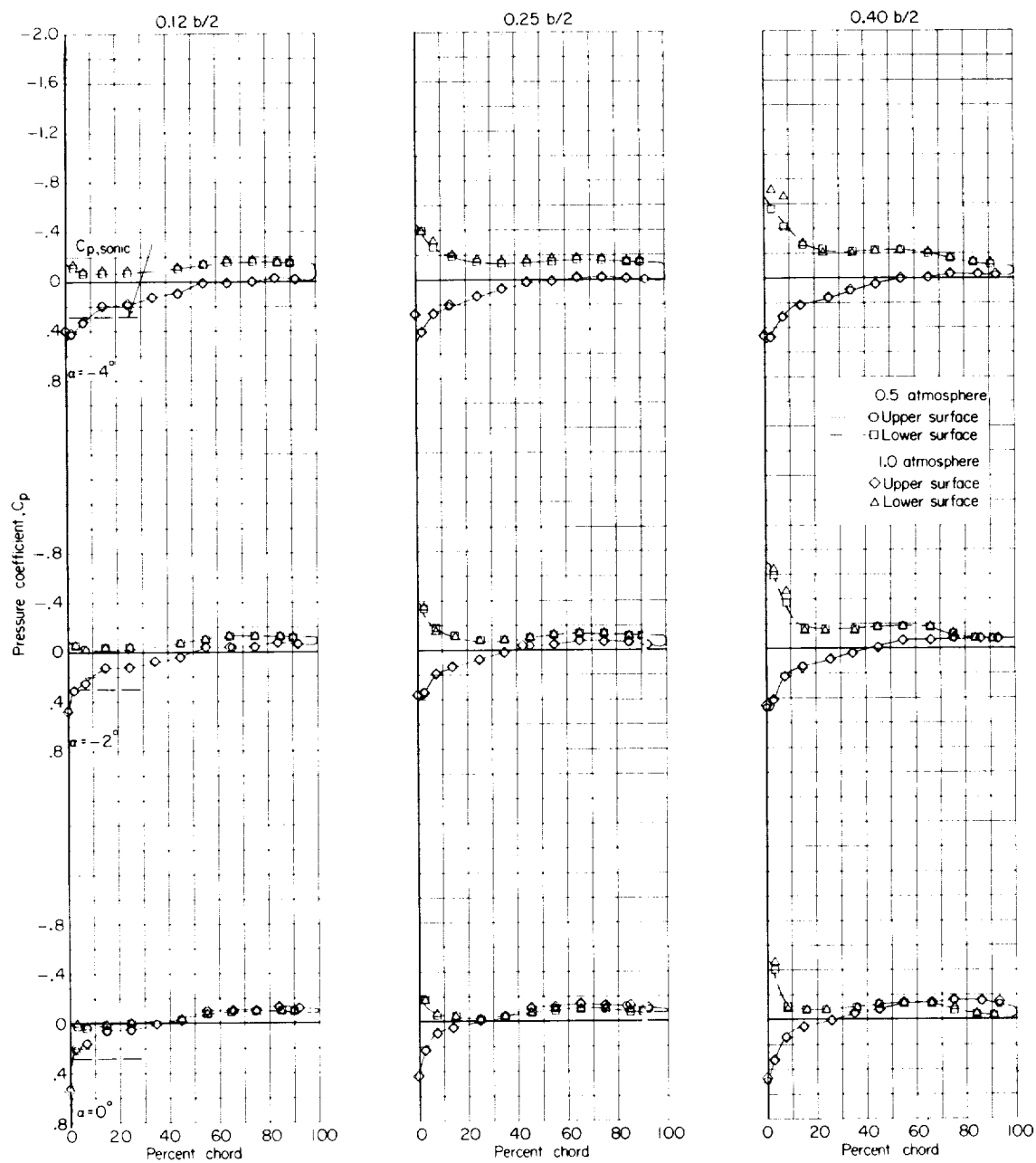
(1) $M = 1.125$; $\alpha = 2^\circ, 4^\circ, 8^\circ,$ and 12° .

Figure 4.- Continued.



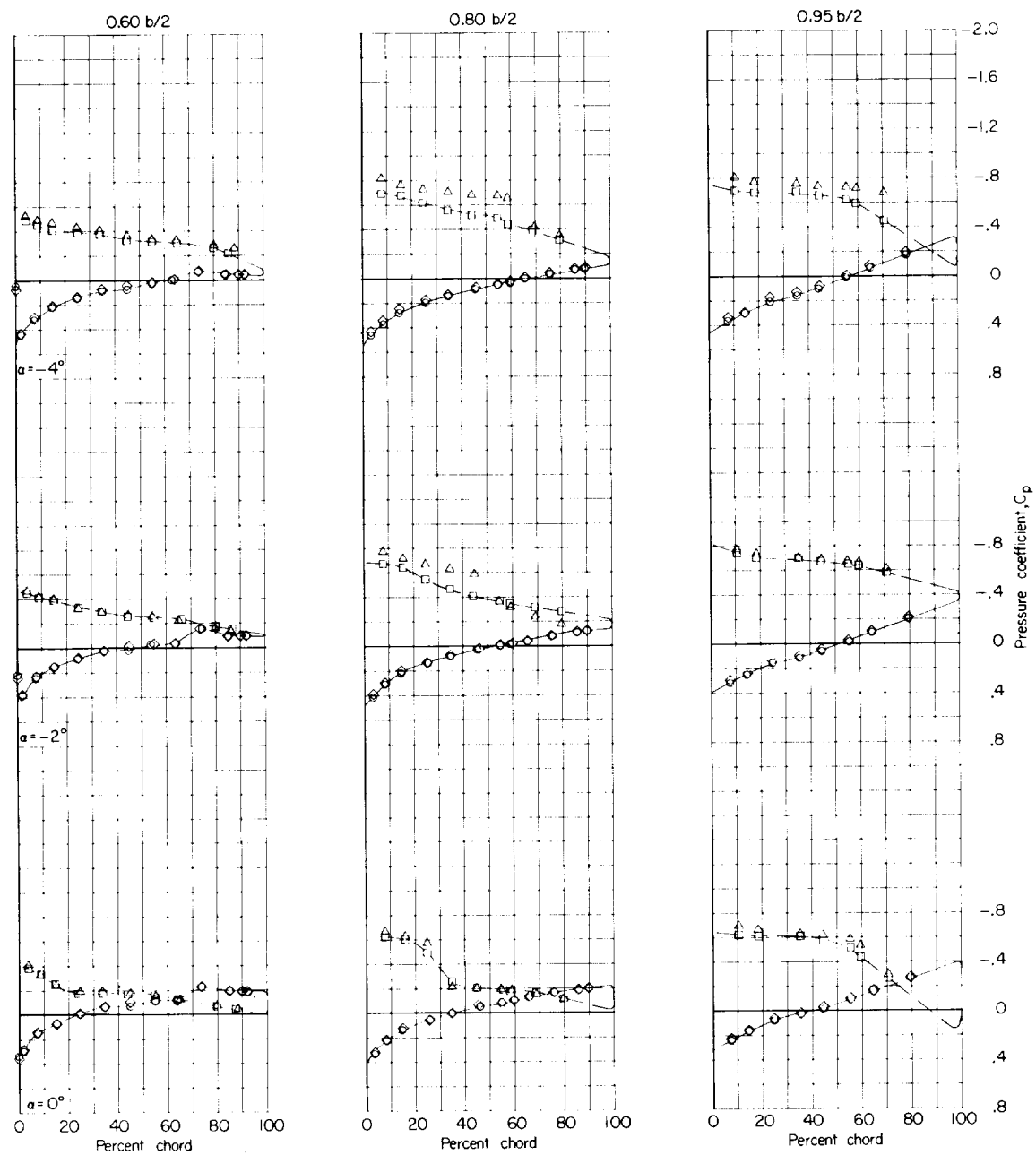
(1) Concluded.

Figure 4.- Continued.



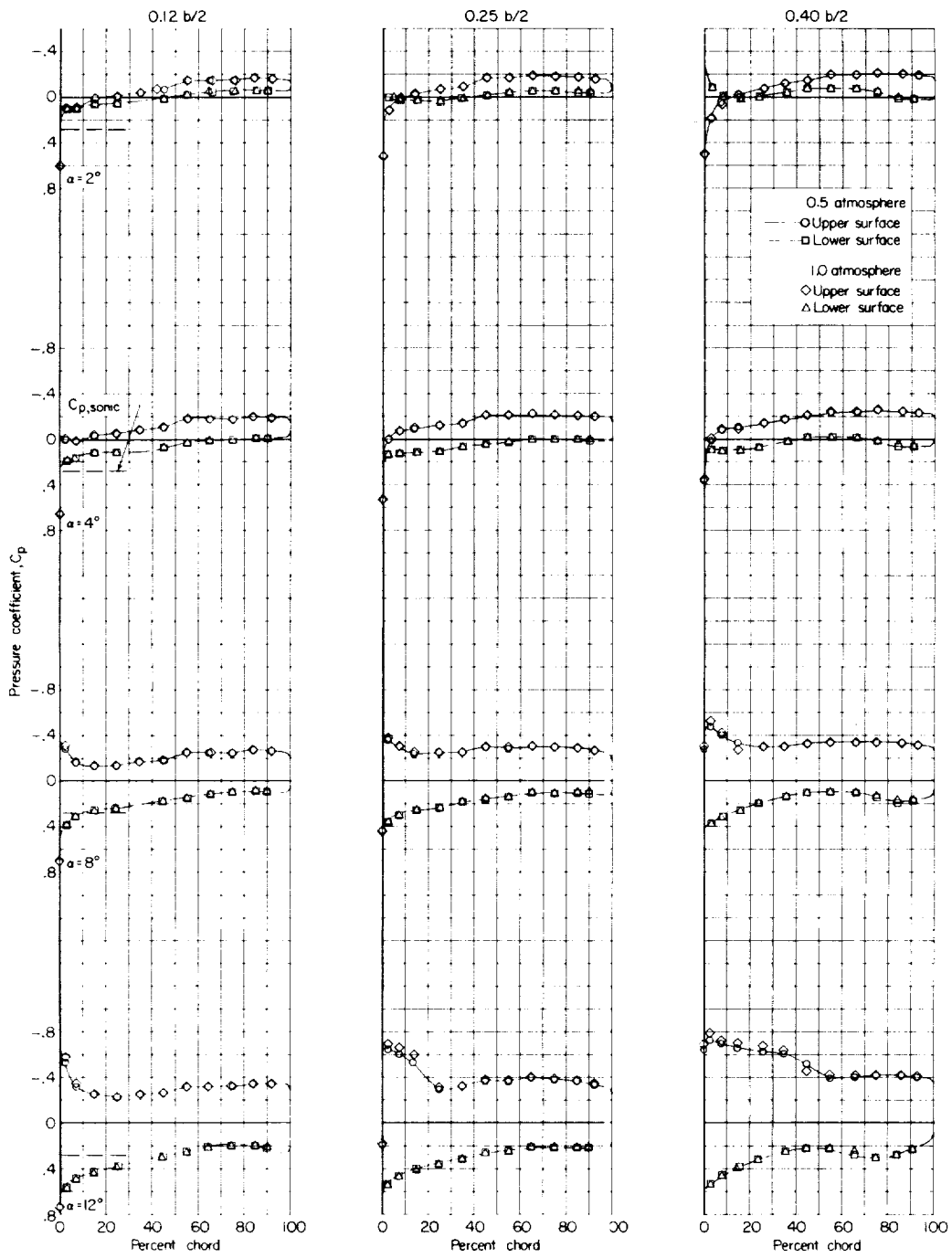
(m) $M = 1.200$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



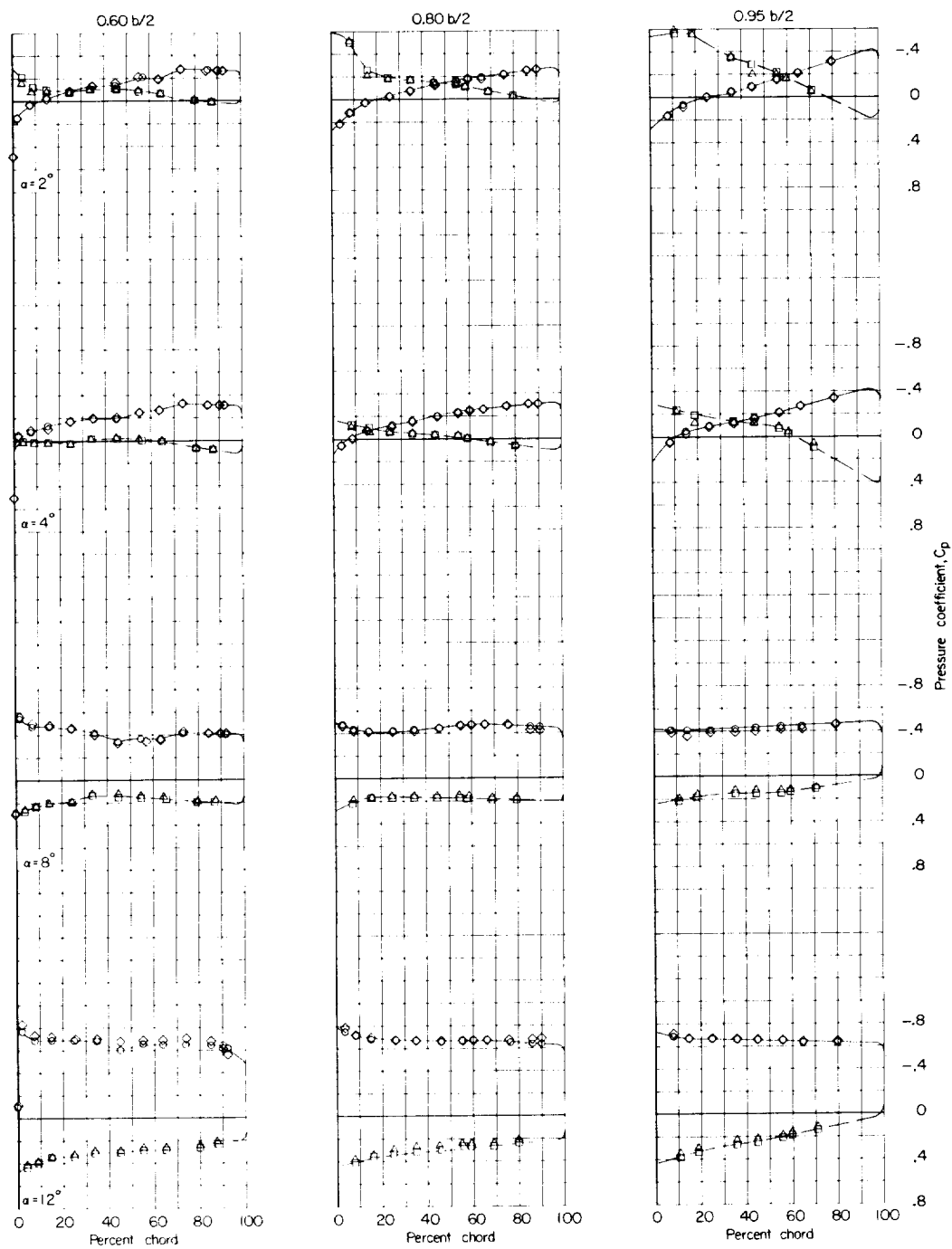
(m) Concluded.

Figure 4.- Continued.



(n) $M = 1.200$; $\alpha = 2^\circ$, 4° , 8° , and 12° .

Figure 4.- Continued.



(n) Concluded.

Figure 4.- Concluded.

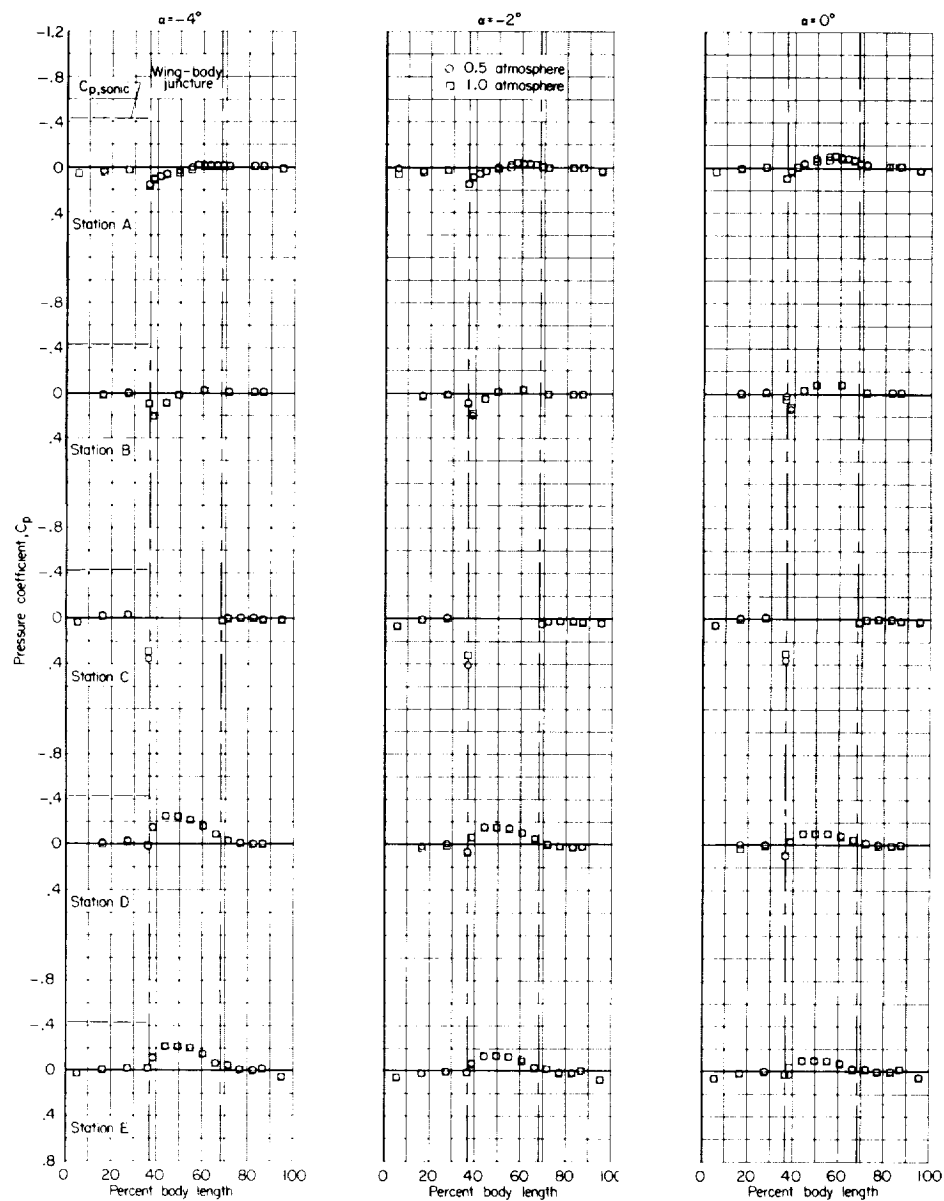
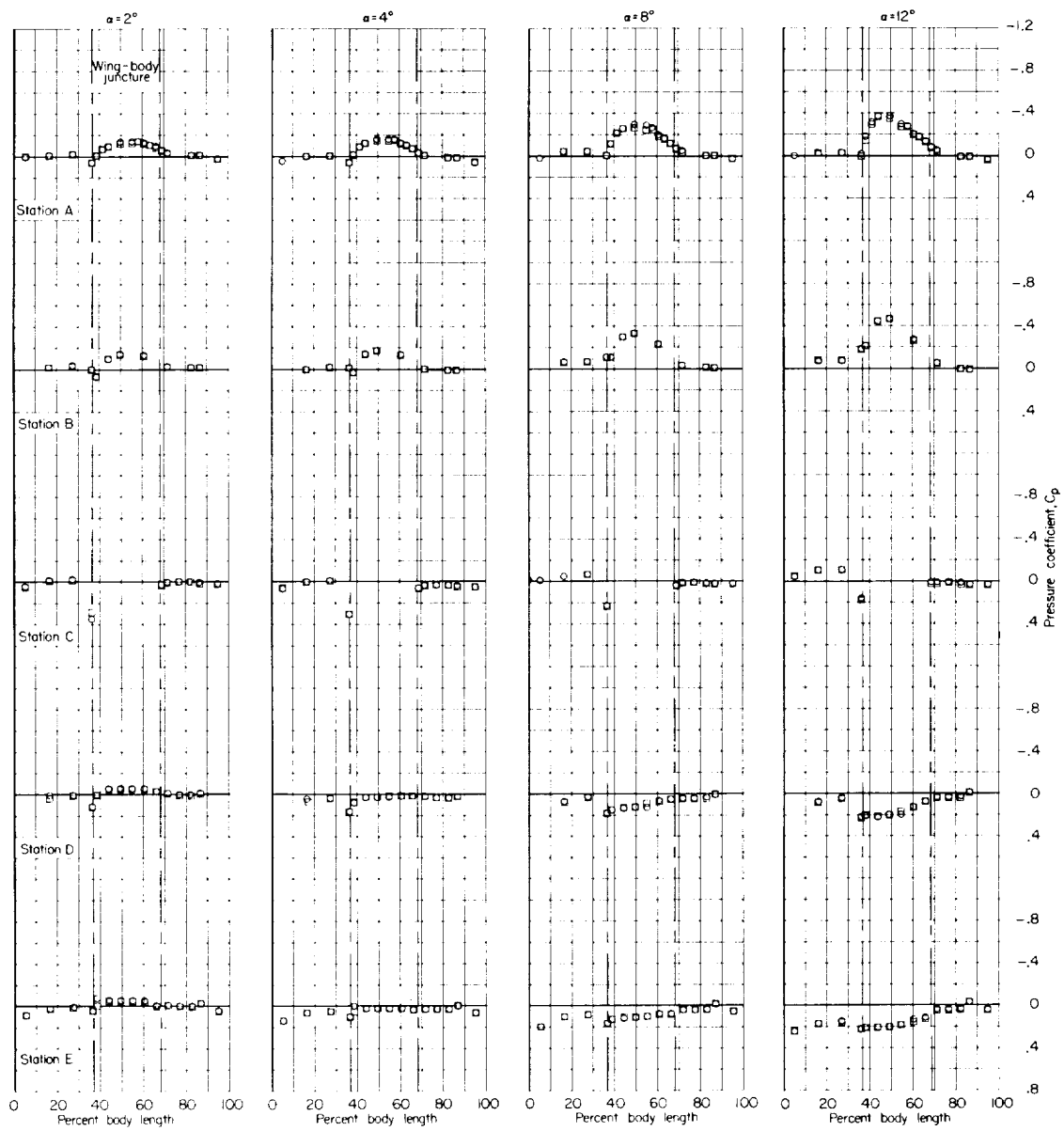
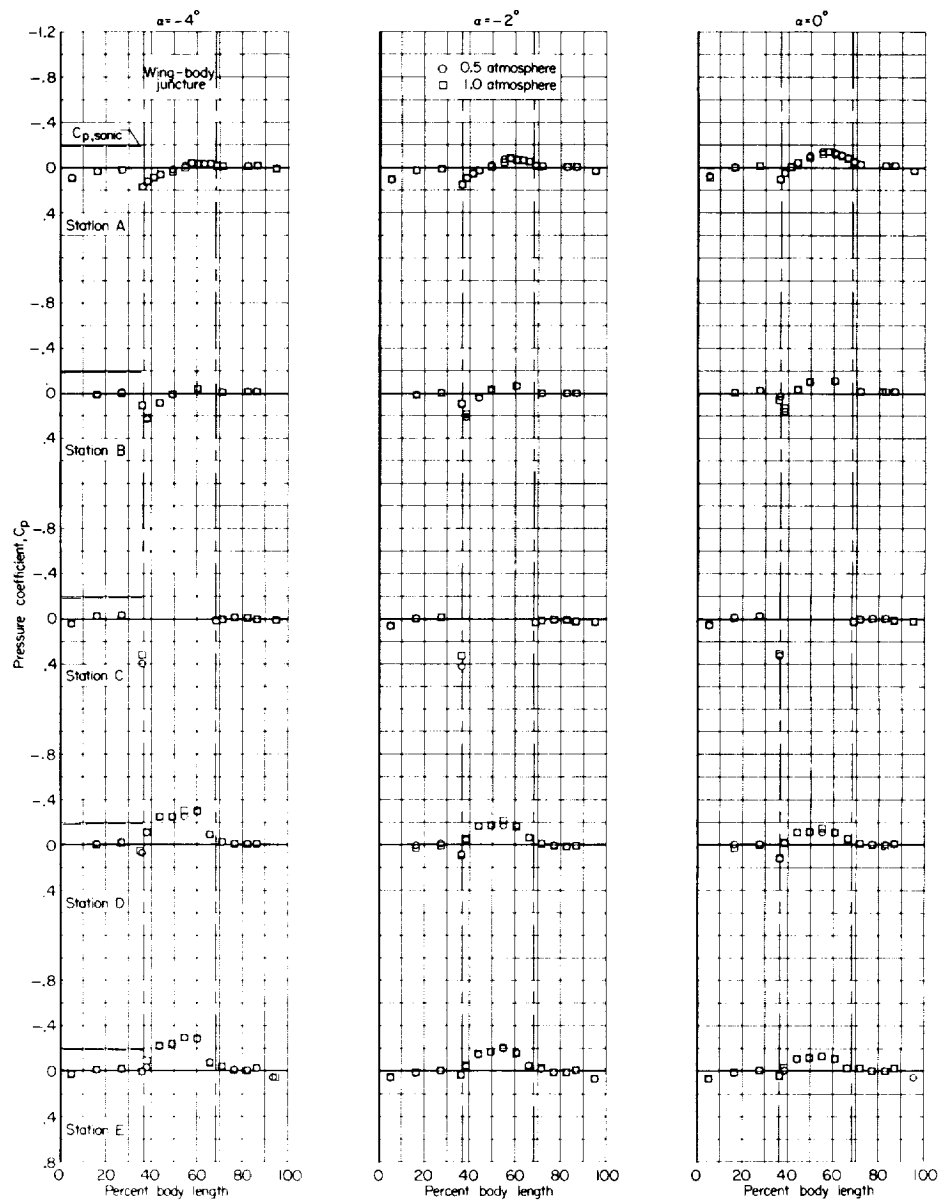
(a) $M = 0.800$.

Figure 5.- Pressure measurements on the body in the presence of the wing.



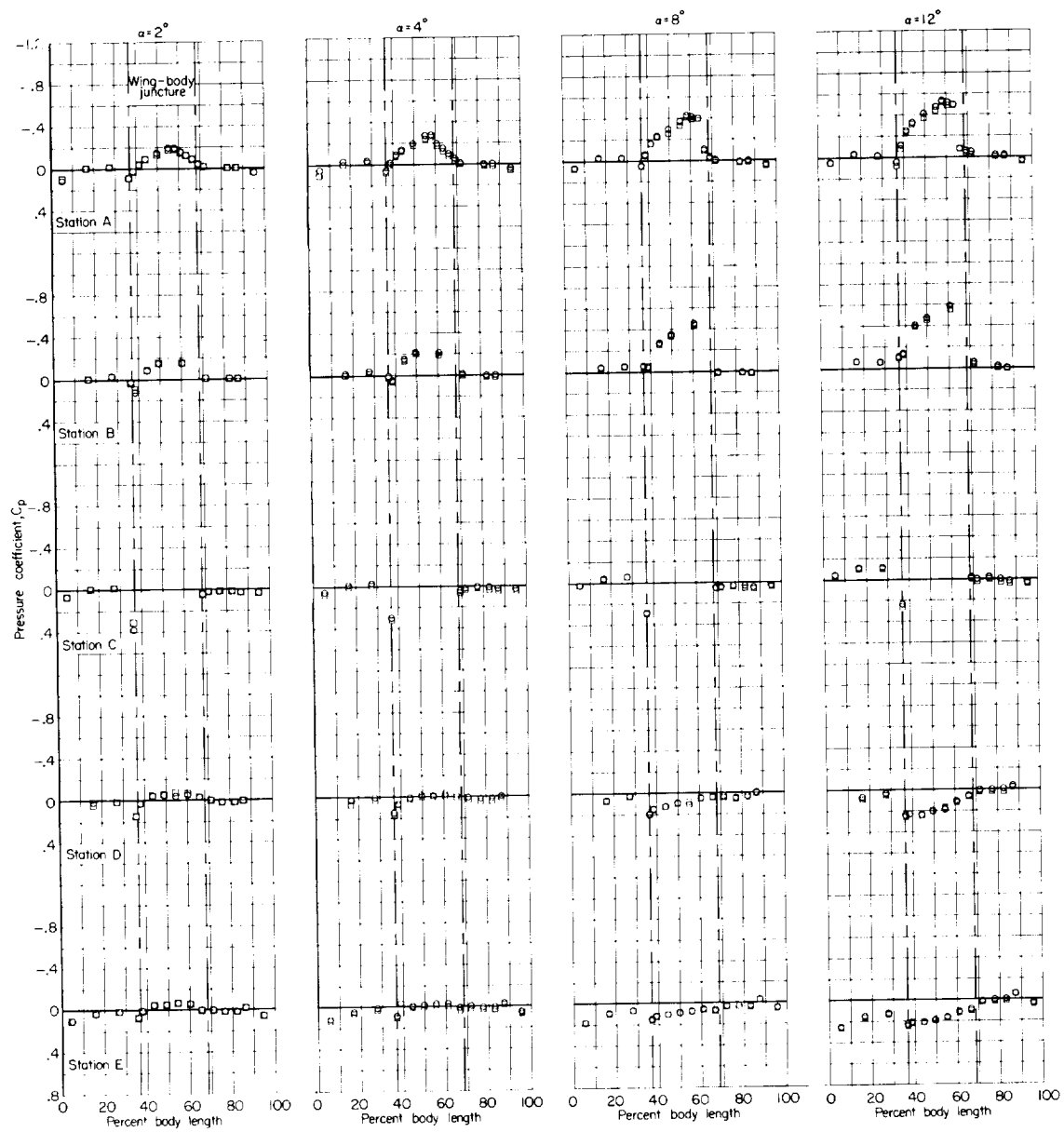
(a) Concluded.

Figure 5.- Continued.



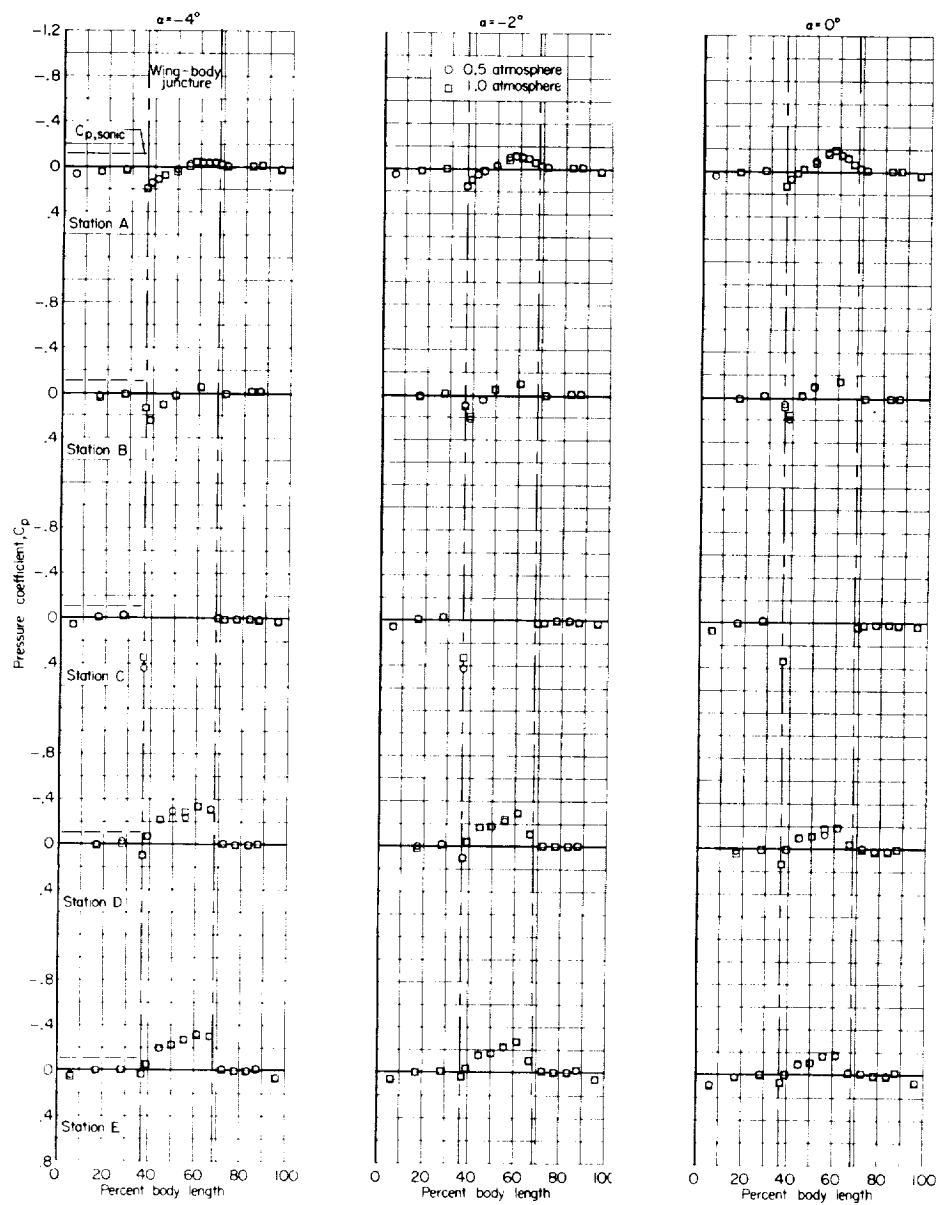
(b) $M = 0.900$.

Figure 5.- Continued.



(b) Concluded.

Figure 5.- Continued.



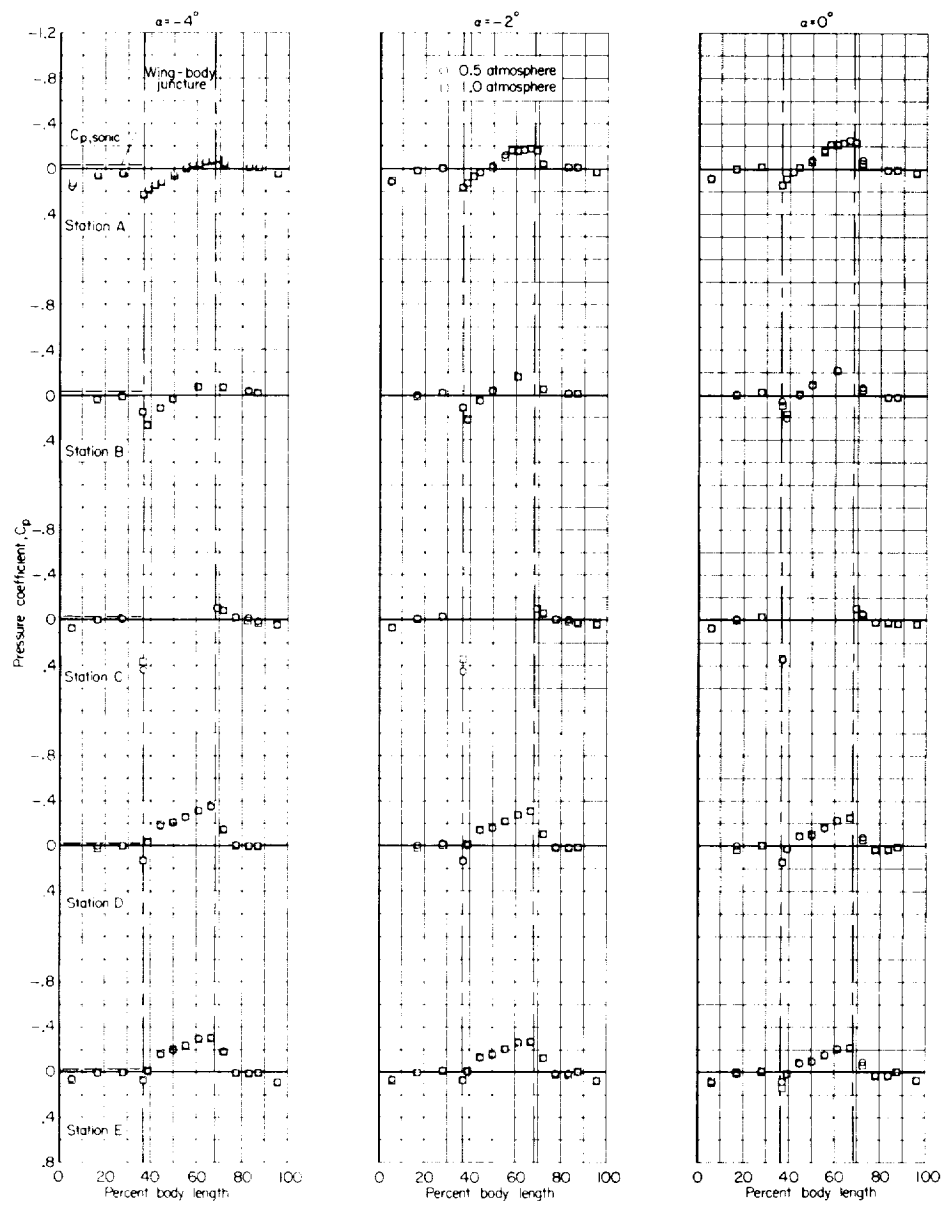
(c) $M = 0.940$.

Figure 5.- Continued.



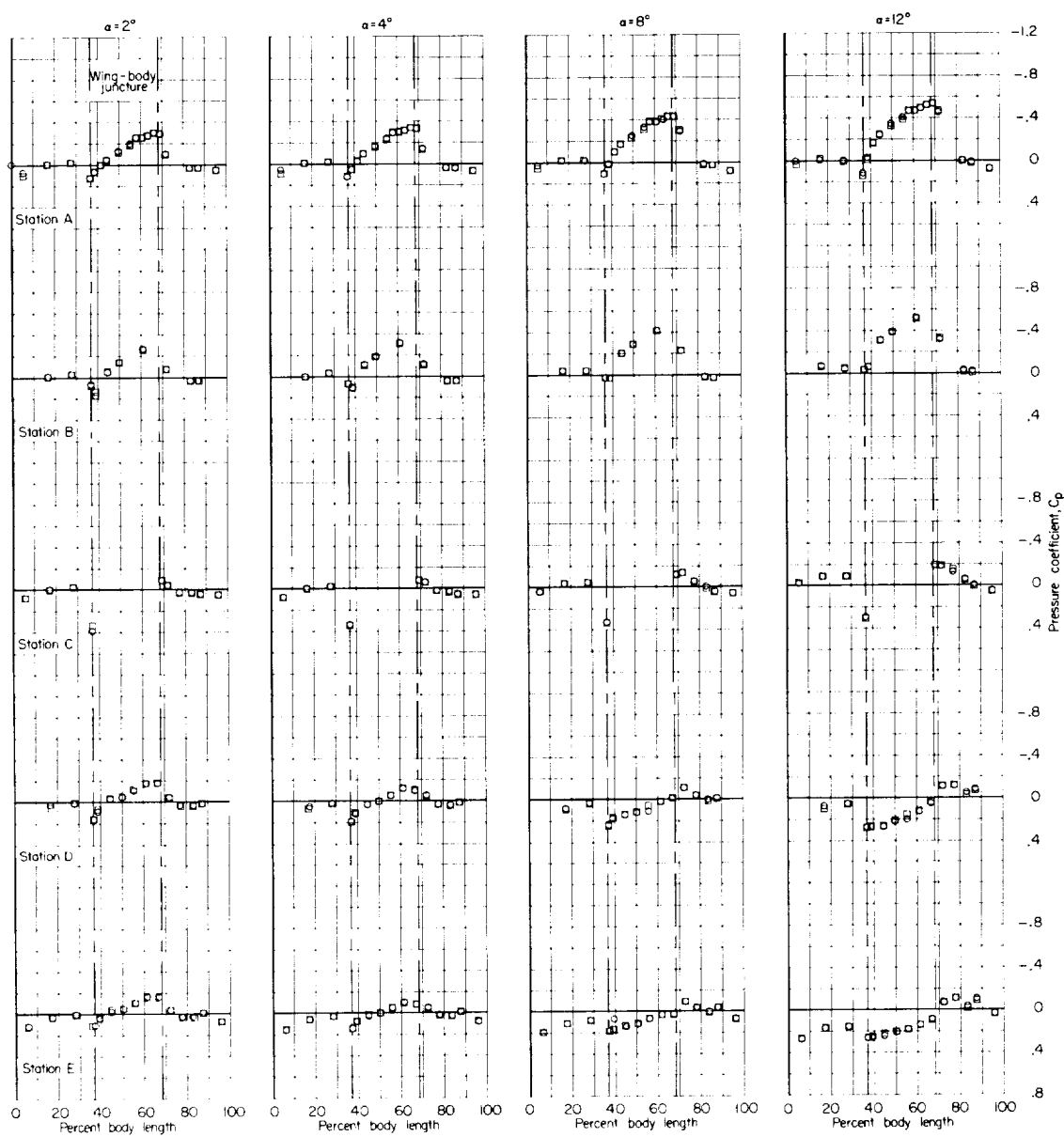
(c) Concluded.

Figure 5.- Continued.



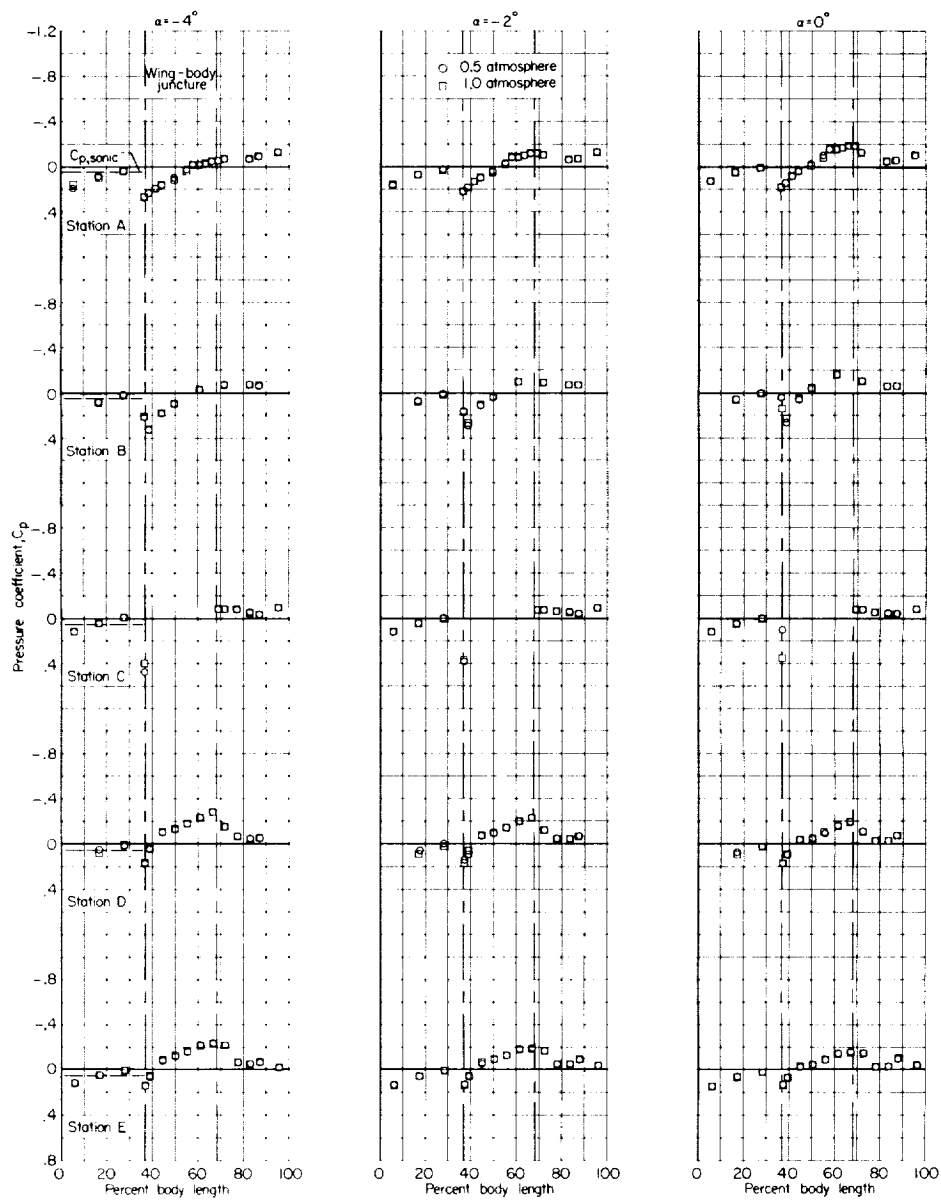
(d) $M = 0.980$.

Figure 5.- Continued.



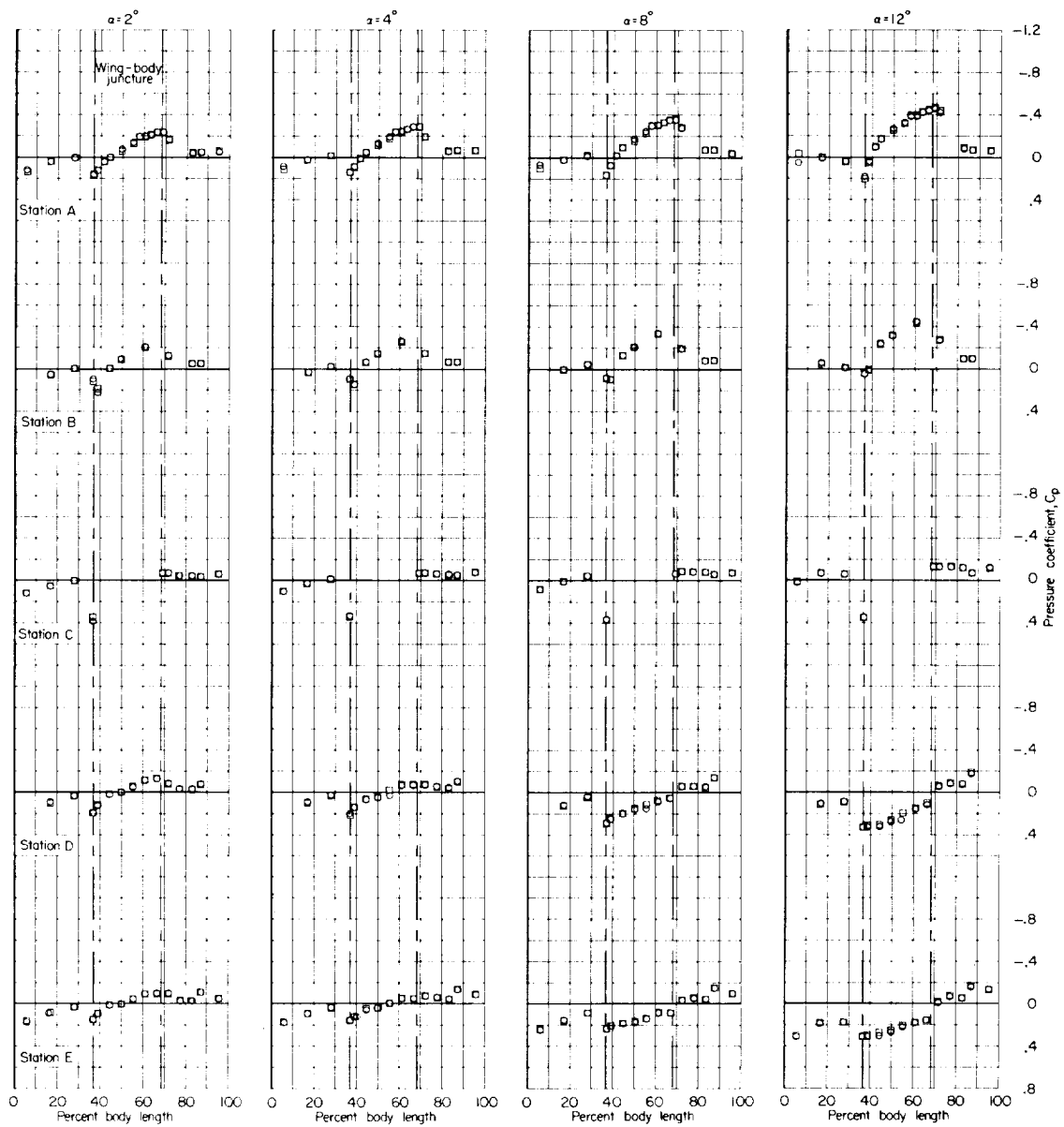
(d) Concluded.

Figure 5.- Continued.



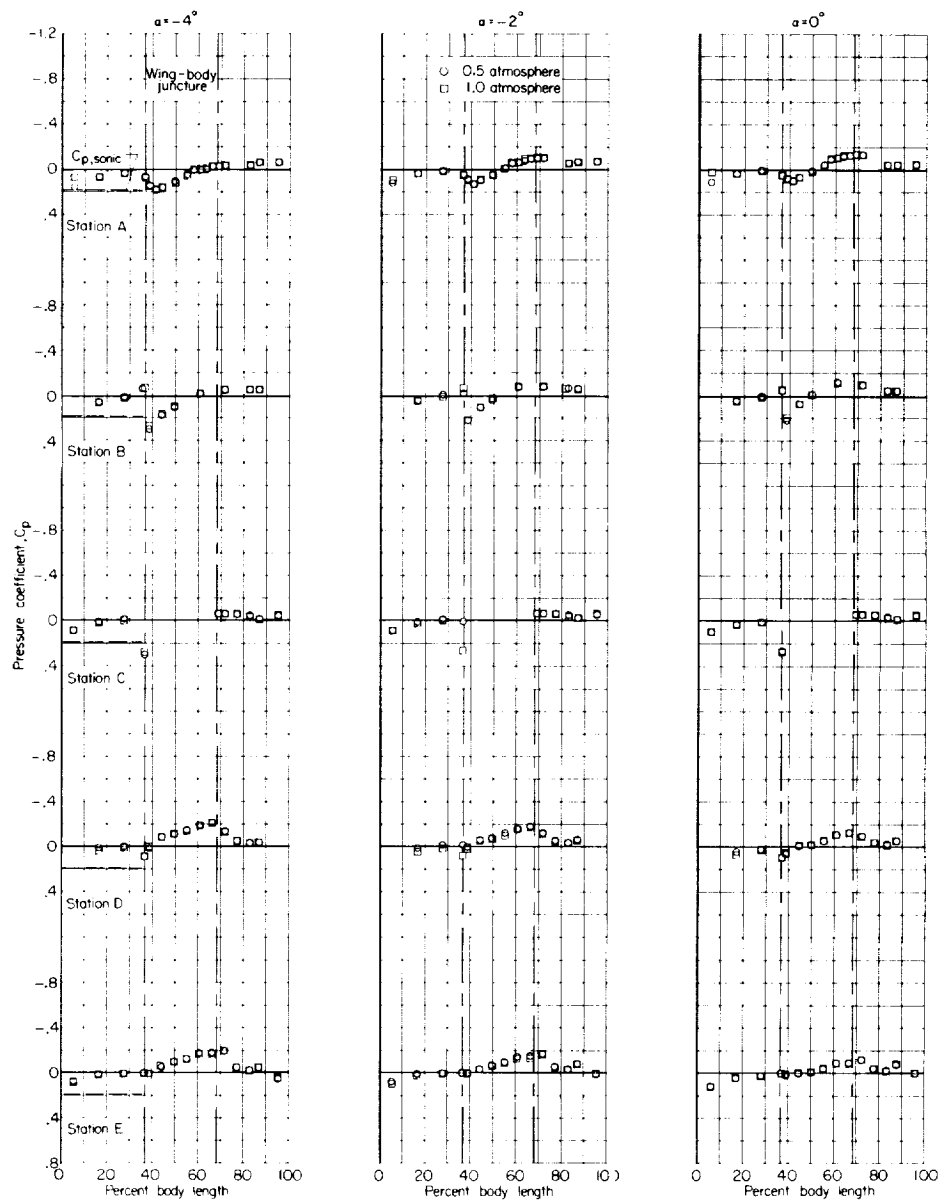
(e) $M = 1.030$.

Figure 5.- Continued.



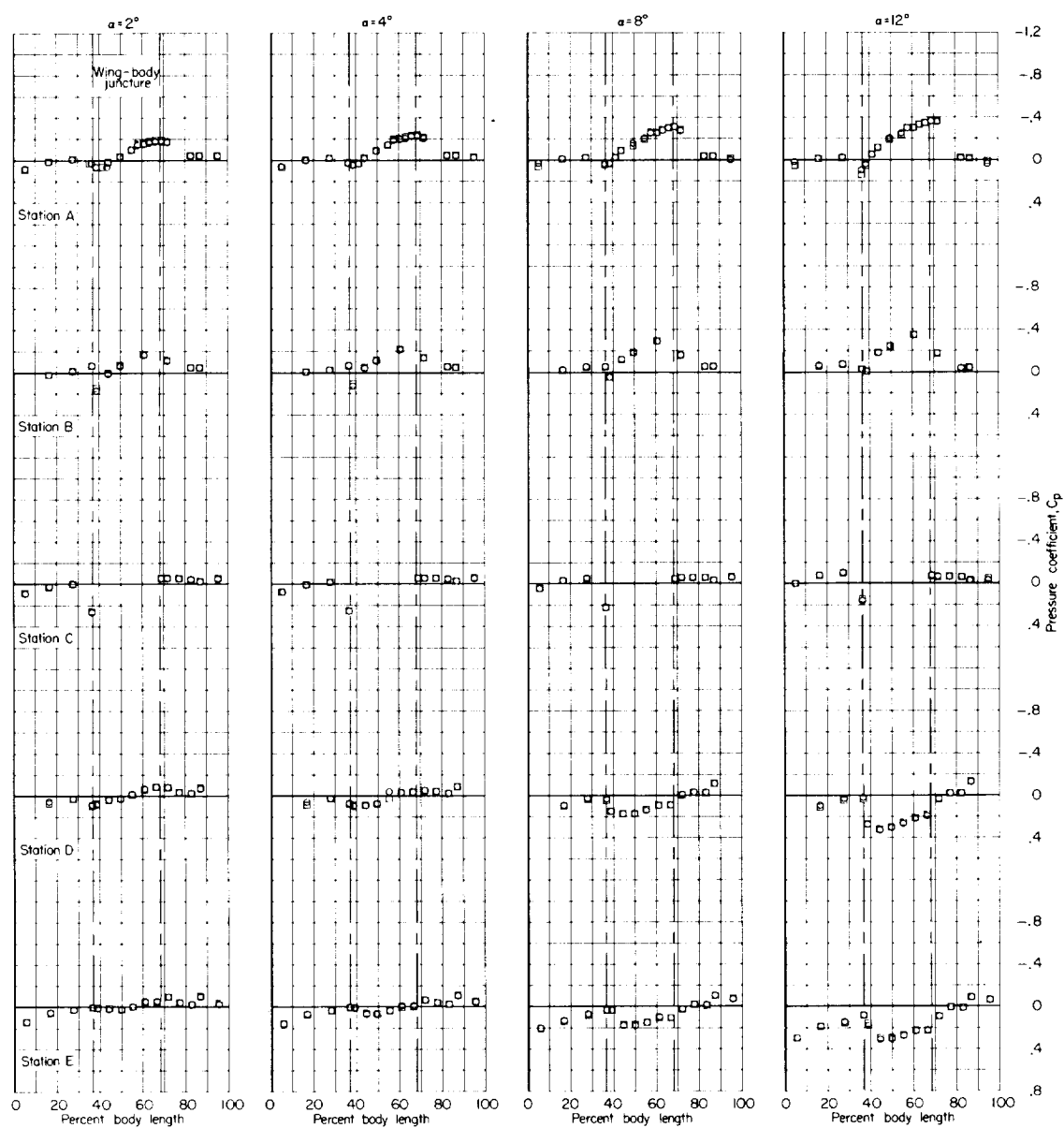
(e) Concluded.

Figure 5.- Continued.



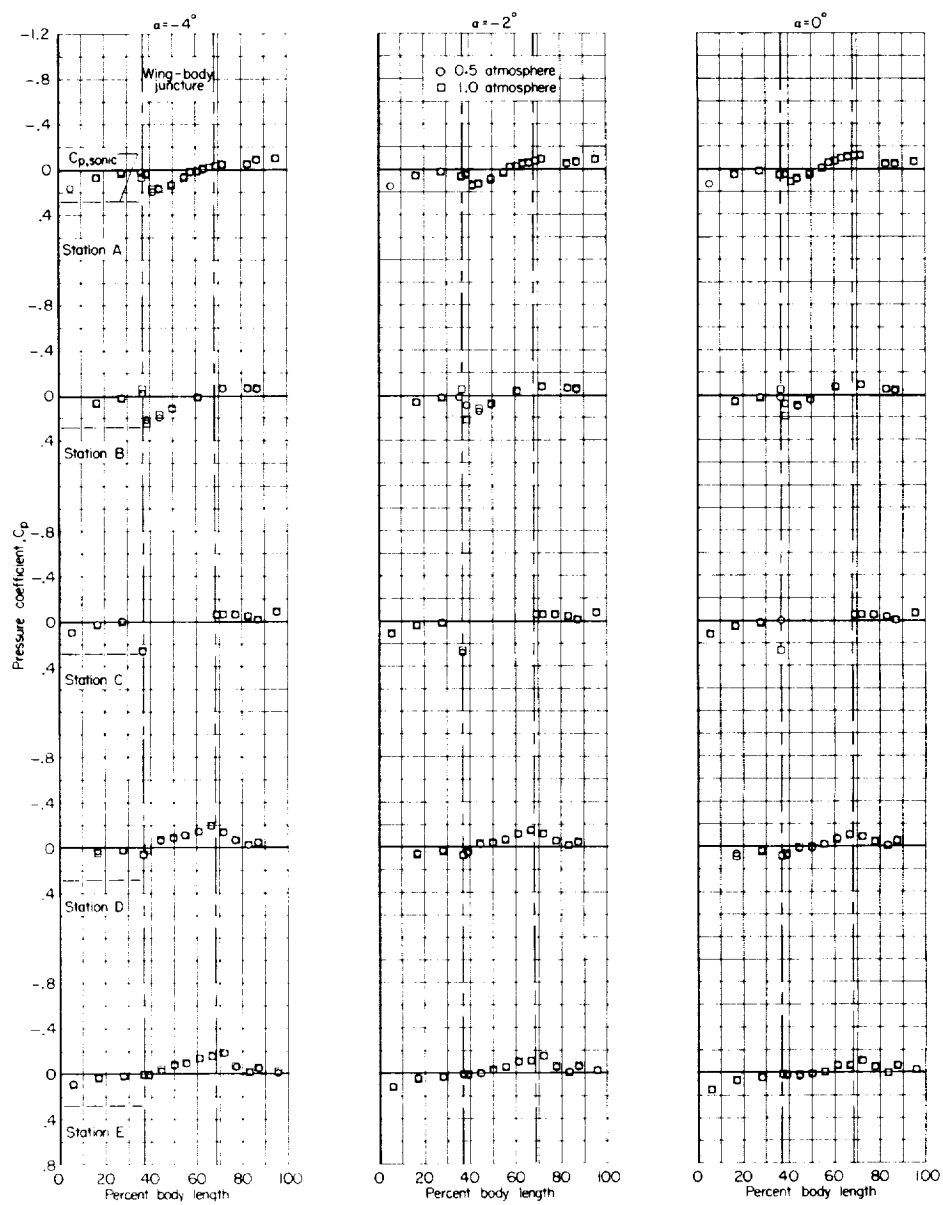
(f) $M = 1.125$.

Figure 5.- Continued.



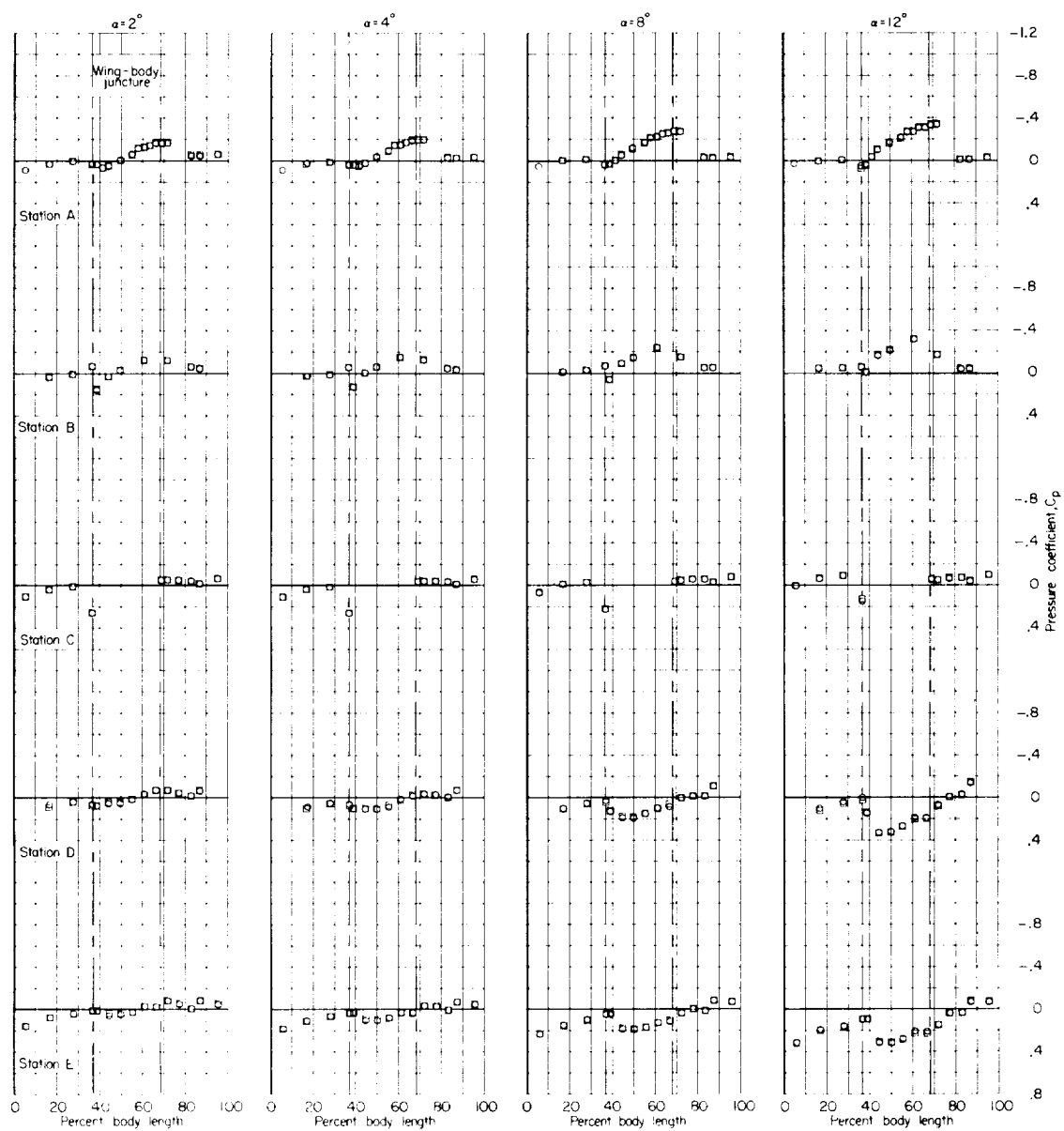
(f) Concluded.

Figure 5.- Continued.



(g) $M = 1.200$.

Figure 5.- Continued.



(g) Concluded.

Figure 5.- Concluded.

